

FINAL REPORT

SPACE SHUTTLE MAIN ENGINE STRUCTURAL ANALYSIS AND DATA REDUCTION/EVALUATION VOLUME 4: HIGH PRESSURE FUEL TURBO-PUMP INLET HOUSING ANALYSIS

April 1989

Contract NAS8-37282

Prepared for

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION
GEORGE C. MARSHALL SPACE FLIGHT CENTER, AL 35812

by

Kirby V. Pool

ORIGINAL CONTAINED
COLOR COPY

 **Lockheed**
Missiles & Space Company, Inc.
Huntsville Engineering Center
4800 Bradford Blvd., Huntsville, AL 35807

(NASA-CR-183667) SPACE SHUTTLE MAIN ENGINE
STRUCTURAL ANALYSIS AND DATA
REDUCTION/EVALUATION. VOLUME 4: HIGH
PRESSURE FUEL TURBO-PUMP INLET HOUSING
ANALYSIS Final Report (Lockheed Missiles

N89-27696

Unclas
G3/20 0211798

FOREWORD

This volume of the final report summarizes the analysis performed on the SSME High Pressure Fuel Turbo-Pump (HPFTP) Inlet Housing. Three DIAL finite element models were built to aid in assessing the structural life of the welds and fillets at the vanes. This analysis was performed by Kirby V. Pool under Contract NAS8-37282.

Complete results are given; however, some assumptions were made in determining the maximum surge pressure and in some weld material properties in the static/fatigue analysis. Therefore more information is requested for the closure of this study.

PRECEDING PAGE BLANK NOT FILMED

CONTENTS

<u>Section</u>		<u>Page</u>
	FOREWORD	ii
1	INTRODUCTION AND OVERVIEW	1
2	FINITE ELEMENT MODEL DESCRIPTION	3
	2.1 Global Model	3
	2.2 Detailed Vane Submodel	4
3	BOUNDARY CONDITIONS AND EXTERNAL LOADS	5
4	MATERIAL PROPERTIES	7
5	STRUCTURAL ANALYSIS	8
	5.1 Approach	8
	5.2 Results	8
	5.2.1 Global Model	8
	5.2.2 Detailed Vane Model	9
6	SUMMARY	11
7	RECOMMENDATIONS	13
8	REFERENCES	14

Appendixes

A	Final Global HPFTP Inlet Housing DIAL Finite Element Model Runstream	A-1
B	Final HPFTP Inlet Housing Detailed Vane Submodel DIAL Finite Element Model Runstream	B-1

LIST OF TABLES

<u>Table</u>		<u>Page</u>
1	Node and Element Breakdown for HPFTP Inlet Housing Components (3-D Global Model)	3
2	HPFTP Inlet Housing Stress Analysis - Summary of Results	11

CONTENTS (Continued)

LIST OF FIGURES

<u>Figure</u>		<u>Page</u>
1	Polaroid Photographs of Cut-up HPFTP Inlet Housing	15
2	HPFTP Inlet Housing - DIAL Global Finite Element Model	16
3	HPFTP Inlet Housing - DIAL Global Finite Element Model (Looking from Pump Toward Turbine)	17
4	HPFTP Inlet Housing - DIAL Global Finite Element Model (Looking from Turbine Toward Pump)	18
5	HPFTP Inlet Housing - DIAL Global Finite Element Model Exploded View Showing Model Components	19
6	HPFTP Inlet Housing - DIAL Global Finite Element Model Shell/Solid Element Interface (in Torus)	20
7	HPFTP Inlet Housing - DIAL Global Finite Element Model Typical Shell Element Vane/Solid Element Connection	21
8	HPFTP Inlet Housing - DIAL Detailed Vane Submodel Final Configuration of Shell Element Vanes	22
9(a,b)	HPFTP Inlet Housing - DIAL Detailed Vane Submodel (Color Light Source Shading Plot)	23
10	HPFTP Inlet Housing - DIAL Detailed Vane Submodel (Looking from Larger End of Torus Toward Smaller End)	24
11	HPFTP Inlet Housing - DIAL Detailed Vane Submodel (Looking from Larger End of Torus Toward Smaller End)	25
12	HPFTP Inlet Housing - Applied FPL Loading	26
13	HPFTP Inlet Housing - DIAL Detailed Vane Submodel Applied Displacement Boundaries (from Global Model) (Torus Removed for Clarity)	27
14(a,b)	HPFTP Inlet Housing - DIAL Detailed Vane Submodel Applied Displacement Vectors from Global Model (Torus)	28
15	Rocketdyne Materials Properties Manual - Ti-5Al-2.5Sn (ELI) Stress/Strain Curve (Typical Values)	29
16	Rocketdyne Materials Properties Manual - Ti-5Al-2.5Sn (ELI) Stress vs Number of Cycles to Failure (S/N) Curve (R = -1)	30
17	Rocketdyne Materials Properties Manual - Ti-5Al-2.5Sn (ELI) Modified Goodman Diagram (Machined Surface Finish)	31
18	Rocketdyne Materials Properties Manual - Ti-5Al-2.5Sn (ELI) Low Cycle Fatigue - Plastic Strain vs Number (R = -1.0)	32
19	HPFTP Inlet Housing - Global Model - Effective Stress Contour Plot of the Inner Ring Due to FPL Loading	33
20	HPFTP Inlet Housing - Global Model - Effective Stress Contour Plot on the Outer Ring Due to FPL Loading	34

CONTENTS (Concluded)

LIST OF FIGURES

<u>Figure</u>		<u>Page</u>
21	HPFTP Inlet Housing - Global Model - Effective Stress Contour Plot of Vane 1 (at Max Torus Radius) at FPL	35
22	HPFTP Inlet Housing - Detailed Vane Submodel - Effective Stress Color Contour Plot of Vane and Ring Intersections	36
23	HPFTP Inlet Housing - Detailed Vane Submodel - Effective Stress Contour Plot of Inner Ring Non-Pressure Surface	37
24	HPFTP Inlet Housing - Detailed Vane Submodel - Effective Stress Contour Plot of Inner Ring Pressure Surface	38
25	HPFTP Inlet Housing - Detailed Vane Submodel - Effective Strain Contour Plot of Outer Ring Pressure Surface	39
26	HPFTP Inlet Housing - Detailed Vane Submodel - Effective Stress Contour Plot of Vane and Fillet	40
27	HPFTP Inlet Housing - Detailed Vane Submodel - Effective Strain Contour Plot of Vane and Fillet	41

1. INTRODUCTION AND OVERVIEW

The SSME High Pressure Fuel Turbo Pump (HPFTP) contains several components that are highly stressed and subject to fatigue from cyclic loading. The Inlet Housing, which directs the flow of liquid hydrogen into the pump, is of particular concern because of the detection of cracks in the welded joints between the torus and the main body of the Inlet Housing (photographs of a sectioned Inlet Housing are shown in Figure 1). Whether these cracks occur as a result of fatigue loading from previous firings or from residual stresses due to the initial welding process, they are significant enough to require weld repair.

The process of weld repair creates some additional concern with regard to this part. During the weld repair process, the entire Inlet Housing is washed in an acid bath to clean and prepare the surfaces. This acid wash etches the grain boundaries of the titanium material, creating potential fatigue crack initiation sites. The existence of these micro-cracks could lead to a shorter high-cycle fatigue life for a given level of mean stress and cyclic loading. The purpose of this analysis was to assess the structural life of the areas around the welds and in the fillets of the vanes (which guide the flow of liquid hydrogen into the impellers).

Three DIAL (Ref. 1) finite element models were built for this analysis. A simple two-dimensional (2-D) model was constructed and analyzed as a first order estimate of the relative stress levels in the weld areas and in the vanes. The second model was a 360° global model, with simplified shell element vanes included, to determine where, around the circumference, the stresses are at a maximum. The third model was a detailed 3-D submodel of a slice of the global model through the region of maximum stress. This submodel included both of the critical weld areas, the torus shell, and one vane modeled

in sufficient detail to include the fillets at the vane attachments. The purpose of this model was to provide more accurate stresses in the critical weld areas as well as in the vane fillets.

As mentioned earlier, the goal of this analysis was to determine, based on the stress levels in the regions of concern and on the signal-to-noise (S/N) curve and Modified Goodman Diagram for the titanium alloy (Ti-5Al-2.5Sn EL1), what the safe life for the SSME HPFTP Inlet Housing should be. The analysis predicts stresses in the vicinity of the vane fillets which exceed the yield strength of the material at Full Power Level (FPL). Although there appears to be a fairly comfortable margin of safety with respect to the ultimate elongation of the material, any appreciable cyclic component to the load will greatly limit the fatigue life of the part. A nonlinear, plastic analysis of the hardware should be performed to provide an accurate estimate of the static stress margin of safety. Furthermore, a detailed study to determine the cyclic loading environment within the Inlet Housing will be necessary to accurately assess the fatigue life of this part.

2. FINITE ELEMENT MODEL DESCRIPTION

This discussion includes the global 3-D model and the detailed vane submodel. Details of the DIAL 2-D finite element model are given in the March and April Progress Reports. Since this model was for preliminary analysis only, details will not be discussed in this Final Report.

2.1 GLOBAL MODEL

Figure 2 is a shaded light source plot of the DIAL global 3-D model of the HPFTP Inlet Housing. Figures 3 and 4 are hidden line mesh plots of the model. Figure 5 shows cutaway views of the main components of the model. Table 1 lists the model components, providing a count of the number of nodes, type and number of elements, and the total number of degrees of freedom (DOF). Note that this model uses linear, hybrid stress solid elements.

Table 1 NODE AND ELEMENT BREAKDOWN FOR HPFTP INLET HOUSING COMPONENTS (3-D GLOBAL MODEL)

Component	Drawing Number	Nodes	Elements
Inlet Housing Main Body (360)	RS007512 (Sheets 35,40,41)	7651	4950 solids
Torus (0 - 360)	RS007512 (Sheet 36)	1754	660 solids 920 shells
Support Structure	RS007687	153	70 solids 24 shells
Vanes	RS007512 (Sheet 45)	494	480 shells
<u>TOTALS</u>		10052 (34980 DOF)	5680 solids 1424 shells

In several places in the model it was necessary to connect shell elements to solid elements. Figure 6 is a detail of a typical shell/solid interface which is designed to transmit moments as well as forces between the solid and shell elements. This type of interface is found in the torus portion of the model. The connection of the shell element vanes to the solid elements of the inner and outer rings (see Figure 4) was accomplished by extending the vane shell elements into the solid elements a depth of one element (thereby creating a moment resisting couple). Figure 7 shows this connection more clearly.

The refinement and thicknesses of the vane shell elements in the global model were established by means of a parametric study which attempted to match the stiffness of a typical "shell element" vane to that of the "solid element" vane in the detailed submodel. (The July Progress Report covers this study in detail.) Figure 8 depicts the final configuration for the global model vanes.

The DIAL runstream which generated the global model is included in Appendix A.

2.2 DETAILED VANE SUBMODEL

Plots of the detailed vane submodel are shown in Figures 9 through 11 (Figures 9a and 9b are light source shaded plots). The submodel comprises 8553 nodes, 1394 parabolic solid elements, and 286 parabolic shell elements, and has a total of 28446 DOF. The vane and fillets were modeled as accurately as possible, based on the dimensions provided in drawing number RS007512-131. A sensitivity study was performed which varied the element refinement in the fillets. The results discussed in the August Progress Report showed that the mesh density was adequate.

The DIAL runstream which generated the detailed vane submodel is included in Appendix B.

3. BOUNDARY CONDITIONS AND EXTERNAL LOADS

In the early phase of this analysis the loading on the Inlet Housing consisted solely of internal pressure within the torus. The pressure used (178 psid) was a nominal pressure supplied by engineers at the Huntsville Engineering Center (HEC). A package containing more realistic loads for the Inlet Housing, prepared by J. Chaffin of Rocketdyne (Ref. 2), was received by HEC and forwarded to LMSC, Sunnyvale, the week of 22 July 1988. Figure 12 is a schematic diagram of the FPL loading which was used for this final analysis. As can be seen in the figure, the 178 psid was increased to 303 psid. The maximum value for these loads in a surge condition is not conclusively known. For the purpose of this analysis, a 10% alternating pressure component was assumed.

The boundary conditions for the global model were simply a fixity of all translations at the location where the Inlet Housing is bolted to the main body of the pump. The support structure (to which the Hydrogen Inlet Manifold is bolted) was not restrained in any way.

The loading on the detailed vane submodel consisted of applied displacements along the boundaries of the submodel and pressure loads, to match the values depicted in Figure 12 for the global model (303 psi internal pressure and 208 psi external back pressure). The applied displacements were obtained from the global model through an automated process in the DIAL finite element code. Figure 13 shows the detailed vane submodel (the torus is removed for clarity) with the surfaces to which the displacement boundary conditions are applied. As can be seen from the figure, displacements were applied on each radial cut surface (at 24° and -30°) as well as on the two circumferential cut surfaces of the submodel. Since the circumferential cut surfaces lie directly behind the vane attachments, it is clear that the displacements applied to

these surfaces will have, by far, the largest effect on the stresses in the vane and fillets. Figures 14a and 14b show the applied displacement vectors on either end of the submodel torus.

The displacements applied to the boundaries of the submodel were compared manually with the displacements of the global model (at the same locations) as a check on the automated process mentioned above. The displacements were continuous and smooth, and no discrepancies were found.

The submodel, which contains one vane, required a span of 54° to assure that there was sufficient distance between the ends of the vane and the model boundaries. However, since the Inlet Housing has 15 vanes around the circumference, the average span per vane is really 24° . This means that there is a significant overlap between the vanes which is not accounted for in the submodel (see phantom lines in Figure 13). The fact that the submodel does not include the portions of the other vanes that would exist in a 54° segment does not significantly affect the accuracy of the results, though. The reason for this is that the applied displacements (which completely dominate the loading) are obtained from the global model, in which there is a vane every 24° . If the displacements are correct, then the loading into the vane should be correct.

One effect of the larger span is an increased surface area for the applied pressure to act upon. The increase in vane stresses due to this additional pressure load is very small because the applied displacements are the major contributor to the stresses in the vane.

4. MATERIAL PROPERTIES

The material used for the HPFTP Inlet Housing is Ti-5Al-2.5Sn ELI. All material property information was obtained from the Rocketdyne Materials Properties Manual (Ref. 3) for a temperature of -350 °F. Figures 15 through 18 show excerpts from the Rocketdyne manual for a stress/strain curve (typical values are shown), a high-cycle fatigue S/N curve, a Modified Goodman Diagram (for a machined surface), and a low-cycle fatigue diagram.

5. STRUCTURAL ANALYSIS

Several iterations were made to improve and validate both the 360° global model and the detailed vane submodel. These iterations are documented in detail in prior Progress Reports and therefore will not be discussed here.

5.1 APPROACH

At the onset of this analysis, it was determined that two models (a 360° global model of the entire Inlet Housing and a detailed submodel of a single vane) would be necessary to adequately assess this geometrically complex part. The global model served three purposes:

- Prediction of the location of the highest vane stresses
- Displacement boundary conditions for the detailed vane submodel analysis
- A first order prediction of stresses in the critical weld areas where the torus is attached to the Inlet Housing main body.

The purpose of the detailed vane submodel was to achieve accurate modeling of the critical weld areas and a vane (complete with fillets). Both of these models were needed to assess the capability of this part to withstand the required environment.

5.2 RESULTS

5.2.1 Global Model

The primary purpose of the global model was to provide displacement boundary conditions for the detailed vane submodel. The stresses are not considered to be accurate, but they are presented here for completeness.

Figure 19 is an effective stress contour plot of the outer ring (from inside the ring looking out) due to FPL loading. Note that there is clearly a region where the stress appears to be the greatest. This maximum (~ 90 ksi) occurs at the location where the torus diameter is a maximum (near vane 1). This is logical, when one considers that the stress in a cylinder with internal pressure varies in direct proportion with the radius of that cylinder. Figure 20 shows the effective stress in the inner ring (from outside the ring looking in) at FPL. Note, again, that the stress varies along the circumference, with the maximum (85 ksi) occurring at the maximum torus diameter location. The weld area on the inner ring (weld 1) is indicated by the dashed line. Because this weld is smooth, with no stress concentrations, the stress here is only about 55 ksi. Figure 21 shows the computed effective strain in vane 1 (at the maximum torus diameter). This also varies as a function of circumferential position.

5.2.2 Detailed Vane Submodel

Based on the results of the global model, the vane closest to the torus maximum diameter was selected to be modeled in the detailed vane submodel. Figure 22 is a color contour plot of the inside (where pressure is applied) surfaces of both the inner and outer rings and the vane. The areas of particularly high stress are clearly shown to be the fillets of the vane and the weld 2 (outer ring) area. Figures 23 and 24 show line contour plots of the effective stresses (for FPL loading) on the inner ring non-pressure and pressure surfaces, respectively. Figure 25 shows the same for the outer ring pressure (inside) surface. The maximum value for effective stress in the inner ring is 119 ksi (Figure 23), and in the weld 1 area (Figure 24) it becomes ~ 90 ksi. The maximum effective stress in the outer ring occurs in the weld 2 area and peaks at a value of ~ 160 ksi. Please note that the areas near the boundaries where there appear to be extremely high stresses are of no concern. These high stresses are products of the applied displacements and die out very quickly.

Figure 26 shows the effective stress in the vane submodel (the torus is removed for clarity) at FPL loading. The maximum effective stress of 237 ksi occurs in the fillets at the leading edge of the vane. This stress value, which exceeds the ultimate stress capability of the material ($S_y = 154$ ksi, $S_u = 163$ ksi - see Figure 15), is not accurate since it was computed assuming linear elastic material response. Figure 26 shows that the maximum effective strain for this linear analysis is 1.37%. The ultimate elongation for the material, according to the Rocketdyne Materials Properties Manual (Ref. 3), is on the order of 15%. The yielding in the vane fillet is extremely localized in the high stress concentration area of the fillet region. In reality (or in a nonlinear analysis), any yielding will allow the load to redistribute and therefore keep the plastic strain low and the margin of safety for the static load condition fairly high. There is little doubt, however, that the stresses in the vane fillet at FPL loading are at or above yield. This directly affects the fatigue life of the HPFTP Inlet Housing.

The current assumption with regard to fatigue life assessment is that the alternating load is 10% of the mean loading. Using this assumption, and looking at the Modified Goodman Diagram in Figure 17, it is clear that the weld 1 area (effective stress is 90 ksi) should withstand 10,000,000 cycles of loading. It is equally clear that the fatigue life of the HPFTP Inlet Housing vanes (effective stress, 237 ksi) and of the weld 2 area (effective stress, 160 ksi) will be extremely limited, possibly to the point of creating low-cycle fatigue problems. Since fatigue failures in the vanes are not common, the cyclic loading environment is apparently not nearly as severe as was assumed here.

6. SUMMARY

Table 2 is a summary of the results, for nominal and FPL loading, for both of the models used in this analysis. Overall, the effective stresses in the detailed vane submodel are about 40 to 78% higher than those predicted in the global model. This is most likely due to the coarseness of the 3-D global model mesh (which also used linear instead of parabolic solid elements). Note that a direct comparison of the stresses between the two models should not be made, since the global model's purpose was primarily to provide input for the detailed vane submodel. A comparison of average effective stress was made near the center of the critical vane for both models. The correlation here for the FPL loading is fairly good.

Table 2 HPFTP Inlet Housing Stress Analysis - Summary of Results

Model (load case)	Weld 1 Inner Ring	Weld 2 Outer Ring	Vane Fillet	Center of Vane 1
Global (NPL) Eff-Stress (ksi)	32	53	--	~20
Global (FPL) Eff-Stress (ksi)	55	90	--	~30
Detailed Vane (NPL) Eff-Stress (ksi)	53 (+1.9)!	94 (+.64)	--	~20
Detailed Vane (FPL) Eff-Stress (ksi)	90 (+.71)	160 (-0.04)*	237 (-.35)*	~30

- NOTES: NPL - Nominal Pressure Level - 189 psid internal torus pressure.
 FPL - Full Power Level - 303 psid internal torus pressure.
 ! - Numbers in parentheses are Static Margins of Safety based on a 1.0 Factor of Safety and $S_y = 154$ ksi.
 * - These margins are the result of a linear analysis. A non-linear plastic analysis would most likely produce positive margins based on the maximum strain allowable of 15% (237 ksi corresponds to effective strain of 1.37%).

Static margins of safety for the FPL loading, based on a 1.0 Factor of Safety and a yield stress of 154 ksi, are included where the stress remains in the linear range. In the fillets of the vanes, where yielding occurs, only a nonlinear plastic analysis can provide a reliable margin.

An accurate assessment of the fatigue life of the HPFTP Inlet Housing requires a knowledge of the cyclic loading environment (including both magnitude and period of the loading), as well as an S/N curve and Modified Goodman Diagram for the proper material with the proper surface finish. Given the magnitude of the stresses predicted here, a low-cycle fatigue curve (for the proper R of +0.90) would also be helpful. Since these data do not yet exist, or at least they have not yet been provided, all that can be stated conclusively is that a concern for the fatigue life of this part does exist.

7. RECOMMENDATIONS

If it is true, as the results of this analysis show, that the vane fillets are stressed to nearly 1.5 times the stress level in the welds, then one must ask why there have been cracks reported in the welds but not in the fillets of the vanes. Apparently, either the material properties in the weld are very different from the wrought material in the vanes, or there is some aspect of the loading that is not being treated properly. Several missing pieces of information are essential to the closure of this study:

1. Material data for the weld material are needed in the form of a stress-strain curve, an S/N curve, a Modified Goodman Diagram for the proper heat-treat (annealed?), temperature (~350 °F), and surface conditions (chem milled?). The titanium in the weld material is a "cast" microstructure as opposed to a "wrought" microstructure for the vanes. Consequently, it is very possible, even likely, that their fatigue characteristics would be very different.
2. Measure pressure data are needed to verify the cyclic component of the load. The loading environment given for this problem assumes that the cyclic component of the load is 10% of the mean value. If it can be shown to be significantly smaller than this in the vane fillet, the loading can be regarded as static and the life of the vane fillet would be determined by low-cycle fatigue, where the number of cycles is the number of engine firings.
3. Data on the effect of cyclic loading with plastic prestrain are needed to predict the life of the vane fillet if the cyclic component of the loading is in fact significant.
4. A nonlinear plastic analysis is needed to determine the level of plastic strain in the vane fillet. This knowledge can be used to determine the static margin of safety and assess the low-cycle fatigue capability of the part, given the data in item 3 above.

8. REFERENCES

1. DIAL Finite Element Analysis System, User's Manual. LMSC Document.
2. J. Chaffin, Rocketdyne Internal Memo, 14 July 1988.
3. Rocketdyne Materials Properties Manual, Section 5002 (Ti-5Al-2.5Sn ELI).

ORIGINAL PAGE
COLOR PHOTOGRAPH

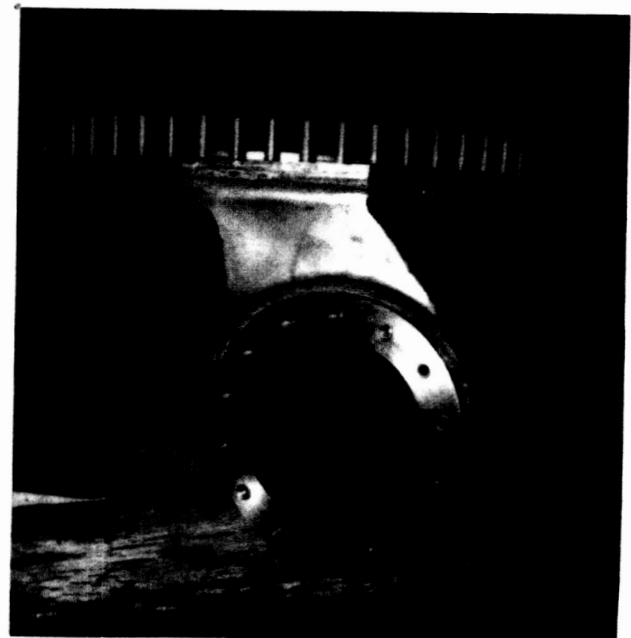
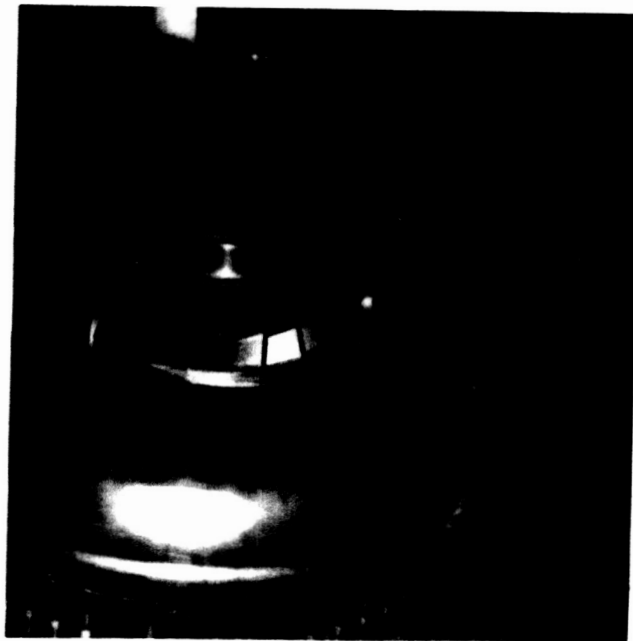
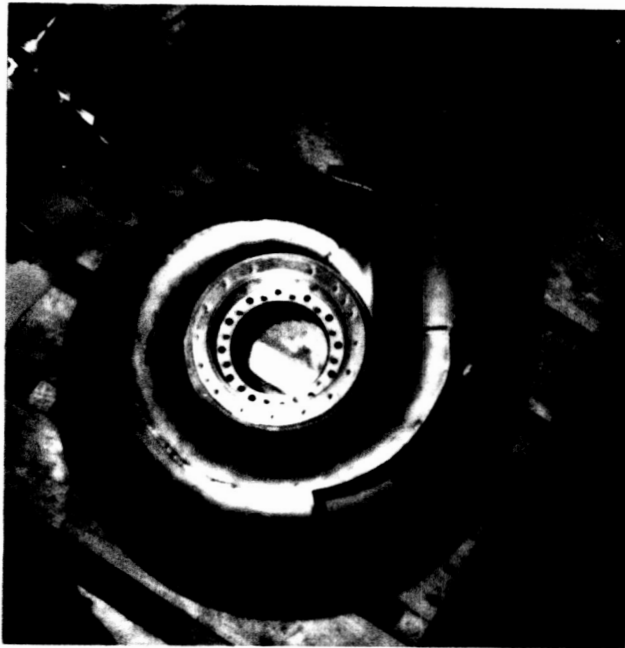


Figure 1 Polaroid Photographs of Cut-Up HPFTP Inlet Housing

ORIGINAL PAGE
COLOR PHOTOGRAPH

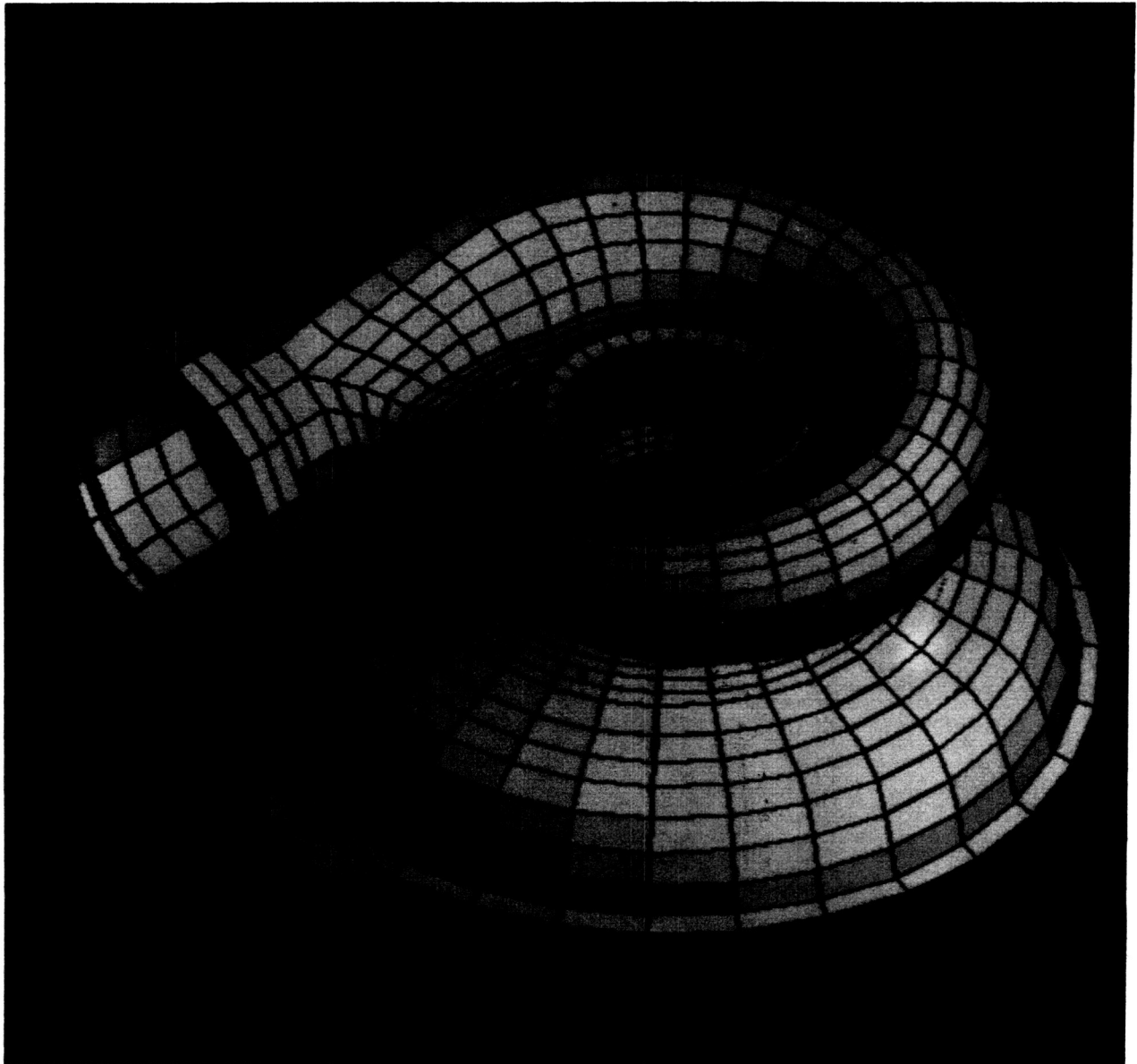


Figure 2 HPFTP Inlet Housing - DIAL Global Finite Element Model

SSME HPFTP 3-D FINITE ELEMENT MODEL

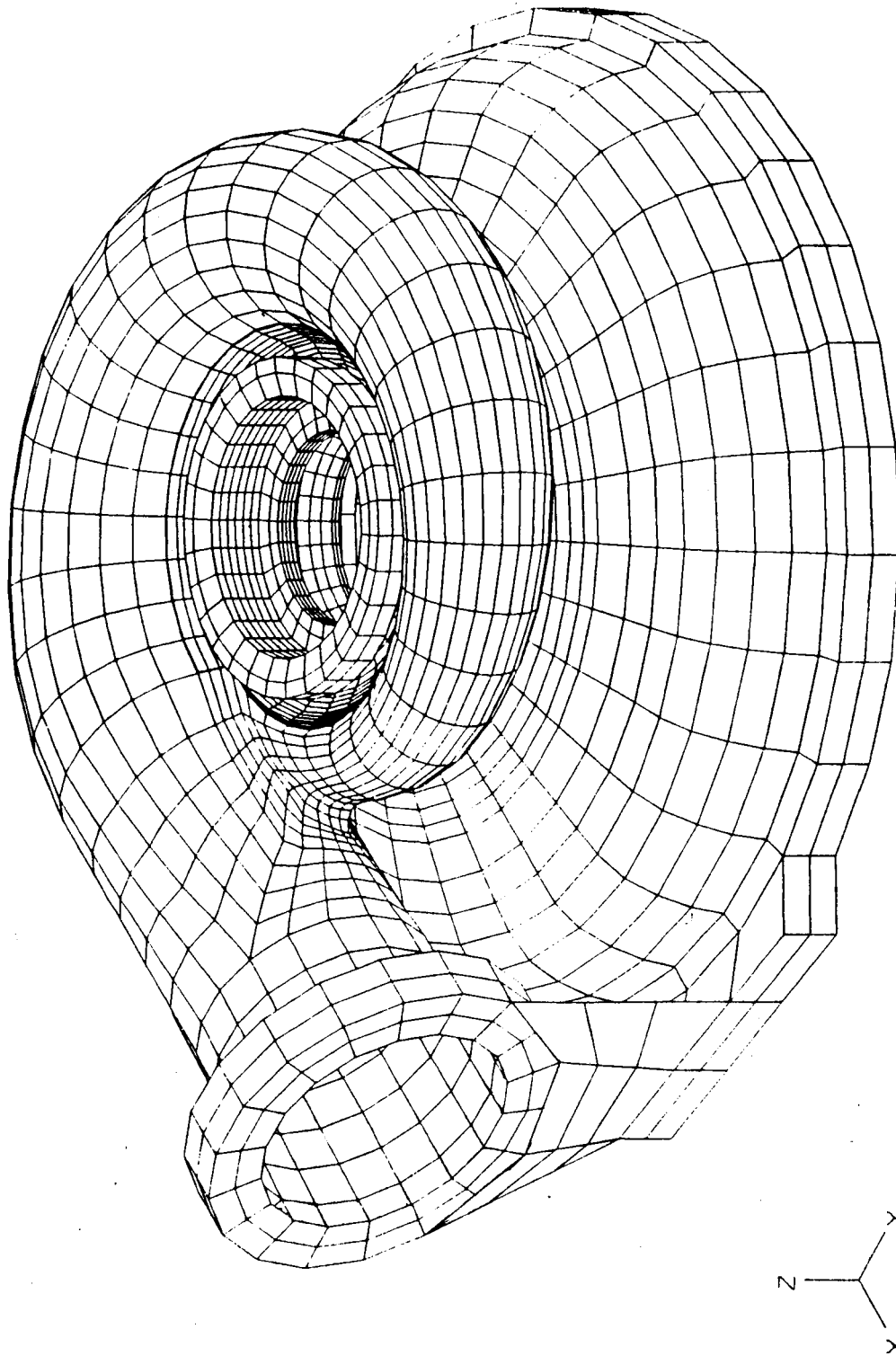


Figure 3 HPFTP Inlet Housing - DIAL Global Finite Element Model
(Looking from Pump Toward Turbine)

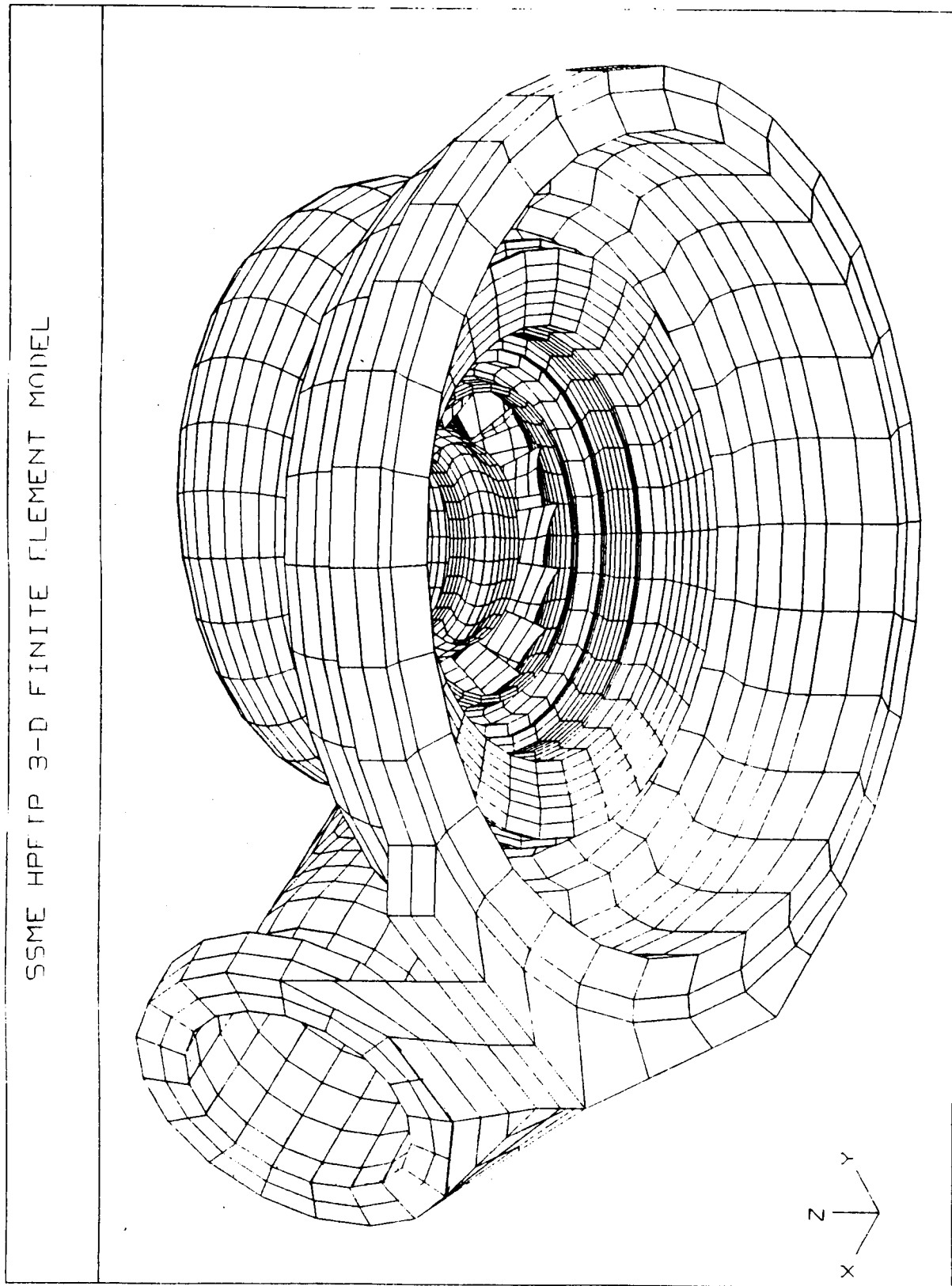
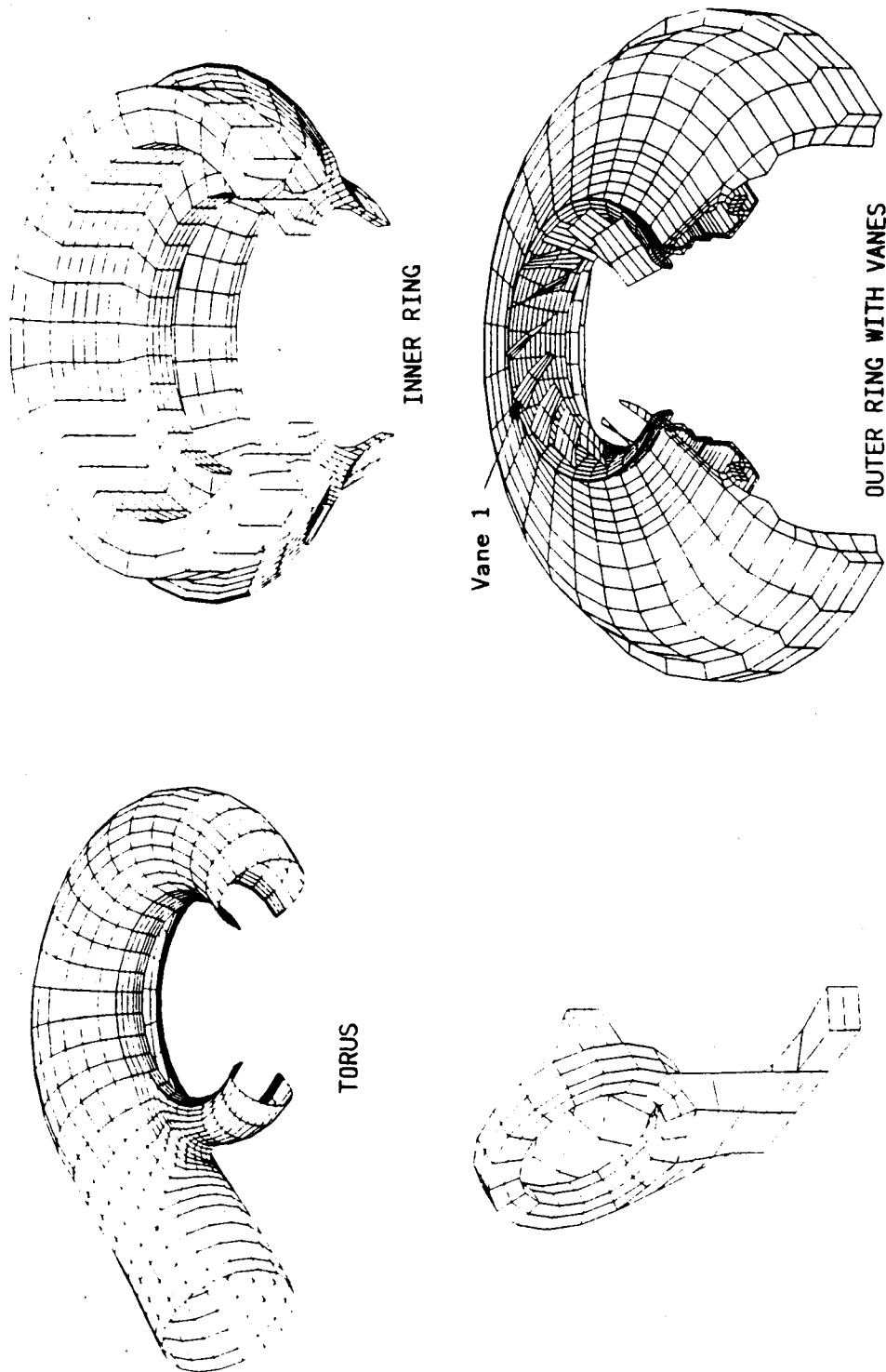


Figure 4 HPFTP Inlet Housing - DIAL Global Finite Element Model
(Looking from Turbine Toward Pump)

MSD

HPFTP INLET HOUSING

3D GLOBAL MODEL



 **Lockheed**
Missiles & Space Company, Inc.

Figure 5 HPFTP Inlet Housing - DIAL Global Finite Element Model
Exploded View Showing Model Components

TYPICAL SHELL/SOLID INTERFACE

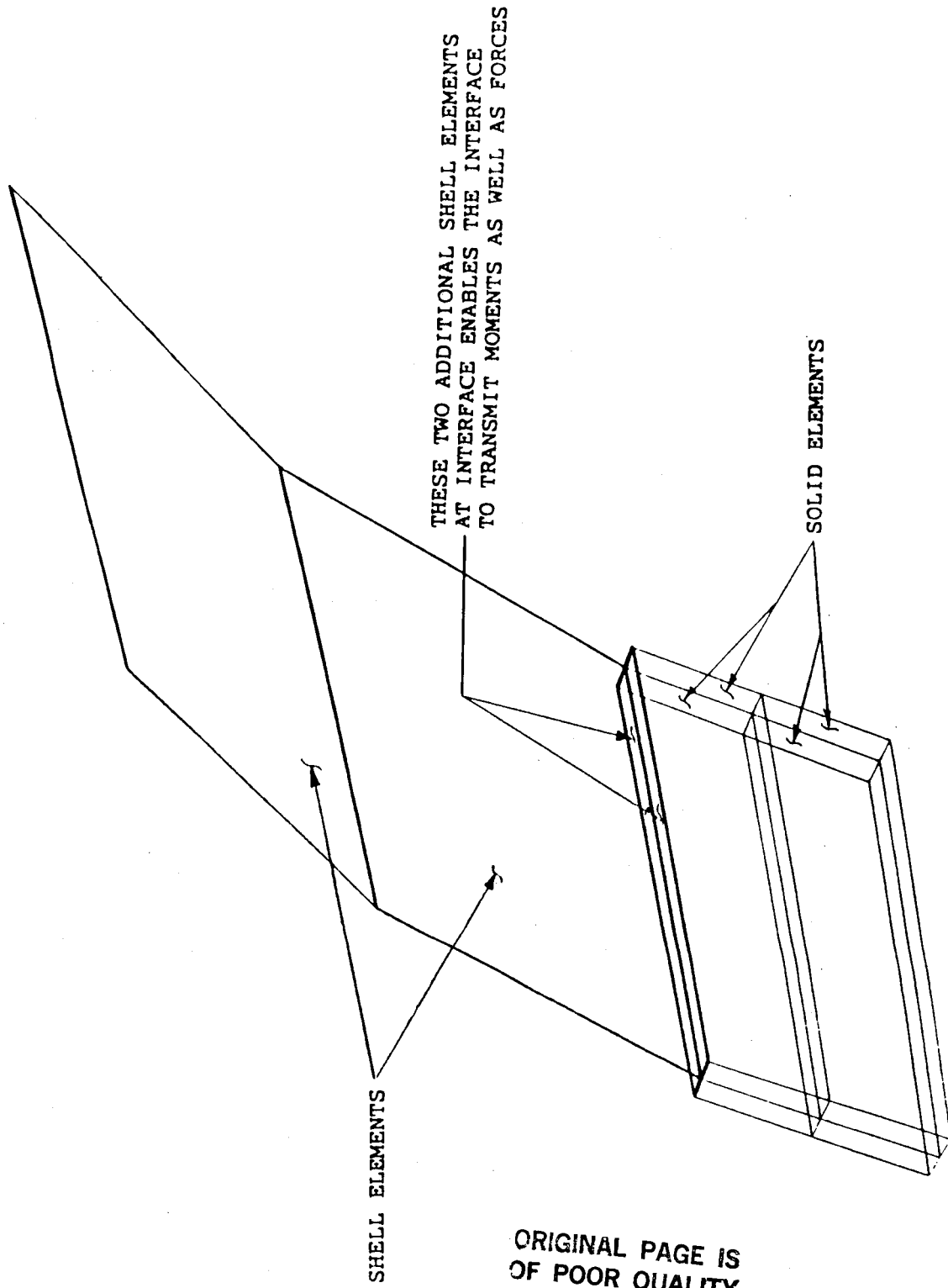


Figure 6 HPFTP Inlet Housing - DIAL Global Finite Element Model
Shell/Solid Element Interface (in Torus)

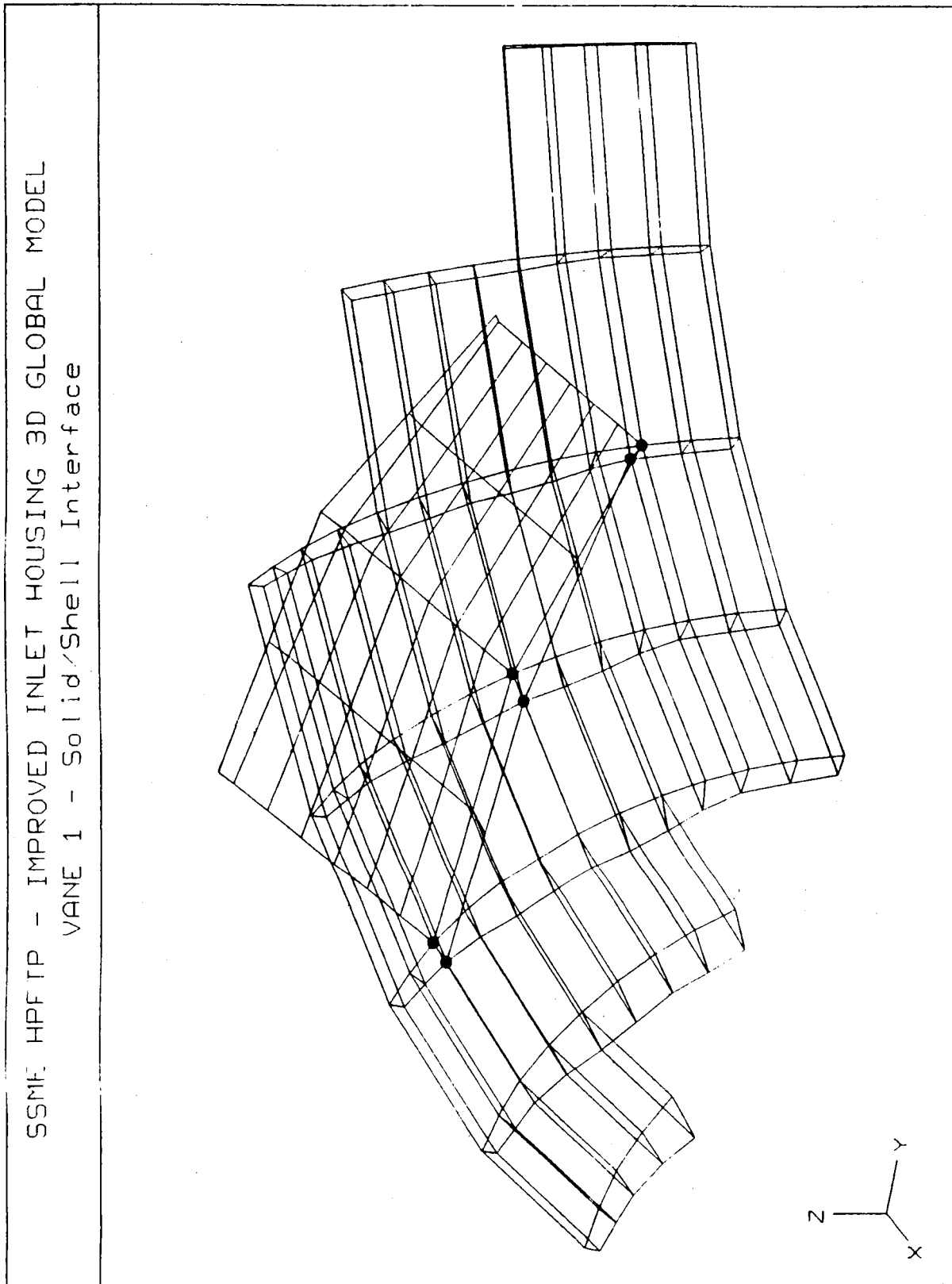


Figure 7 HPFTP Inlet Housing - DIAL Global Finite Element Model
Typical Shell Element Vane/Solid Element Connection

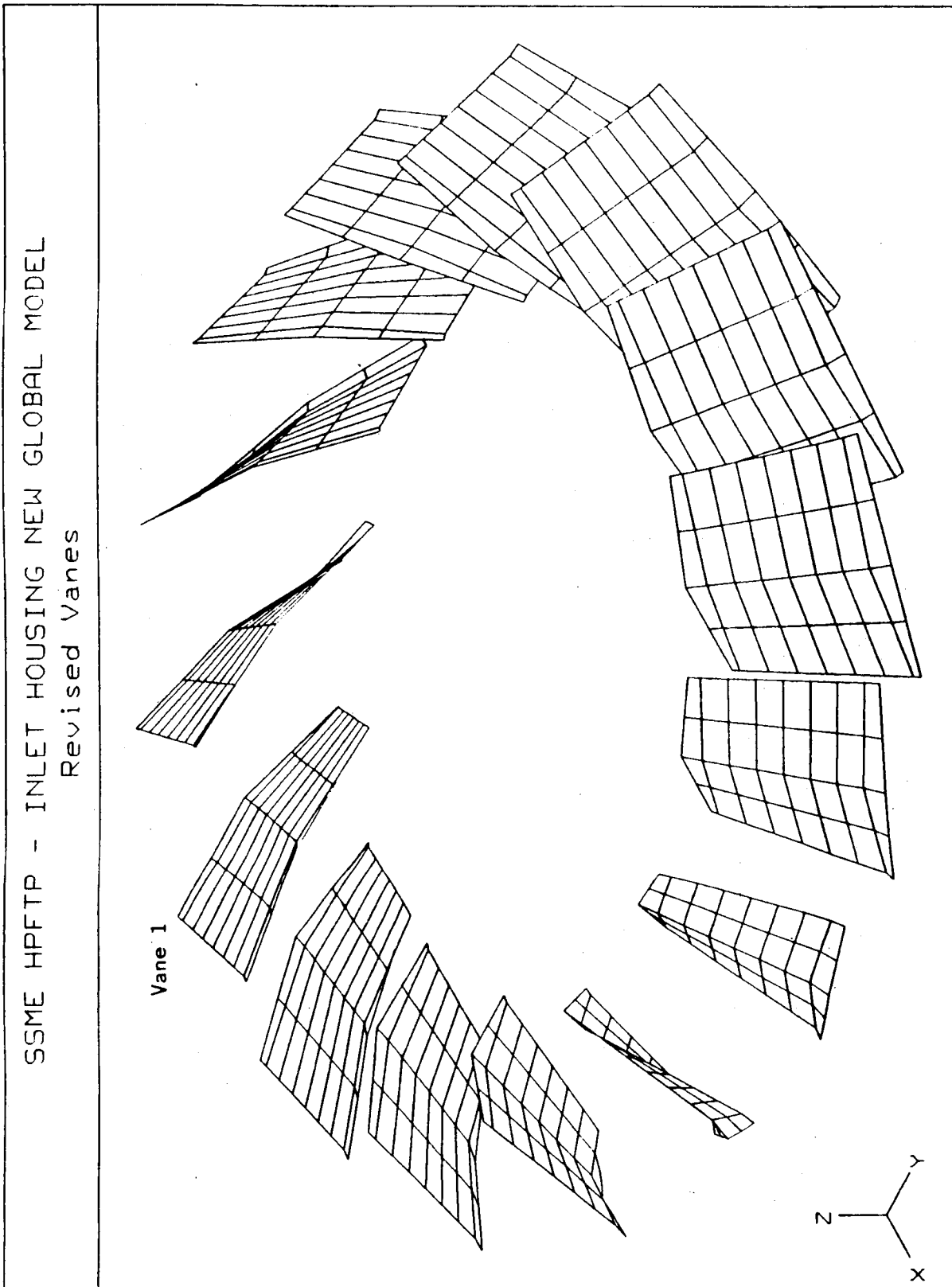


Figure 8 HPFTP Inlet Housing - DIAL Global Finite Element Model
Final Configuration of Shell Element Vanes

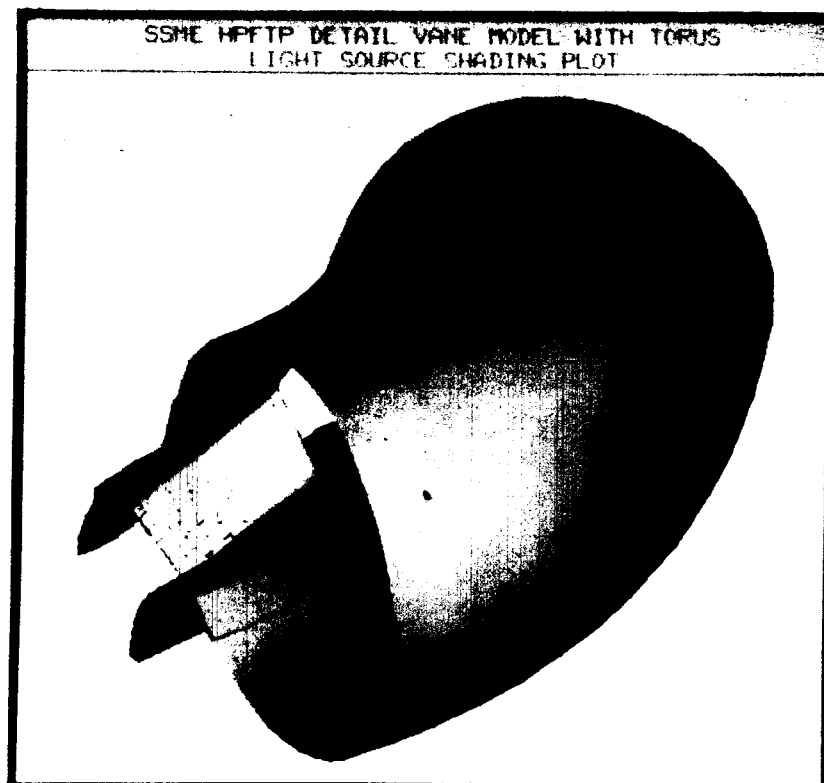
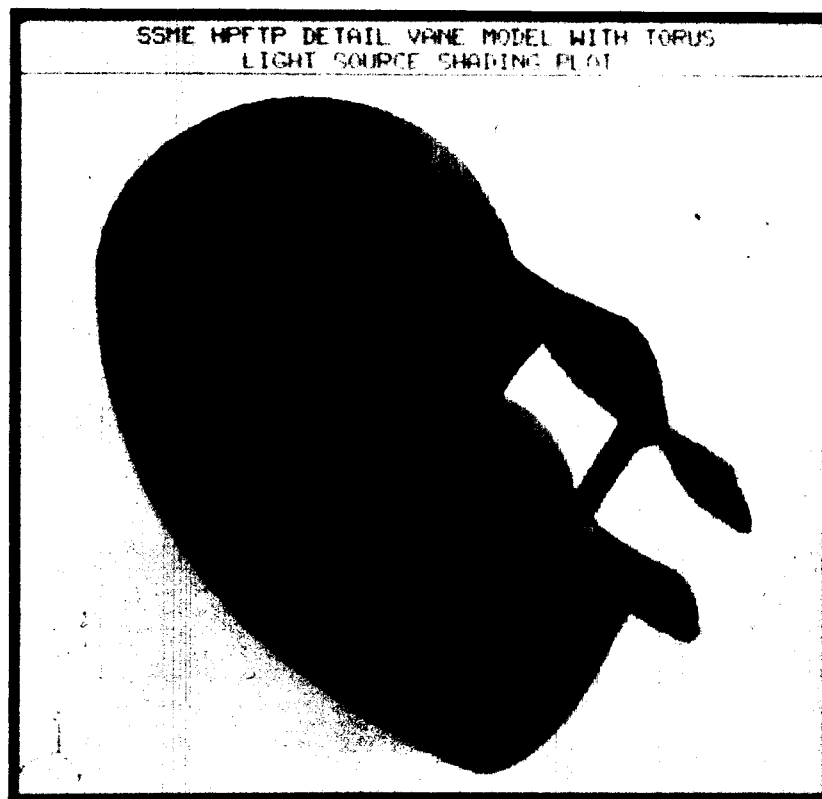


Figure 9(a,b) HPFTP Inlet Housing - DIAL Detailed Vane Submodel
(Color Light Source Shading Plot)

V2PLT1

NEW DETAILED VANE MODEL

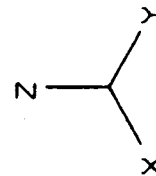
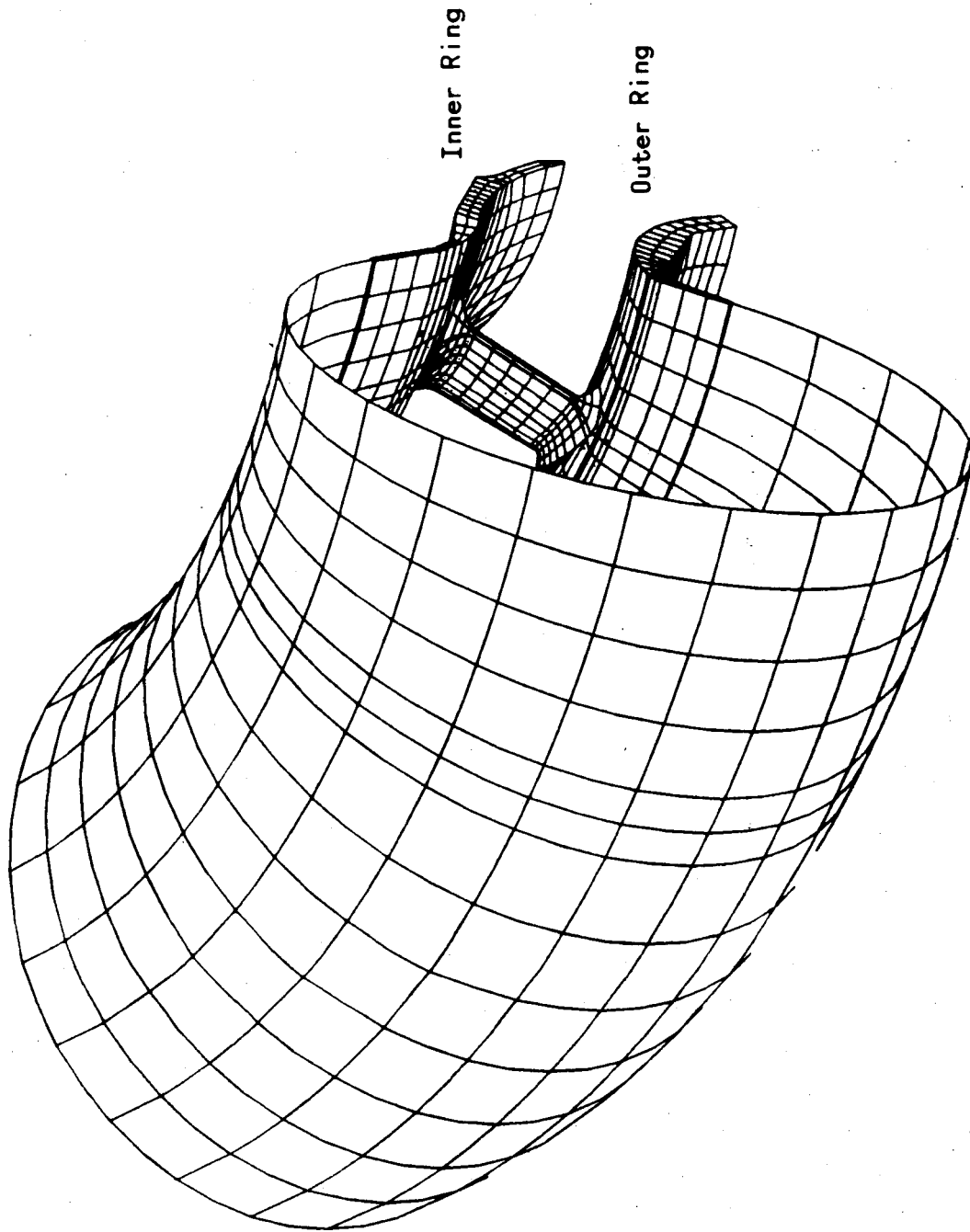


Figure 10 HPFTP Inlet Housing - DIAL Detailed Vane Submodel
(Looking from Larger End of Torus Toward Smaller End)

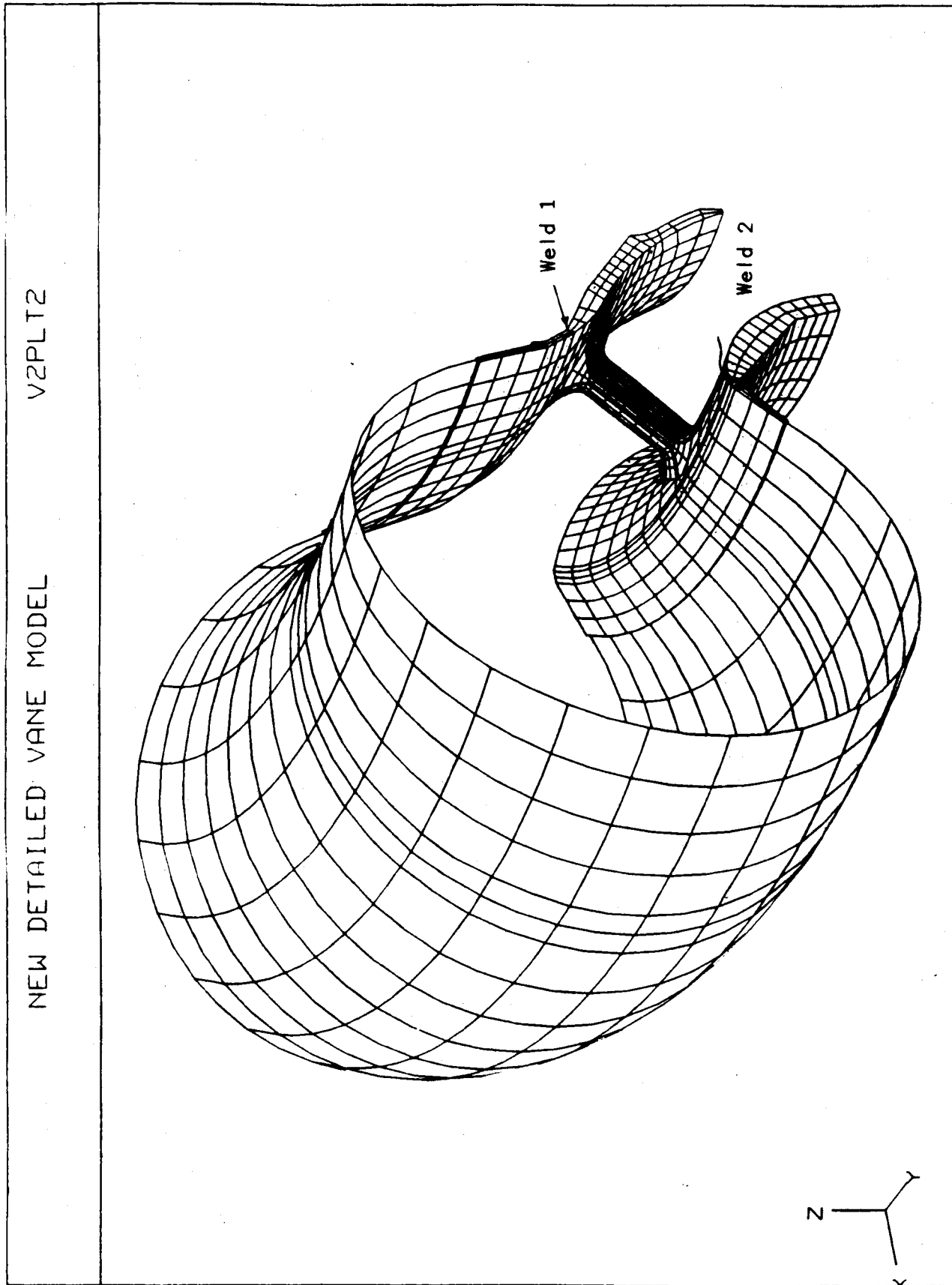


Figure 11 HPFTP Inlet Housing - DIAL Detailed Vane Submodel
(Looking from Larger End of Torus Toward Smaller End)

SSMF HPFIP - INFL HOUSING
FULL POWER LEVEL (FPL) LOADING

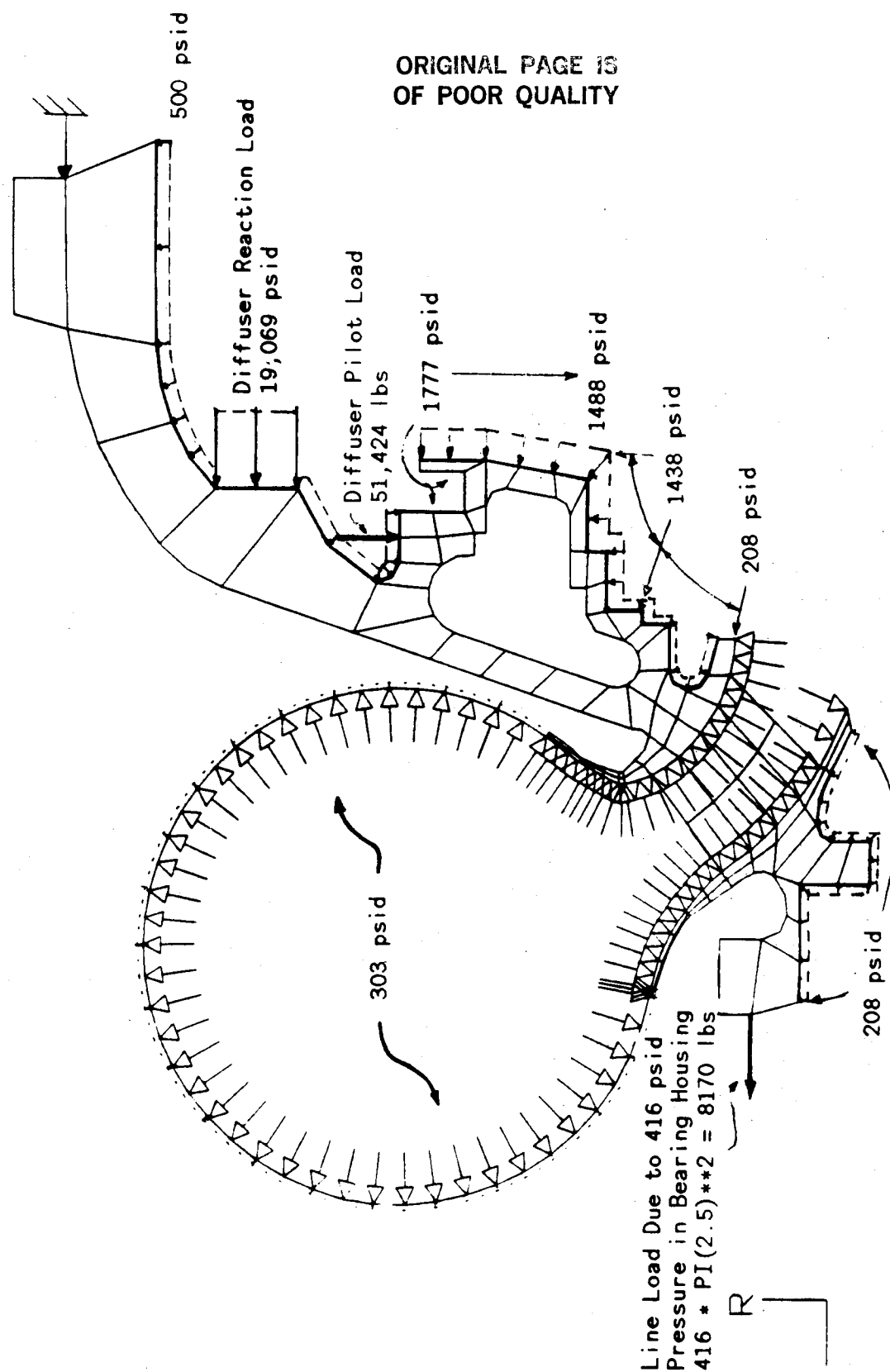


Figure 12 HPFTP Inlet Housing - Applied FPL Loading

ORIGINAL PAGE IS
OF POOR QUALITY

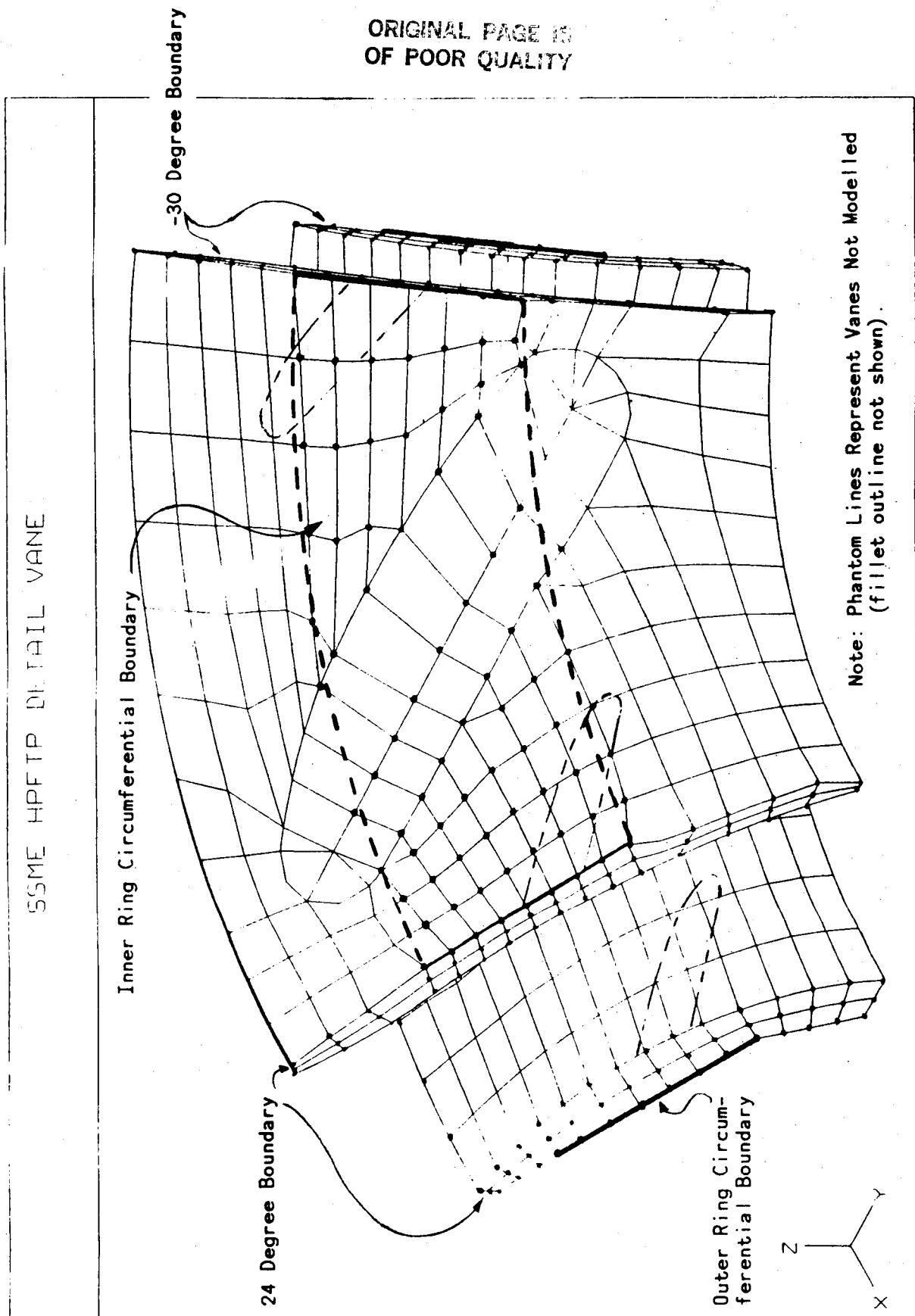


Figure 13 HPFTP Inlet Housing - DIAL Detailed Vane Submodel
Applied Displacement Boundaries (from Global Model)
(Torus Removed for Clarity)

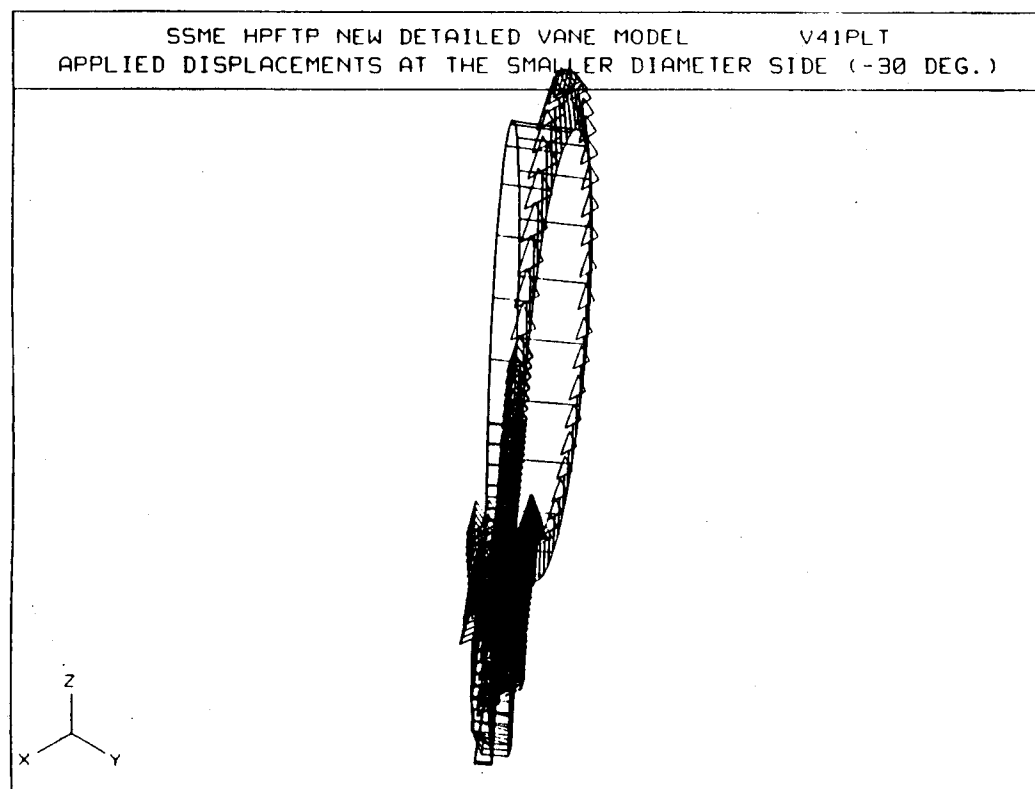
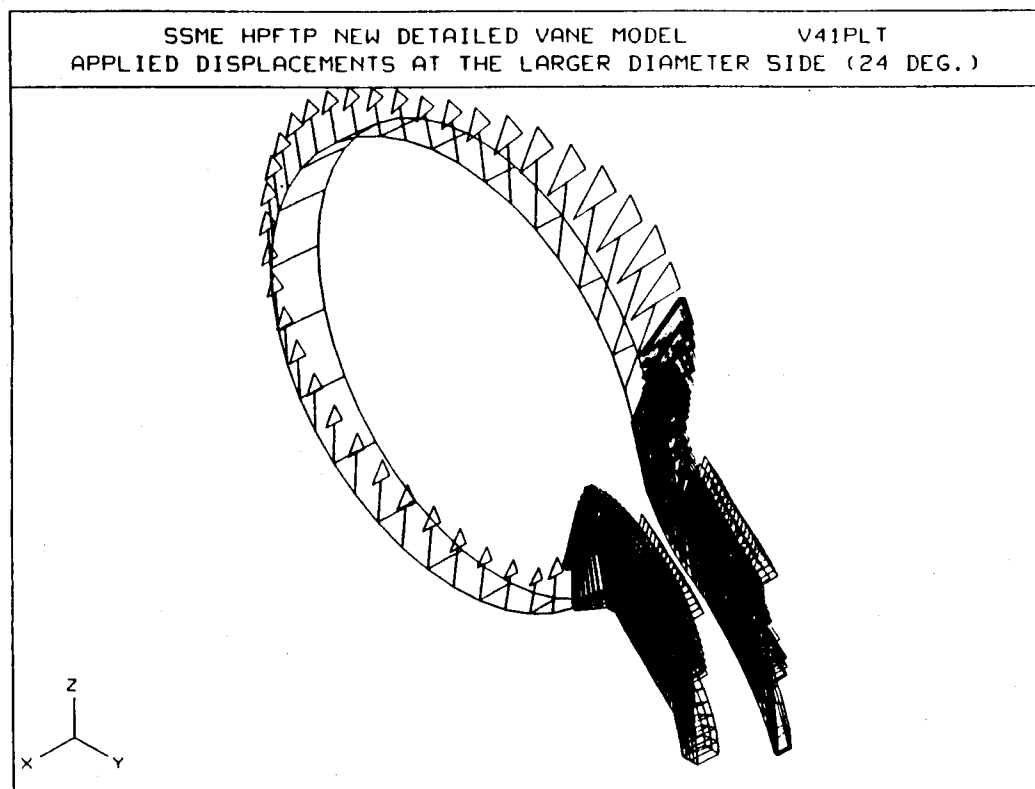


Figure 14(a,b) HPFTP Inlet Housing - DIAL Detailed Vane Submodel
Applied Displacement Vectors from Global Model (Torus)



MATERIALS PROPERTIES MANUAL

TYPICAL (PREDICTED)

1700F AIR 3HRS/1400F VACUUM 4HRS

DATE-07-07-87

REFERENCE-5002-09

3RD EDITION PAGE-5002.27.10.50-01

5002.27.10.50-01A

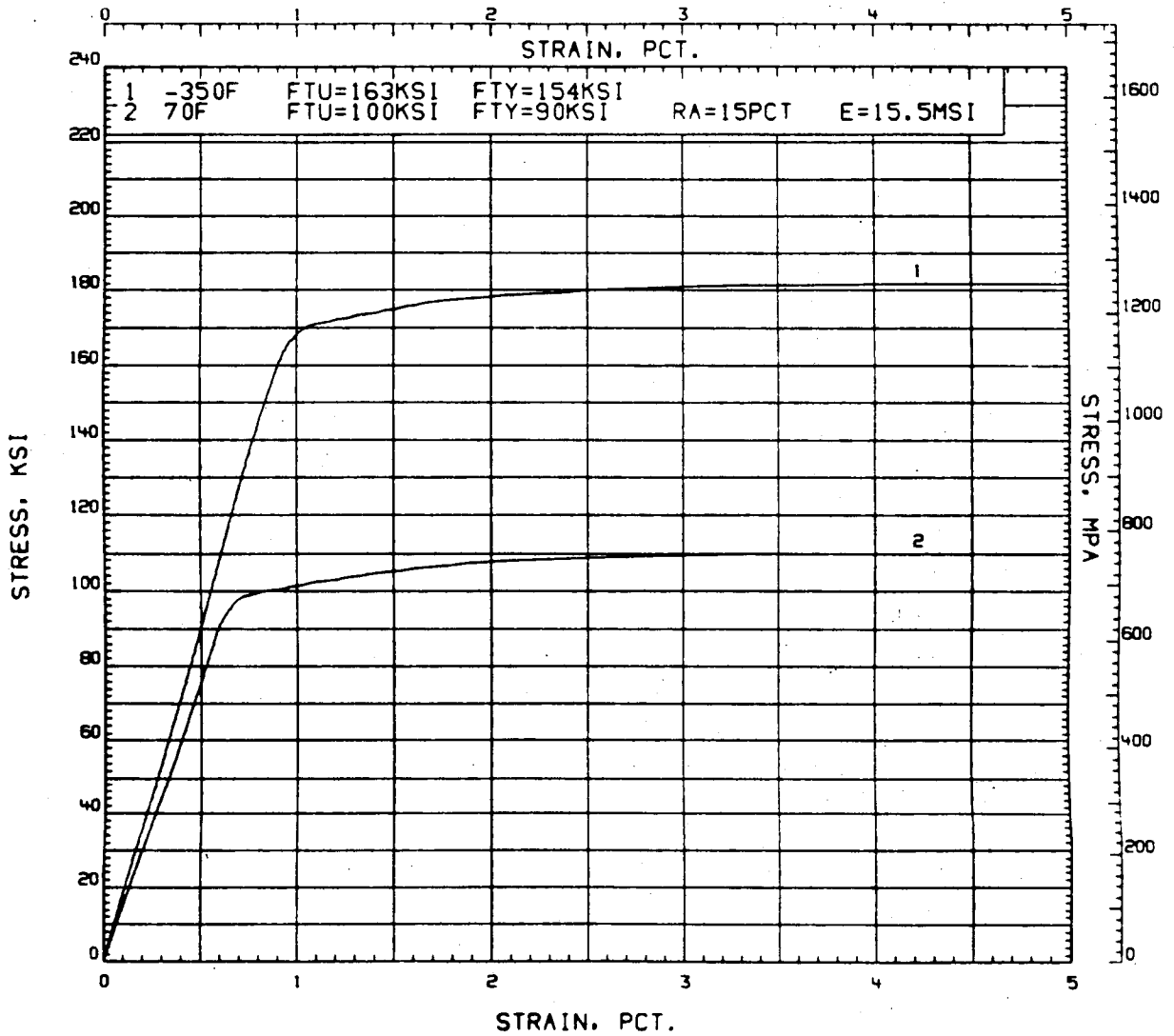
TI-5AL-2.5SN ELI

STRESS-STRAIN DIAGRAM

WROUGHT, CONVENTIONAL

ANNEALED

SPEC R80170-079.152



4th Edition

10-30-87

Figure 15 Rocketdyne Materials Properties Manual - Ti-5Al-2.5Sn (ELI)
Stress/Strain Curve (Typical Values)



MATERIALS PROPERTIES MANUAL

PREDICTED MINIMUM AXIAL R=-1.0

1700F AIR 3HRS/1400F VACUUM 4HRS

CHEM MILLED

LT. 4IN SECTION THICKNESS

DATE-9-1-77

REFERENCE-5002-09

3RD EDITION PAGE-5002.33.10.50-02

5002.33.10.50-02

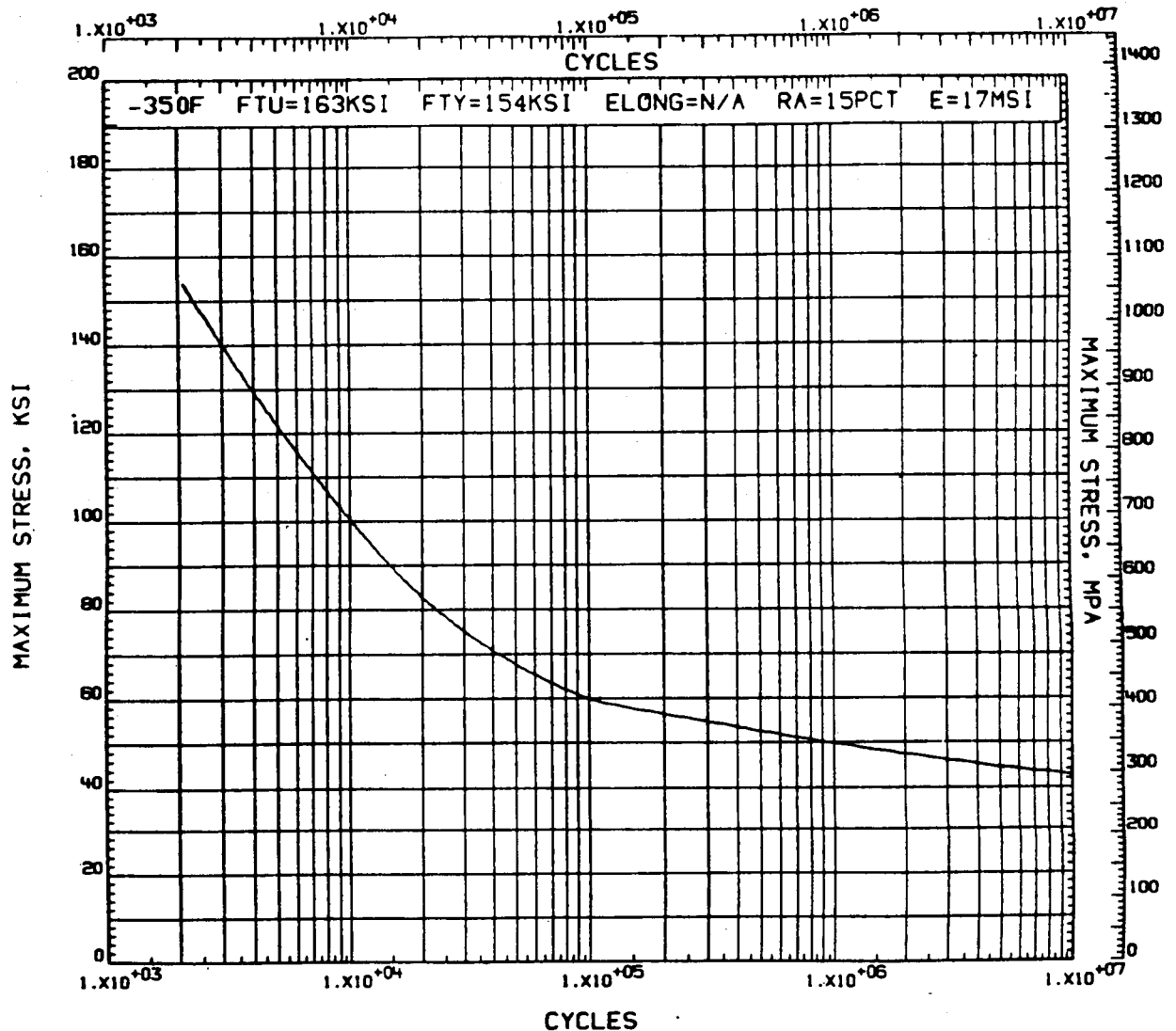
TI-5AL-2.5SN ELI

HIGH CYCLE FATIGUE

WROUGHT, CONVENTIONAL

ANNEALED

SPEC RB0170-079.152



4th Edition

10-30-87

Figure 16 Rocketdyne Materials Properties Manual - Ti-5Al-2.5Sn (ELI)
Stress vs Number of Cycles to Failure (S/N) Curve (R = -1.0)



MATERIALS PROPERTIES MANUAL

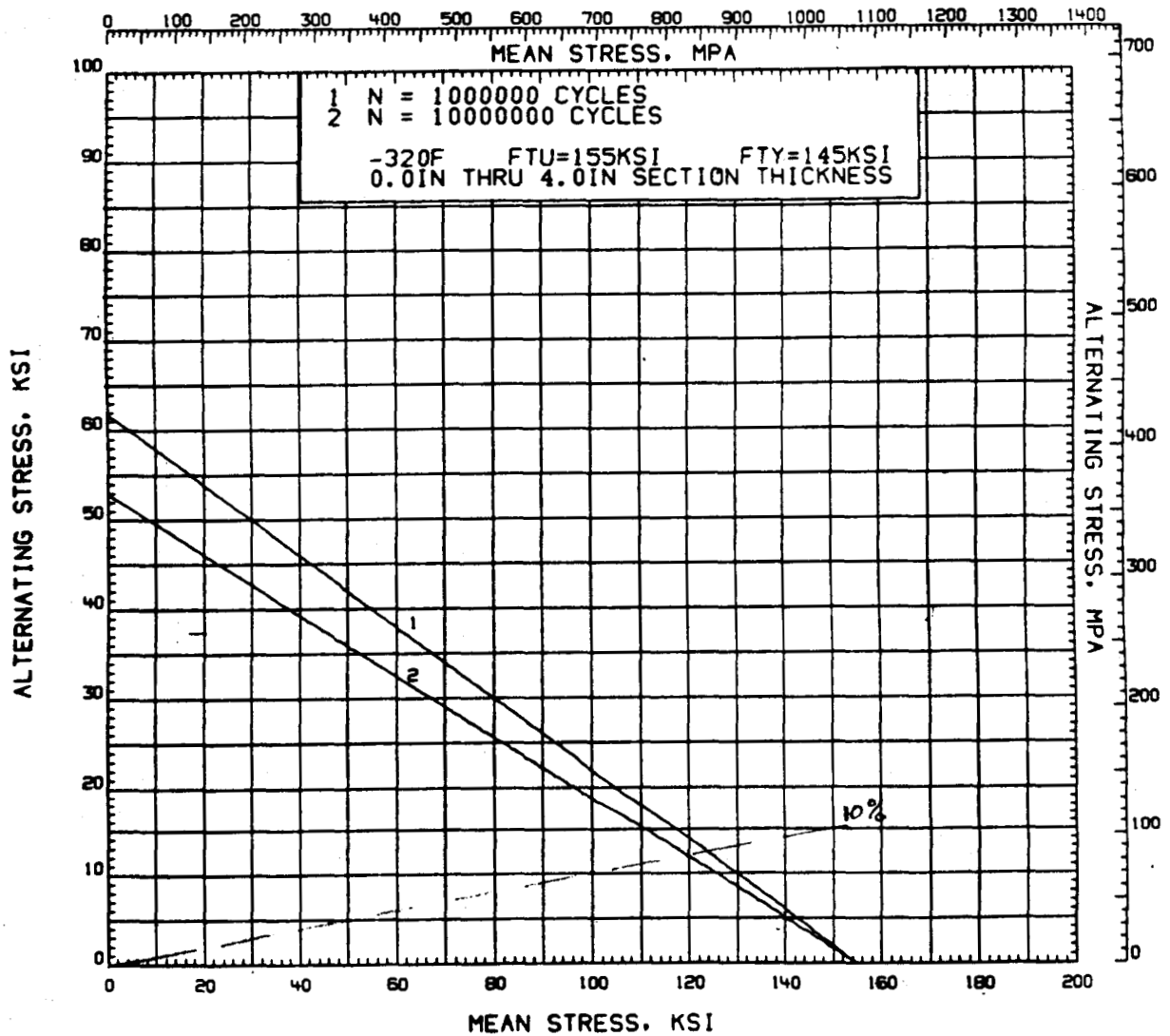
EXPECTED MINIMUM
AXIAL
MACHINED 32 FINISH
1700F AIR 3HRS/1400F VACUUM 4HRS

DATE-9-1-77
REFERENCE-5002-04 (MFR 9-176A-123)
3RD EDITION PAGE-5002.33.12.50-02

5002.33A.12.50-02

TI-5AL-2.5SN ELI
MODIFIED GOODMAN DIAGRAM
BAR OR FORGING
ANNEALED

SPEC RB0170-079.152



4th Edition
10-30-87

Figure 17 Rocketdyne Materials Properties Manual - Ti-5Al-2.5Sn (ELI)
Modified Goodman Diagram (Machined Surface Finish)



MATERIALS PROPERTIES MANUAL

PREDICTED MINIMUM

MUS/3

1700F AIR 3HRS/1400F VACUUM 4HRS

DATE-9-1-77

REFERENCE-5002-09

3RD EDITION PAGE-5002.34.10.50-01

5002.34.10.50-01

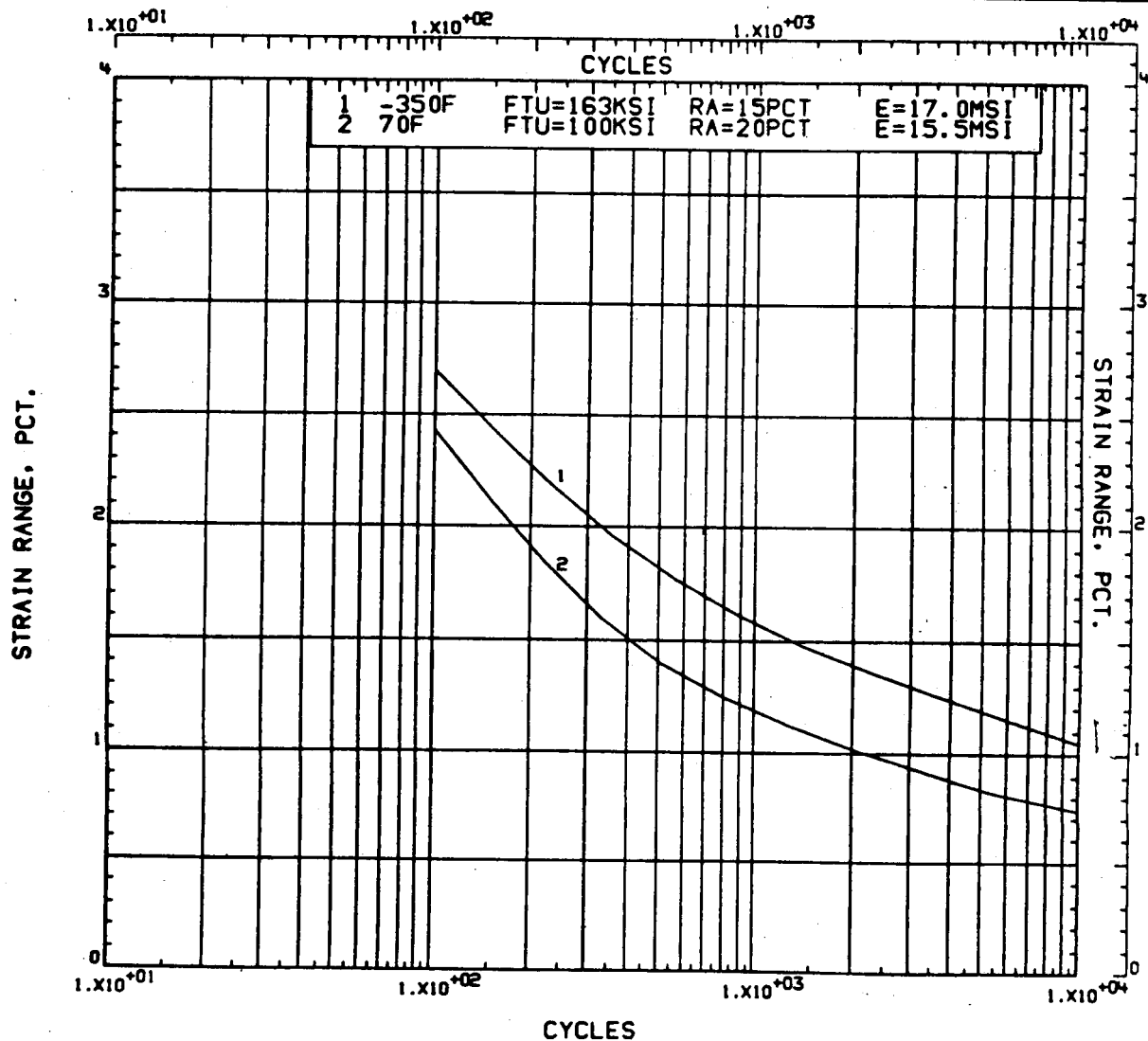
TI-5AL-2.5SN ELI

LOW CYCLE FATIGUE

WROUGHT, CONVENTIONAL

ANNEALED

SPEC RB0170-079.152



4th Edition

10-30-87

Figure 18 Rocketdyne Materials Properties Manual - Ti-5Al-2.5Sn (ELI)
Low Cycle Fatigue - Plastic Strain vs Number (R = -1.0))

SSME HPFTP - IMPROVED INLET HOUSING 3D GLOBAL MODEL
STRESS CONTOUR PLOT - 0 TO 144 DEG - INNER RING

DIAL L3D3

CONTOUR PLOT
EFFECTIVE
STRESS

INDEX VALUES
1 0.100E+05
2 0.200E+05
3 0.300E+05
4 0.400E+05
5 0.500E+05
6 0.600E+05
7 0.700E+05
8 0.800E+05

MIN= 0.1138E+04
MAX= 0.8529E+05 *

(*) Max Stress Weld 1

(+) Max Stress Inner Ring

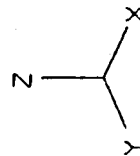
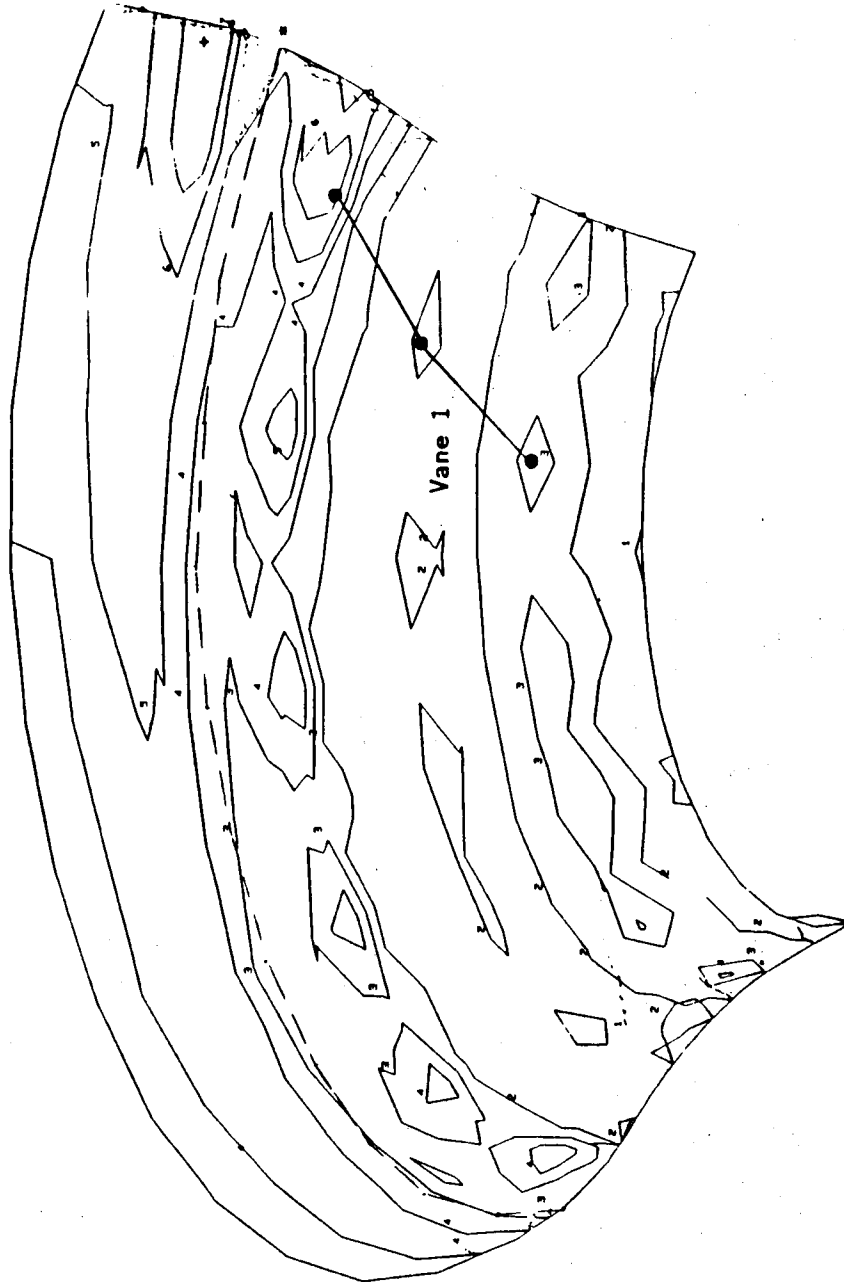


Figure 19. HPFTP Inlet Housing - Global Model - Effective Stress
Contour Plot of the Inner Ring Due to FPL Loading.

Figure 19 HPFTP Inlet Housing - Global Model - Effective Stress
Contours Plot of the Inner Ring Due to FPL Loading

SSME HPFTP - IMPROVED INLET HOUSING 3D GLOBAL MODEL
STRESS CONTOUR PLOT FROM 0 TO 144 DEGREES - OUTER RING

DIAL L3D3

CONTOUR PLOT
EFFECTIVE
STRESS

INDEX	VALUES
1	0.200E+05
2	0.250E+05
3	0.300E+05
4	0.350E+05
5	0.400E+05
6	0.450E+05
7	0.500E+05
8	0.550E+05
9	0.600E+05
0	0.650E+05
A	0.700E+05
B	0.750E+05
C	0.800E+05
D	0.850E+05
E	0.900E+05

MIN= 0.1886E+05
MAX= 0.9064E+05 *

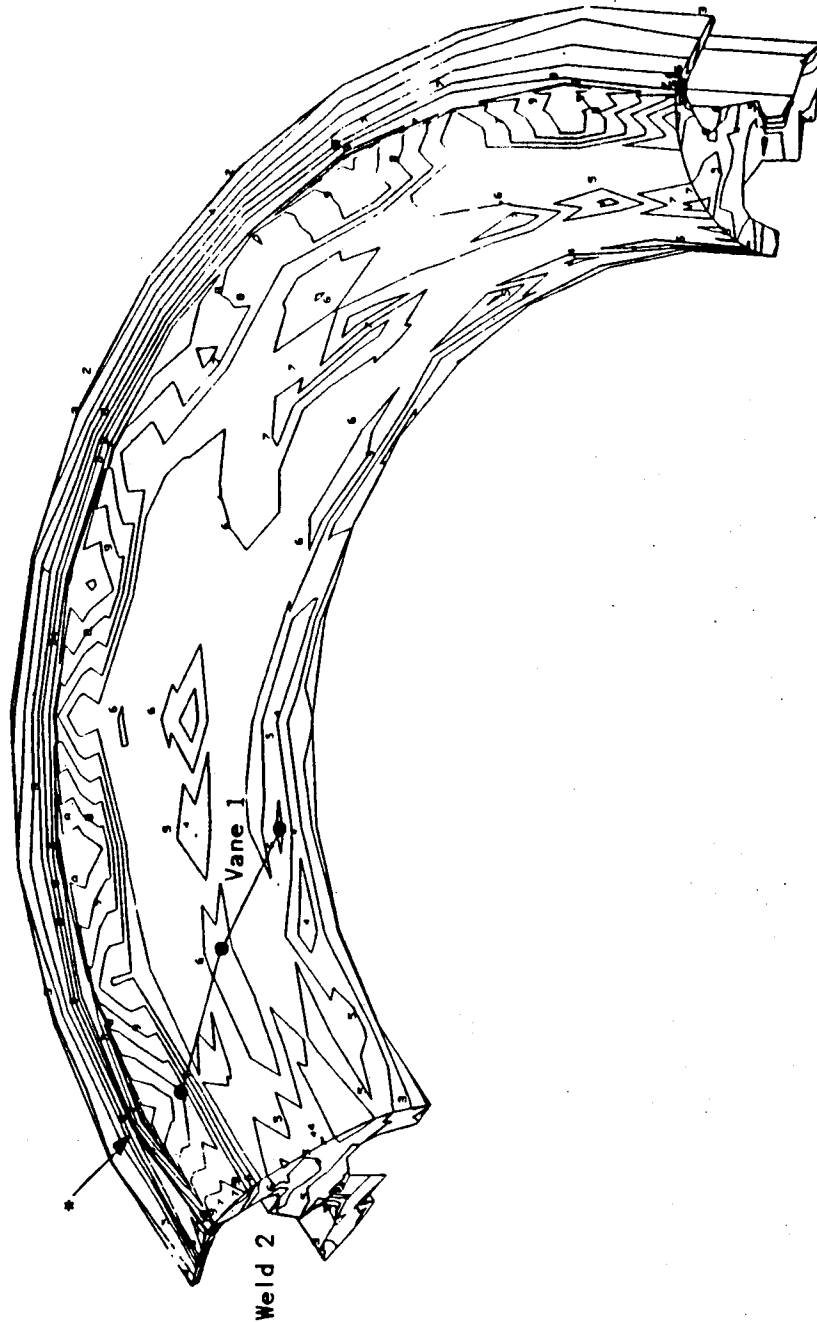


Figure 20 HPFTP Inlet Housing - Global Model - Effective Stress
Contour Plot of the Outer Ring Due to FPL Loading

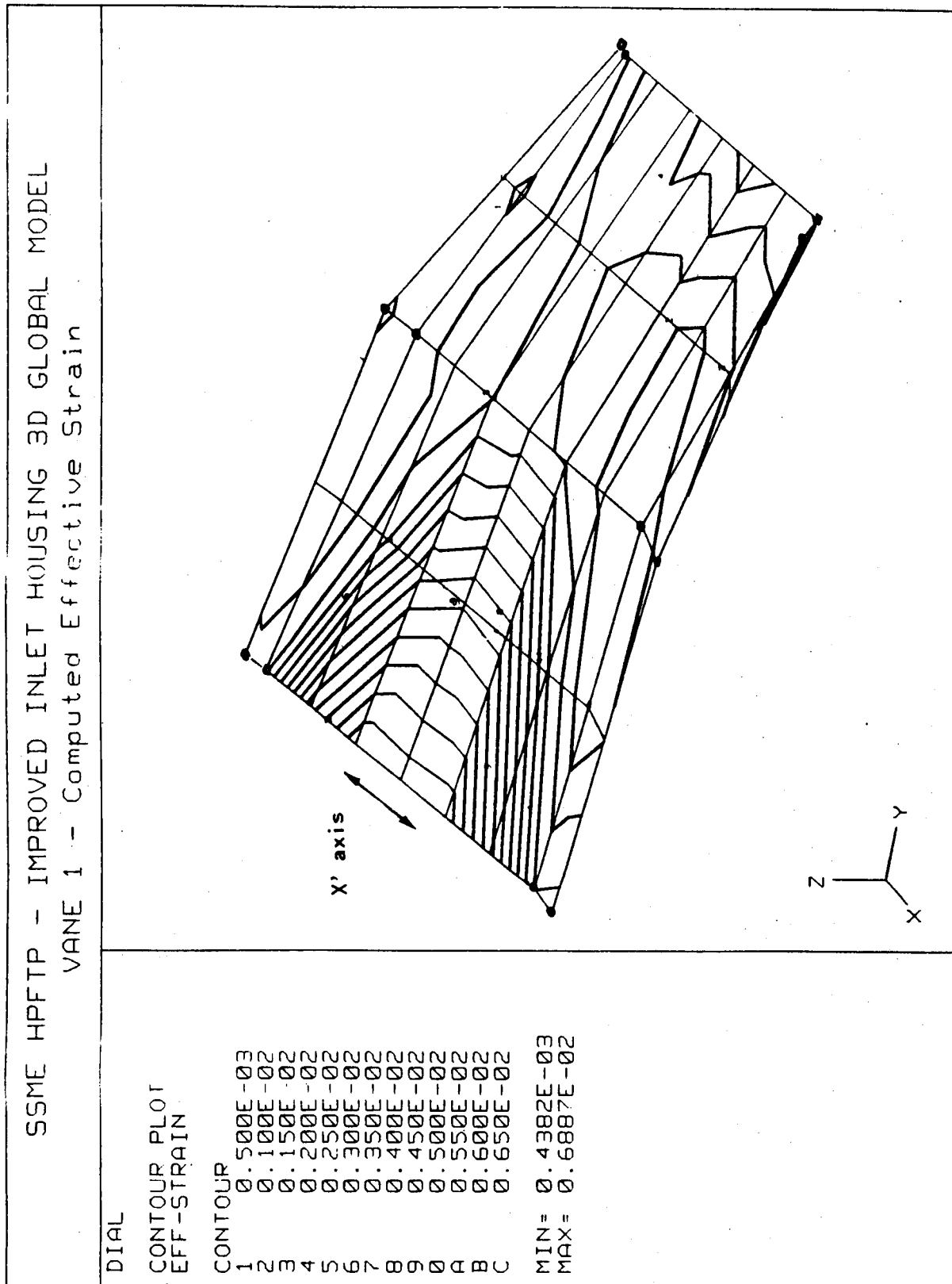
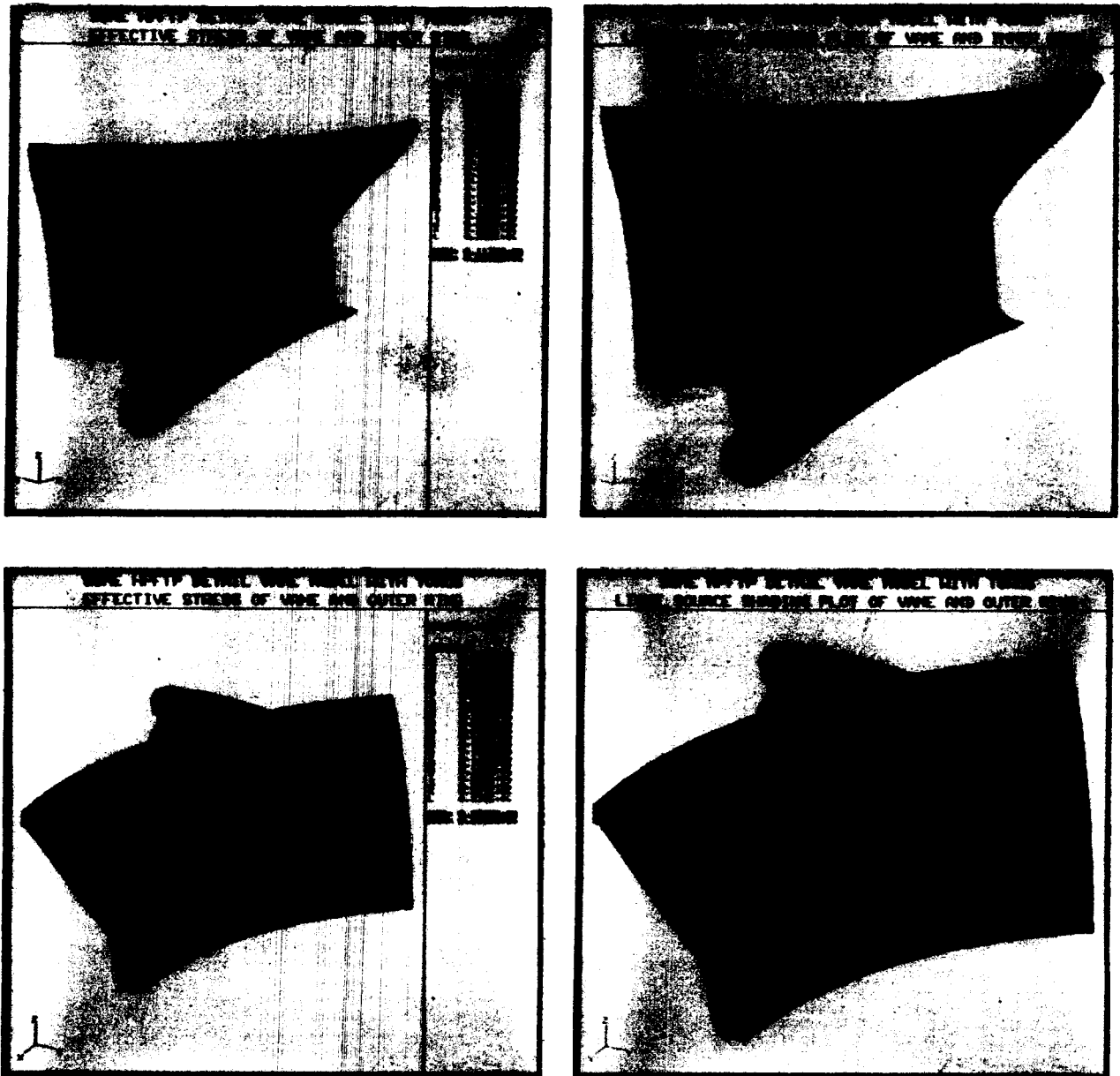


Figure 21 HPFTP Inlet Housing - Global Model - Effective Stress
Contour Plot of Vane 1 (at Max Torus Radius) at FPL

ORIGINAL PAGE
COLOR PHOTOGRAPH



ORIGINAL PAGE
COLOR PHOTOGRAPH

Figure 22 HPFTP Inlet Housing - Detailed Vane Submodel - Effective Stress Color Contour Plot of Vane and Ring Intersections

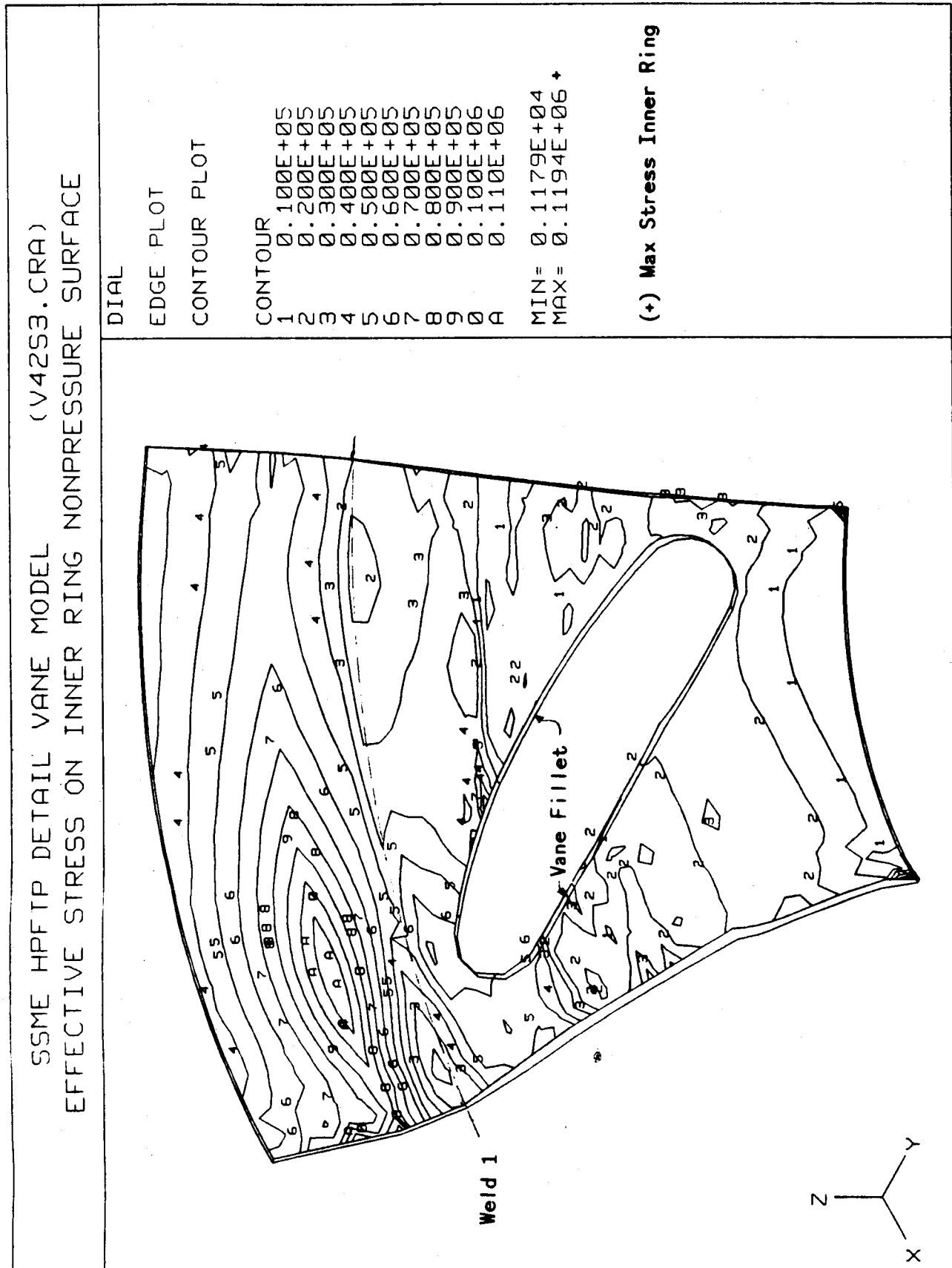


Figure 23 HPFTP Inlet Housing - Detailed Vane Submodel - Effective Stress Contour Plot of Inner Ring Non-Pressure Surface

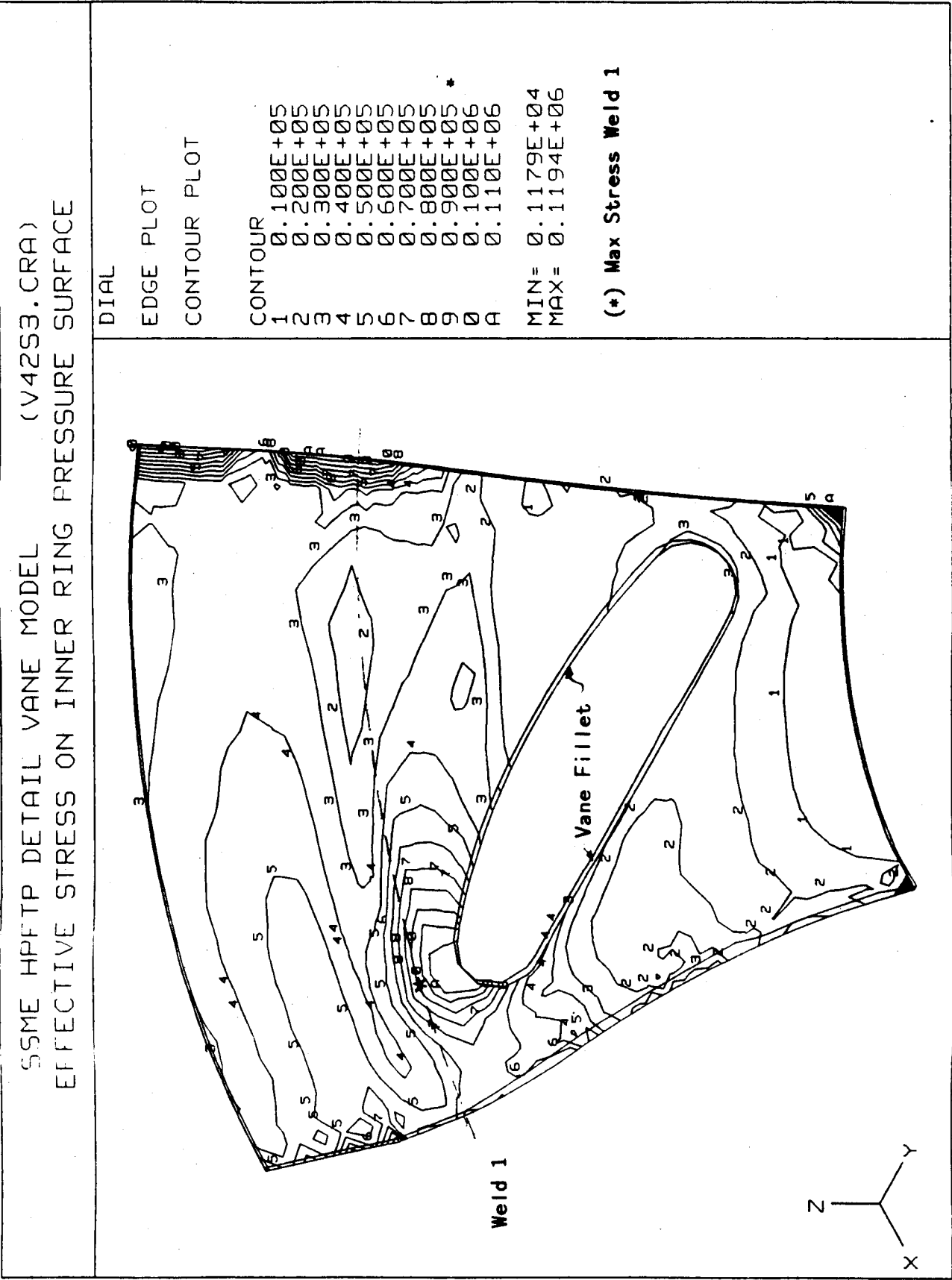


Figure 24 HPFTP Inlet Housing - Detailed Vane Submodel - Effective Stress Contour Plot of Inner Ring Pressure Surface

SSME HPFTP DETAIL VANE MODEL (V42S3.CRA)
EFFECTIVE STRESS ON OUTER RING PRESSURE SURFACE

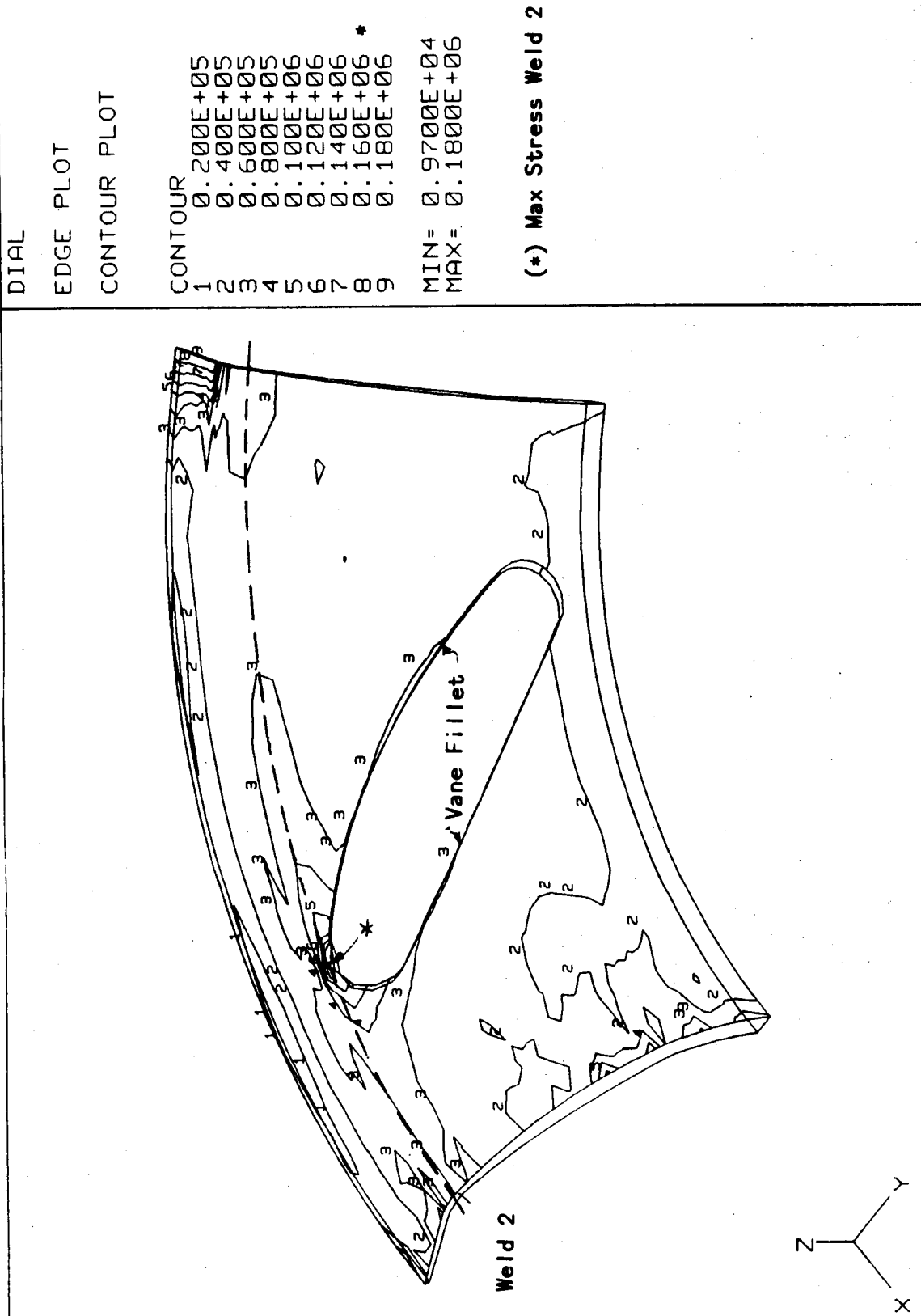


Figure 25 HPFTP Inlet Housing - Detailed Vane Submodel - Effective Stress Contour Plot of Outer Ring Pressure Surface

SSME HPFTP DETAIL VANE MODEL (V42S1.PRF)
EFFECTIVE STRESS ON VANE BOTTOM SURFACE

DIAL
HIDDEN LINE PLOT
CONTOUR PLOT
CONTOUR
1 0.200E+05
2 0.400E+05
3 0.600E+05
4 0.800E+05
5 0.100E+06
6 0.120E+06
7 0.140E+06
8 0.160E+06
9 0.180E+06
0 0.200E+06
A 0.220E+06
MIN= 0.2337E+04
MAX= 0.2365E+06 *

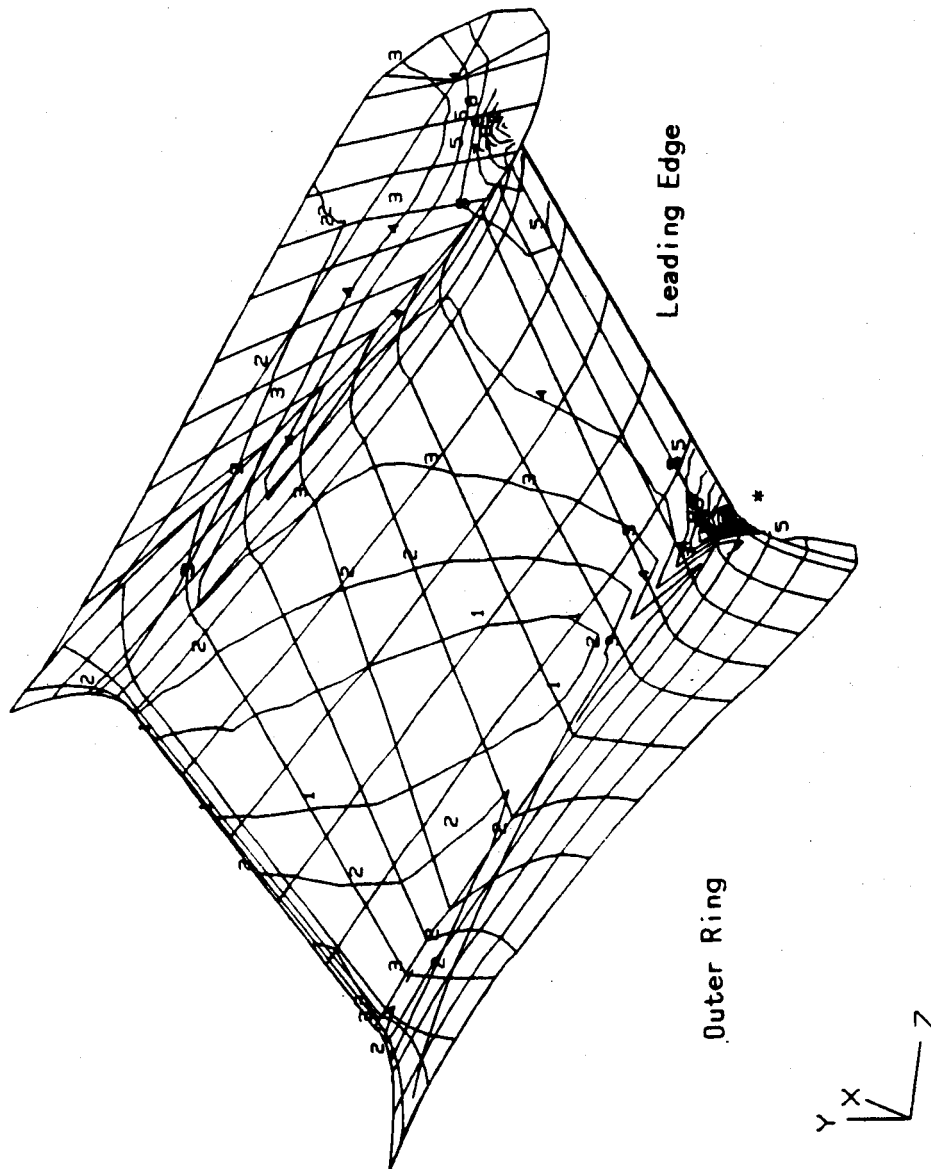


Figure 26 HPFTP Inlet Housing - Detailed Vane Submodel - Effective
Stress Contour Plot of Vane and Fillet

SSME HPFTP DETAIL VANE MODEL (V42S2.CRA)
EFFECTIVE STRAIN ON VANE BOTTOM SURFACE

DIAL
HIDDEN LINE PLOT
CONTOUR PLOT
CONTOUR
1 0.100E-02
2 0.200E-02
3 0.300E-02
4 0.400E-02
5 0.500E-02
6 0.600E-02
7 0.700E-02
8 0.800E-02
9 0.900E-02
0 1.00E-01
A 0.110E-01
B 0.120E-01
C 0.130E-01
MIN= 0.1357E-03
MAX= 0.1373E-01 *

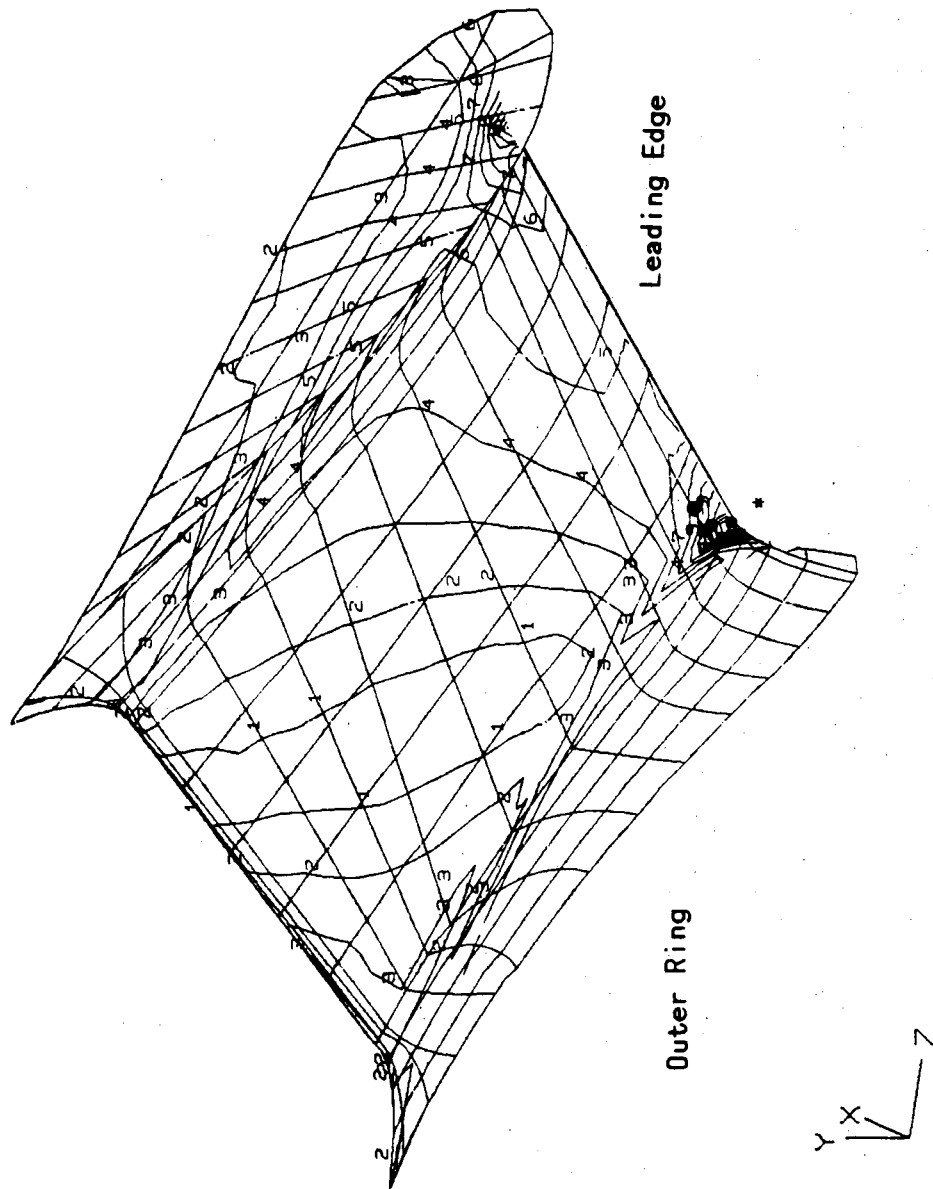


Figure 27 HPFTP Inlet Housing - Detailed Vane Submodel - Effective Strain Contour Plot of Vane and Fillet

Appendix A

FINAL GLOBAL HPFTP INLET HOUSING
DIAL FINITE ELEMENT MODEL RUNSTREAM

```

FETCH, DN=MESH, DF=TR, TEXT='DISKB: [FERGUSON.CEXL3D2] MESH.CEX'.
MESH.
FETCH, DN=BAND, DF=TR, TEXT='DISKB: [FERGUSON.CEXL3D2] BAND.CEX'.
BAND.
FETCH, DN=SETUP, DF=TR, TEXT='DIAL$CRAY: SETUP.CEX'.
SETUP.
FETCH, DN=MATL, DF=TR, TEXT='DISKB: [FERGUSON.CEXL3D2] MATL.CEX'.
MATL.
FETCH, DN=LOAD, DF=TR, TEXT='DISKB: [FERGUSON.CEXL3D2] LOAD.CEX'.
LOAD.
FETCH, DN=SOLVE, DF=TR, TEXT='DISKB: [FERGUSON.CEXL3D2] SOLVE.CEX'.
SOLVE.
FETCH, DN=SCOPE, DF=TR, TEXT='DISKB: [FERGUSON.CEXL3D2] SCOPE.CEX'.
SCOPE.
DISPOSE, DN=FT10, TEXT='DISK6: [KPOOL] FOR010.DAT'.
FETCH, DN=UTILITY, DF=TR, TEXT='DISKB: [FERGUSON.CEXL3D2] UTILITY.CEX'.
UTILITY.
DISPOSE, DN=BCD1, DF=BB, TEXT='DISK6: [KPOOL] HYBRID5.PUN'.
BAD.
EXIT.
SAVE, DN=FILO02, PDN=HPFTP, ID=KPOOL, NA.
DISPOSE, DN=FILO02, DF=TR, TEXT='HPFTP-INLET.DB'.
EXIT.
EXIT.
FETCH, DN=FILO02, DF=TR, TEXT='HPFTP-INLET.DB'.
ACCESS, DN=FILO02, PDN=HPFTP, ID=KPOOL, UQ.
ASSIGN, DN=FILO02, LM=300000, U.
/EOF
$ MESH
  CLEAR -1
  MAX/MXPOINT=8725 15000 15000
  ELTYPE 4,1,6
  ASSIGN IPAL=0
REMARK '
REMARK ' *****
REMARK ' SPACE SHUTTLE MAIN ENGINE HIGH PRESSURE FUEL TURBO PUMP (HPFTP)
REMARK ' Vanes are modified to extend into inner and outer rings
REMARK ' (1 layer of elements) so that there is moment transfered.
REMARK ' ALL NEW LOADS ARE APPLIED - FPL
REMARK ' *****
REMARK '
  SET SYNTAX ON
DEFSYS 1 1 3M0.0, 1.0,0.0,0.0 0.0,1.0,0.0 #CYLINDRICAL COORD SYSTEM
DEFSYS 11 1 0.0,-0.000001,0. -1.0,-0.000001,0.0 0.0,-1.0,0.0
REMARK '
REMARK ' *****
REMARK ' * AXISYMMETRIC SOLID ELEMENT MESHES *
REMARK ' * IN MAIN BODY OF PUMP BELOW TOROID * HYBRID SOLID ELEM
REMARK ' * THREE MESHES *
REMARK ' *****

#MESH POINTS FOR MESH 1 (INNER RING) THETA=0.0 DEG

# 999981-12C KVP SSME HPF1 2 1
IJPOINT 1 3 15 2.500000 0.0 4.671000 1
          2 4 15 2.949999 0.0 4.790000 1
          3 5 15 3.250000 0.0 4.790000 1
          4 5 13 3.250000 0.0 4.099999 1
          5 4 13 2.865000 0.0 4.099999 1
          6 4 11 2.615000 0.0 3.849999 1

```


7	0	0	2.615000	0.0	3.710355	1
8	4	9	2.749561	0.0	3.488602	1
308	6	9	2.749561	0.0	3.488602	1
9	0	0	2.931933	0.0	3.469481	1
10	6	11	3.136975	0.0	3.595601	1
11	6	13	3.331487	0.0	3.731799	1
12	6	15	3.525998	0.0	3.867997	1
315	7	15	0.0	0.0		
17	8	15	3.563346	0.0	3.814658	1
18	8	13	3.406328	0.0	3.624912	1
19	8	11	3.230719	0.0	3.461722	1
20	8	9	2.968478	0.0	3.257798	1
21	8	7	2.726711	0.0	3.030447	1
22	8	5	2.511195	0.0	2.778073	1
23	8	3	2.324505	0.0	2.503693	1
24	8	1	2.069802	0.0	1.969996	1
25	6	1	2.030000	0.0	2.168929	1
26	6	3	2.230315	0.0	2.560510	1
27	0	0	2.333184	0.0	2.781142	1
28	4	5	2.349998	0.0	3.023998	1
328	6	5	2.349998	0.0	3.023998	1
29	3	5	2.193999	0.0	3.179998	1
30	1	5	1.849999	0.0	3.179999	1
31	1	9	1.849999	0.0	3.570000	1
32	2	9	2.139997	0.0	3.570000	1
33	3	9	2.500000	0.0	3.569999	1
133	3	10				

#MESH 2 POINTS

IJPOINT	40	15	1	3.116799	0.0	1.339998	1
	41	15	3	3.274999	0.0	1.339998	1
	42	13	3	3.362834	0.0	1.667802	1
	43	11	3	3.573189	0.0	1.808357	1
143	12	3					
	44	11	4	3.740000	0.0	1.618148	1
	45	12	4	3.740000	0.0	1.209999	1
	46	13	4	3.987499	0.0	1.209999	1
	47	15	4	3.987499	0.0	1.089999	1
	48	15	6	4.325000	0.0	1.089999	1
	49	19	6	4.325000	0.0	0.550000	1
	50	19	8	4.485000	0.0	0.550000	1
	51	21	8	4.484999	0.0	-0.111607	1
	52	25	8	5.439998	0.0	-0.280000	1
	53	25	6	6.067499	0.0	-0.280000	1
	54	26	6	6.067499	0.0	-0.176000	1
	55	26	8	5.637500	0.0	-0.176000	1
	56	26	10	5.637500	0.0	0.200000	1
	72	7	6	4.075229	0.0	2.158201	1
	73	0	0	4.008238	0.0	2.158201	1
	74	7	3	3.912857	0.0	2.221931	1
	75	0	0	3.969543	0.0	2.368747	1
	76	5	3	4.045116	0.0	2.444320	1
	77	3	3	4.154998	0.0	2.554201	1
	78	1	3	4.195000	0.0	2.554202	1
	84	1	2				
	85	1	1	4.195000	0.0	2.662999	1
	86	3	1	4.138799	0.0	2.662999	1
	87	5	1	3.888425	0.0	2.579901	1
	88	7	1	3.642982	0.0	2.411384	1

89	9	1	3.438335	0.0	2.194444	1
90	11	1	3.279151	0.0	1.942248	1
91	13	1	3.171350	0.0	1.664181	1
93	9	6	4.120360	0.0	1.759949	1
94	11	6	4.010991	0.0	1.632932	1
95	12	6	4.023471	0.0	1.465781	1
96	13	6	4.150488	0.0	1.356413	1
97	13	8	4.417089	0.0	1.268602	1
98	15	8	4.499999	0.0	1.124999	1
99	17	8	4.500000	0.0	0.875000	1
100	17	10	4.650000	0.0	0.875000	1
101	21	10	4.649999	0.0	0.216948	1
102	22	10	4.782215	0.0	0.059379	1
103	24	10	5.252214	0.0	-0.023495	1
104	25	10	5.440000	0.0	0.134075	1

#MESH 3 POINTS

IJPOINT	57	12	6	6.247499	0.0	0.200000	1
	157	11	6				
	58	10	6	6.247499	0.0	0.660000	1
	59	9	6	6.457225	0.0	0.849284	1
	159	9	7				
	60	9	8	7.199999	0.0	-0.000001	1
	61	9	9	7.975501	0.0	-0.000001	1
	62	9	12	8.524999	0.0	-1.322000	1
	63	9	14	8.525000	0.0	-3.160000	1
	64	8	14	9.349999	0.0	-2.810999	1
	65	7	14	9.825000	0.0	-2.810999	1
	66	7	12	9.825000	0.0	-1.580000	1
	67	8	12	9.334236	0.0	-1.448501	1
	68	8	9	8.485347	0.0	0.504793	1
	69	8	8	7.914613	0.0	0.893628	1
	70	8	6	6.683242	0.0	1.299203	1
	71	7	6	5.960766	0.0	1.537164	1
	92	2	4	4.287511	0.0	1.772429	1
	105	11	1	5.440000	0.0	0.390000	1
	106	11	2	5.549999	0.0	0.390000	1
	107	10	2	5.549999	0.0	0.590000	1
	108	10	4	5.852603	0.0	0.676646	1
	109	9	4	5.975420	0.0	0.895178	1
	110	8	4	5.927133	0.0	1.141163	1
	111	7	4	5.730817	0.0	1.297049	1
	201	0	0	2.865000	0.0	3.849999	1
	204	0	0	4.924999	0.0	0.935000	1
	202	0	0	2.193999	0.0	3.023999	1
	203	0	0	2.06033	0.0	4.929980	1
	205	0	0	6.240000	0.0	4.188000	1
	206	0	0	2.055000	0.0	4.903000	1
	207	0	0	4.219000	0.0	1.564420	1
	208	0	0	5.617370	0.0	0.952625	1
	209	0	0	4.810000	0.0	0.216948	1
	210	0	0	5.280000	0.0	0.134075	1
	211	0	0	3.548150	0.0	1.618150	1
	212	0	0	7.523570	0.0	-0.293631	1
	213	0	0	6.660000	0.0	-1.322000	1
	214	0	0	5.550000	0.0	-1.932000	1
	215	0	0	6.450240	0.0	0.646194	1
	216	0	0	5.930320	0.0	-0.360994	1

REMARK '*****
 REMARK ' MESH 1 - INNER RING
 REMARK '*****

SLINES 30,29
 CIRCLE 29,28,202
 SPLINE 28,328,0 28,328,27,26,25
 SPLINE 328,26,0 28,328,27,26,25
 SPLINE 26,25,0 28,328,27,26,25
 SLINES 25,24
 SPLINE 24,23,0 24,23,22,21,20,19,18,17
 SPLINE 23,22,0 24,23,22,21,20,19,18,17
 SPLINE 22,21,0 24,23,22,21,20,19,18,17
 SPLINE 21,20,0 24,23,22,21,20,19,18,17
 SPLINE 20,19,0 24,23,22,21,20,19,18,17
 SPLINE 19,18,0 24,23,22,21,20,19,18,17
 SPLINE 18,17,0 24,23,22,21,20,19,18,17
 SLINES 17,12,11,10
 SPLINE 10,308,0 10,9,308,7,6
 SLINE 308,8
 SPLINE 8,6,0 10,9,8,7,6
 CIRCLE 6,5,201
 SLINES 5,4,3,2,1,33,32,31,30

SLINES 10,19:33,8:8,28:308,328:33,29

VOID 28 11
 VOID 4 12
 IJSOLID 0 0 1 HSO 0 NAME=MSH1
 IJSOLID 11 17 1 HSO 0 NAME=,,,WLD1
 IJSOLID 315 24 1 HSO 0 NAME=,,INNER,PRES
 KNAME 2 2 1 31 INNER,BOLT
 IJNAME 21 8 INSD,VANE
 IJNAME 19 10 INSD,VANE
 IJNAME 23 26 INSD,VANE

IJNAME 1 133 P208,FAC2
 IJNAME 31 30 P208,FAC2
 IJNAME 31 32 P208,FAC4
 IJNAME 30 28 P208,FAC1
 IJNAME 328 25 P208,FAC2

PRISM 31 0. 0. 0. 3 360. 1. 0. 0. 0. 0. 0.

MESH 1
 MERGE

REMARK '*****
 REMARK ' MESH 2 - OUTER RING
 REMARK '*****

SLINE 85,86
 SPLINE 86,87,0 85,86,87,88,89,90,91,40
 SPLINE 87,88,0 85,86,87,88,89,90,91,40
 SPLINE 88,89,0 85,86,87,88,89,90,91,40
 SPLINE 89,90,0 85,86,87,88,89,90,91,40
 SPLINE 90,91,0 85,86,87,88,89,90,91,40

SPLINE 91,40,0 85,86,87,88,89,90,91,40
 SLINES 40 41 42
 CIRCLE 42,43,211:43,44,211
 SLINES 44T56,104
 CIRCLE 104,103,210
 SLINE 103,102
 CIRCLE 102,101,209
 SLINES 101,100,99,98,97,96
 CIRCLE 96,95,207:95,94,207:94,93,207
 SLINES 93,72
 SPLINE 72,74,0 72,73,74,75,76
 SPLINE 74,76,0 72,73,74,75,76
 SLINE 76,77,78,85

SLINES 86,77:88,74:44,94:52,55:87,76:42,91:74,43
 SLINES 96,46:96,48:98,48:99,50:93,89
 SLINES 51,101
 IJSOLID 0 0 1 HSD 0 NAME=MSH2
 IJSOLID 78 86 1 HSD 0 NAME=,,,WLD2
 IJSOLID 84 40 1 HSD 0 NAME=,,OUTR,PRES
 VOID 43,47
 IJNAME 87,76,OUTR,VANE
 IJNAME 89,93,OUTR,VANE
 IJNAME 91,42,OUTR,VANE

IJNAME 41 143 P208,FAC4
 IJNAME 43 44 P208,FAC5
 IJNAME 45 47 P208,FAC1
 IJNAME 47 48 P438,FAC5
 IJNAME 48 49 P438,FAC1
 IJNAME 49 50 P438,FAC5
 IJNAME 50 51 P438,FAC1
 IJNAME 54 56 P777,FAC5

PRISM 31 0. 0. 0. 3 360. 1. 0. 0. 0. 0. 0.

MESH

MERGE

REMARK ' *****
 REMARK ' MESH 3 - OUTER RING (PART II)
 REMARK ' *****

IJPOINT	56	12	2	5.637500	0.0	0.200000	1
	72	1	6	4.075229	0.0	2.158201	1
	93	1	4	4.120360	0.0	1.759949	1
	104	12	1	5.440000	0.0	0.134075	1

CIRCLE 93,92,207
 SLINES 92,111
 CIRCLE 111,110,208:110,109,208:109,108,208:108,107,208
 SLINES 107,106,105,104,56,57,58
 CIRCLE 58,59,215:59,60,216
 SLINES 60,61
 CIRCLE 61,62,213
 SLINES 62T67
 CIRCLE 67,68,214:68,69,212
 SLINES 69T72,93

SLINES 71,111:70,110:58,108:106,56:69,60:68,61:67,62:64,67

IJSOLID 0 0 1 HSD 0 NAME=MSH3
KNAME 64 64 1 31 OUTR,BOLT

IJNAME 56 57 P777,FAC5
IJNAME 57 157 P334,FAC4 #51,424 LBS/ 2*PI*R*.46 (SEE IJPOINTS 57,58) + 500 PSI
IJNAME 58 58 P500,FAC4
IJNAME 159 60 P500,FAC5
IJNAME 61 63 P500,FAC5
IJNAME 60 61 P19K,FAC5

PRISM 31 0. 0. 0. 3 360. 1. 0. 0. 0. 0. 0.

MESH

MERGE

REMARK '

REMARK ' *****

REMARK ' * SHELL ELEMENT MESH MAKING UP TOROID *

REMARK ' * FROM THETA = 0 TO 300 DEGREES *

REMARK ' *****

999981-12C KVP SSME HPF1 3 1

#####

#section - 3

#####

#FIXED POINTS (EXCEPT FOR THETA)

IJPOINT	1203	1	3	3.525998	0.0	3.867997	1
	1703	1	1	3.563346	0.0	3.814658	1
	303	0	0	2.060328	0.0	4.929984	1
	603	0	0	2.054999	0.0	4.903000	1
	1302	4	3	3.690646	0.0	4.143754	1
	1602	4	1	3.741757	0.0	4.119106	1
	7702	4	2	3.716223	0.0	4.131503	1
	7803	30	3	4.195000	0.0	2.554202	1
	8503	30	1	4.195000	0.0	2.662999	1
	8402	28	1	4.290326	0.0	2.636950	1
	7902	28	3	4.269582	0.0	2.544046	1
	8102	28	2	4.279954	0.0	2.590498	1
	7603	0	0	4.154998	0.0	2.554201	1
	8703	0	0	4.138799	0.0	2.662999	1

#VARYING POINTS

IJPOINT	1303	0	0	3.839394	0.0	4.596750	1
	7703	0	0	3.863730	0.0	4.592191	1
	1603	0	0	3.888068	0.0	4.587631	1
	1503	7	1	3.930226	0.0	4.783211	1
	8603	7	2	3.905653	0.0	4.787814	1
	1403	7	3	3.881081	0.0	4.792418	1
	8403	0	0	4.546110	0.0	2.455962	1
	8103	0	0	4.528584	0.0	2.438040	1
	7903	0	0	4.511099	0.0	2.420265	1
	8303	25	1	4.717591	0.0	2.345176	1
	8003	25	3	4.690458	0.0	2.303178	1
	8203	25	2	4.704024	0.0	2.324177	1
	103	17	2	8.649978	0.0	4.182926	1
	503	0	0	6.240000	0.0	4.182997	1

#####

#Section - 5

#####

#FIXED POINTS (EXCEPT FOR THETA)

IJPOINT	1205	1	3	3.525998	30.0	3.867997	1
	1705	1	1	3.563346	30.0	3.814658	1

305	0	0	2.060328	30.0	4.929984	1	
605	0	0	2.054999	30.0	4.903000	1	
1304	4	3	3.690646	30.0	4.143754	1	
1604	4	1	3.741757	30.0	4.119106	1	
7704	4	2	3.716223	30.0	4.131503	1	
7805	30	3	4.195000	30.0	2.554202	1	
8505	30	1	4.195000	30.0	2.662999	1	
8404	28	1	4.290326	30.0	2.636950	1	
7904	28	3	4.269582	30.0	2.544046	1	
8104	28	2	4.279954	30.0	2.590498	1	
7605	0	0	4.154998	30.0	2.554201	1	
8705	0	0	4.138799	30.0	2.662999	1	
#VARYING POINTS							
IJPOINT	1305	0	0	3.834550	30.0	4.571858	1
	1605	0	0	3.883470	30.0	4.561982	1
	1505	7	1	3.928404	30.0	4.756945	1
	1405	7	3	3.879393	30.0	4.766839	1
	8405	0	0	4.539644	30.0	2.462191	1
	7905	0	0	4.505280	30.0	2.425872	1
	8305	25	1	4.710428	30.0	2.351691	1
	8005	25	3	4.683267	30.0	2.309711	1
	8105	0	0	4.522462	30.0	2.444031	1
	8205	25	2	4.696847	30.0	2.330701	1
	7705	0	0	3.859010	30.0	4.566920	1
	8605	7	2	3.903898	30.0	4.761891	1
	105	17	2	8.440594	30.0	4.142996	1
	505	0	0	6.129998	30.0	4.142996	1
#####							
#Section - 7							
#####							
#FIXED POINTS (EXCEPT FOR THETA)							
IJPOINT	1207	1	3	3.525998	60.0	3.867997	1
	1707	1	1	3.563346	60.0	3.814658	1
	307	0	0	2.060328	60.0	4.929984	1
	607	0	0	2.054999	60.0	4.903000	1
	1306	4	3	3.690646	60.0	4.143754	1
	1606	4	1	3.741757	60.0	4.119106	1
	7706	4	2	3.716223	60.0	4.131503	1
	7807	30	3	4.195000	60.0	2.554202	1
	8507	30	1	4.195000	60.0	2.662999	1
	8406	28	1	4.290326	60.0	2.636950	1
	7906	28	3	4.269582	60.0	2.544046	1
	8106	28	2	4.279954	60.0	2.590498	1
	7607	0	0	4.154998	60.0	2.554201	1
	8707	0	0	4.138799	60.0	2.662999	1
#VARYING POINTS							
IJPOINT	1307	0	0	3.827292	60.0	4.537622	1
	1607	0	0	3.876534	60.0	4.526687	1
	1507	7	1	3.926016	60.0	4.720570	1
	1407	7	3	3.877205	60.0	4.731409	1
	8407	0	0	4.531909	60.0	2.469357	1
	7907	0	0	4.498318	60.0	2.432321	1
	8307	25	1	4.697639	60.0	2.354384	1
	8007	25	3	4.669139	60.0	2.313302	1
	8107	0	0	4.515113	60.0	2.450838	1
	8207	25	2	4.683389	60.0	2.333843	1
	7707	0	0	3.851912	60.0	4.532154	1
	8607	7	2	3.901610	60.0	4.725989	1
	107	17	2	8.193307	60.0	4.087998	1
	507	0	0	6.000000	60.0	4.087998	1

#####

#Section - 9

#####

#FIXED POINTS (EXCEPT FOR THETA)

IJPOINT	1209	1	3	3.525998	90.0	3.867997	1
	1709	1	1	3.563346	90.0	3.814658	1
	309	0	0	2.060328	90.0	4.929984	1
	609	0	0	2.054999	90.0	4.903000	1
	1308	4	3	3.690646	90.0	4.143754	1
	1608	4	1	3.741757	90.0	4.119106	1
	7708	4	2	3.716223	90.0	4.131503	1
	7809	30	3	4.195000	90.0	2.554202	1
	8509	30	1	4.195000	90.0	2.662999	1
	8408	28	1	4.290326	90.0	2.636950	1
	7908	28	3	4.269582	90.0	2.544046	1
	8108	28	2	4.279954	90.0	2.590498	1
	7609	0	0	4.154998	90.0	2.554201	1
	8709	0	0	4.138799	90.0	2.662999	1

#VARYING POINTS

IJPOINT	1309	0	0	3.819539	90.0	4.504210	1
	1609	0	0	3.869071	90.0	4.492221	1
	1509	7	1	3.922709	90.0	4.685012	1
	1409	7	3	3.874111	90.0	4.696774	1
	8409	0	0	4.523301	90.0	2.476985	1
	7909	0	0	4.490571	90.0	2.439186	1
	8309	25	1	4.686240	90.0	2.359630	1
	8009	25	3	4.657018	90.0	2.319057	1
	8109	0	0	4.506936	90.0	2.458085	1
	8209	25	2	4.671629	90.0	2.339343	1
	7709	0	0	3.844304	90.0	4.498215	1
	8609	7	2	3.898410	90.0	4.690893	1
	109	17	2	7.956713	90.0	4.037998	1
	509	0	0	5.875000	90.0	4.037998	1

#####

#Section 11

#####

#FIXED POINTS (EXCEPT FOR THETA)

IJPOINT	1211	1	3	3.525998	120.0	3.867997	1
	1711	1	1	3.563346	120.0	3.814658	1
	311	0	0	2.060328	120.0	4.929984	1
	611	0	0	2.054999	120.0	4.903000	1
	1310	4	3	3.690646	120.0	4.143754	1
	1610	4	1	3.741757	120.0	4.119106	1
	7710	4	2	3.716223	120.0	4.131503	1
	7811	30	3	4.195000	120.0	2.554202	1
	8511	30	1	4.195000	120.0	2.662999	1
	8410	28	1	4.290326	120.0	2.636950	1
	7910	28	3	4.269582	120.0	2.544046	1
	8110	28	2	4.279954	120.0	2.590498	1
	7611	0	0	4.154998	120.0	2.554201	1
	8711	0	0	4.138799	120.0	2.662999	1

#VARYING POINTS

IJPOINT	1311	0	0	3.810061	120.0	4.466805	1
	1611	0	0	3.859895	120.0	4.453612	1
	1511	7	1	3.918268	120.0	4.645047	1
	1411	7	3	3.869933	120.0	4.657844	1
	8411	0	0	4.511195	120.0	2.487138	1
	7911	0	0	4.479675	120.0	2.448324	1
	8311	25	1	4.676920	120.0	2.373953	1
	8011	25	3	4.648720	120.0	2.332664	1

8111	0	0	4.495435	120.0	2.467731	1
8211	25	2	4.662820	120.0	2.353308	1
7711	0	0	3.834978	120.0	4.460209	1
8611	7	2	3.894100	120.0	4.651445	1
111	17	2	7.682194	120.0	3.987990	1
511	0	0	5.729998	120.0	3.987990	1

#####

#Section 13

#####

#FIXED POINTS (EXCEPT FOR THETA)

IJPOINT	1213	1	3	3.525998	150.0	3.867997	1
	1713	1	1	3.563346	150.0	3.814658	1
	313	0	0	2.060328	150.0	4.929984	1
	613	0	0	2.054999	150.0	4.903000	1
	1312	4	3	3.690646	150.0	4.143754	1
	1612	4	1	3.741757	150.0	4.119106	1
	7712	4	2	3.716223	150.0	4.131503	1
	7813	30	3	4.195000	150.0	2.554202	1
	8513	30	1	4.195000	150.0	2.662999	1
	8412	28	1	4.290326	150.0	2.636950	1
	7912	28	3	4.269582	150.0	2.544046	1
	8112	28	2	4.279954	150.0	2.590498	1
	7613	0	0	4.154998	150.0	2.554201	1
	8713	0	0	4.138799	150.0	2.662999	1

#VARYING POINTS

IJPOINT	1313	0	0	3.796484	150.0	4.418265	1
	1613	0	0	3.846666	150.0	4.403473	1
	1513	7	1	3.915975	150.0	4.591550	1
	1413	7	3	3.868014	150.0	4.605687	1
	8413	0	0	4.496839	150.0	2.498368	1
	7913	0	0	4.466755	150.0	2.458431	1
	8313	25	1	4.663096	150.0	2.386676	1
	8013	25	3	4.635214	150.0	2.345172	1
	8113	0	0	4.481796	150.0	2.478399	1
	8213	25	2	4.649155	150.0	2.365924	1
	7713	0	0	3.821575	150.0	4.410869	1
	8613	7	2	3.891994	150.0	4.598619	1
	113	17	2	7.365129	150.0	3.922998	1
	513	0	0	5.570000	150.0	3.922998	1

#####

#Section 15

#####

#FIXED POINTS (EXCEPT FOR THETA)

IJPOINT	1215	1	3	3.525998	180.0	3.867997	1
	1715	1	1	3.563346	180.0	3.814658	1
	315	0	0	2.060328	180.0	4.929984	1
	615	0	0	2.054999	180.0	4.903000	1
	1314	4	3	3.690646	180.0	4.143754	1
	1614	4	1	3.741757	180.0	4.119106	1
	7714	4	2	3.716223	180.0	4.131503	1
	7815	30	3	4.195000	180.0	2.554202	1
	8515	30	1	4.195000	180.0	2.662999	1
	8414	28	1	4.290326	180.0	2.636950	1
	7914	28	3	4.269582	180.0	2.544046	1
	8114	28	2	4.279954	180.0	2.590498	1
	7615	0	0	4.154998	180.0	2.554201	1
	8715	0	0	4.138799	180.0	2.662999	1

#VARYING POINTS

IJPOINT	1315	0	0	3.782863	180.	4.374143	1
	1615	0	0	3.833319	180.	4.357860	1

1515	7	1	3.907163	180.	4.544185	1
1415	7	3	3.859579	180.	4.559540	1
8415	0	0	4.424942	180.	2.552450	1
7915	0	0	4.398211	180.	2.497786	1
8315	25	1	4.593356	180.	2.441578	1
8015	25	3	4.565862	180.	2.3998	1
8115	0	0	4.411576	180.	2.525118	1
8215	25	2	4.579609	180.	2.420696	1
7715	0	0	3.808090	180.	4.366001	1
8615	7	2	3.883370	180.	4.551862	1
115	17	2	7.090474	180.	3.872999	1
515	0	0	5.415000	180.	3.872999	1

#####

#Section 17

#####

#FIXED POINTS (EXCEPT FOR THETA)

IJPOINT	1217	1	3	3.525998	210.0	3.867997	1
	1717	1	1	3.563346	210.0	3.814658	1
	317	0	0	2.060328	210.0	4.929984	1
	617	0	0	2.054999	210.0	4.903000	1
	1316	4	3	3.690646	210.0	4.143754	1
	1616	4	1	3.741757	210.0	4.119106	1
	7716	4	2	3.716223	210.0	4.131503	1
	7817	30	3	4.195000	210.0	2.554202	1
	8517	30	1	4.195000	210.0	2.662999	1
	8416	28	1	4.290326	210.0	2.636950	1
	7916	28	3	4.269582	210.0	2.544046	1
	8116	28	2	4.279954	210.0	2.590498	1
	7617	0	0	4.154998	210.0	2.554201	1
	8717	0	0	4.138799	210.0	2.662999	1

#VARYING POINTS

IJPOINT	1317	0	0	3.763176	210.	4.316481	1
	1617	0	0	3.813922	210.	4.298196	1
	1517	7	1	3.894891	210.	4.485970	1
	1417	7	3	3.846293	210.	4.497732	1
	8417	0	0	4.379584	210.	2.585257	1
	7917	0	0	4.352711	210.	2.518019	1
	8317	25	1	4.553713	210.	2.482040	1
	8017	25	3	4.528217	210.	2.439029	1
	8117	0	0	4.366147	210.	2.551638	1
	8217	25	2	4.540965	210.	2.460534	1
	7717	0	0	3.788548	210.	4.307338	1
	8617	7	2	3.870592	210.	4.491851	1
	117	17	2	6.740663	210.	3.813000	1
	517	0	0	5.224999	210.	3.813000	1

#####

#Section 19

#####

#FIXED POINTS (EXCEPT FOR THETA)

IJPOINT	1219	1	3	3.525998	240.0	3.867997	1
	1719	1	1	3.563346	240.0	3.814658	1
	319	0	0	2.060328	240.0	4.929984	1
	619	0	0	2.054999	240.0	4.903000	1
	1318	4	3	3.690646	240.0	4.143754	1
	1618	4	1	3.741757	240.0	4.119106	1
	7718	4	2	3.716223	240.0	4.131503	1
	7819	30	3	4.195000	240.0	2.554202	1
	8519	30	1	4.195000	240.0	2.662999	1
	8418	28	1	4.290326	240.0	2.636950	1
	7918	28	3	4.269582	240.0	2.544046	1

8118	28	2	4.279954	240.0	2.590498	1
7619	0	0	4.154998	240.0	2.554201	1
8719	0	0	4.138799	240.0	2.662999	1
#VARYING POINTS						
IJPOINT	1319	0	0	3.735987	240.	4.245709 1
	1619	0	0	3.786980	240.	4.224884 1
	1519	7	1	3.874114	240.	4.405333 1
	1419	7	3	3.827825	240.	4.424236 1
	8419	0	0	4.336511	240.	2.612899 1
	7919	0	0	4.311336	240.	2.532804 1
	8319	25	1	4.520979	240.	2.532796 1
	8019	25	3	4.501063	240.	2.486933 1
	8119	0	0	4.323923	240.	2.572851 1
	8219	25	2	4.511021	240.	2.509864 1
	7719	0	0	3.761483	240.	4.235296 1
	8619	7	2	3.850969	240.	4.414784 1
	119	17	2	6.338047	240.	3.747998 1
	519	0	0	5.004999	240.	3.747998 1

#Section 21

#FIXED POINTS (EXCEPT FOR THETA)

IJPOINT	1221	1	3	3.525998	270.0	3.867997 1
	1721	1	1	3.563346	270.0	3.814658 1
	321	0	0	2.060328	270.0	4.929984 1
	621	0	0	2.054999	270.0	4.903000 1
	1320	4	3	3.690646	270.0	4.143754 1
	1620	4	1	3.741757	270.0	4.119106 1
	7720	4	2	3.716223	270.0	4.131503 1
	7821	30	3	4.195000	270.0	2.554202 1
	8521	30	1	4.195000	270.0	2.662999 1
	8420	28	1	4.290326	270.0	2.636950 1
	7920	28	3	4.269582	270.0	2.544046 1
	8120	28	2	4.279954	270.0	2.590498 1
	7621	0	0	4.154998	270.0	2.554201 1
	8721	0	0	4.138799	270.0	2.662999 1

#VARYING POINTS

IJPOINT	1321	0	0	3.690667	270.	4.143827 1
	1621	0	0	3.741778	270.	4.119180 1
	1521	7	1	3.842451	270.	4.292672 1
	1421	7	3	3.797414	270.	4.314390 1
	8421	0	0	4.290326	270.	2.636950 1
	7921	0	0	4.269582	270.	2.544046 1
	8321	25	1	4.482183	270.	2.578427 1
	8021	25	3	4.467595	270.	2.530602 1
	8121	0	0	4.279954	270.	2.590498 1
	8221	25	2	4.474889	270.	2.554515 1
	7721	0	0	3.716223	270.	4.131503 1
	8621	7	2	3.819932	270.	4.303531 1
	121	17	2	5.876244	270.	3.652999 1
	521	0	0	4.745000	270.	3.652999 1

#Section 23

#FIXED POINTS (EXCEPT FOR THETA)

IJPOINT	1223	1	3	3.525998	300.0	3.867997 1
	1723	1	1	3.563346	300.0	3.814658 1
	323	0	0	2.060328	300.0	4.929984 1
	623	0	0	2.054999	300.0	4.903000 1
	1322	4	3	3.690646	300.0	4.143754 1

1622	4	1	3.741757	300.0	4.119106	1	
7722	4	2	3.716223	300.0	4.131503	1	
7823	30	3	4.195000	300.0	2.554202	1	
8523	30	1	4.195000	300.0	2.662999	1	
8422	28	1	4.290326	300.0	2.636950	1	
7922	28	3	4.269582	300.0	2.544046	1	
8122	28	2	4.279954	300.0	2.590498	1	
7623	0	0	4.154998	300.0	2.554201	1	
8723	0	0	4.138799	300.0	2.662999	1	
#VARYING POINTS							
IJPOINT	1323	0	0	3.690646	300.	4.143754	1
	1623	0	0	3.741757	300.	4.119106	1
	1523	7	1	3.878649	300.	4.243695	1
	1423	7	3	3.848908	300.	4.283832	1
	8423	0	0	4.290326	300.	2.636950	1
	7923	0	0	4.269582	300.	2.544046	1
	8323	25	1	4.491205	300.	2.618833	1
	8023	25	3	4.486713	300.	2.569035	1
	8123	0	0	4.279954	300.	2.590498	1
	8223	25	2	4.488959	300.	2.593933	1
	7723	0	0	3.716223	300.	4.131503	1
	8623	7	2	3.863789	300.	4.263800	1
	123	17	2	5.317389	300.	3.518000	1
	523	0	0	4.415000	300.	3.518000	1

SET SYNTAX ON
DO ;10 &I=0,20,2

IJGRID 3+&I
#CIRCLE 1703+&I,1602+&I,603+&I
SLINES 1703+&I,1602+&I
#SPLINE 1602+&I,1503+&I,0,1703+&I,1602+&I,1603+&I,1503+&I
SLINES 1602+&I,1503+&I

SLINES 1503+&I,8603+&I,1403+&I

#SPLINE 1403+&I,1302+&I,0,1403+&I,1303+&I,1302+&I,1203+&I
SLINES 1403+&I,1302+&I

#CIRCLE 1302+&I,1203+&I,303+&I
SLINES 1302+&I,1203+&I

SLINES 1203+&I,1703+&I:1302+&I,7702+&I,1602+&I

#SPLINE 7702+&I,8603+&I,0,7702+&I,7703+&I,8603+&I
SLINES 7702+&I,8603+&I

IJGRID 103+&I
#SPLINE 8303+&I,8402+&I,0,8303+&I,8403+&I,8402+&I,8503+&I,8703+&I
#SPLINE 8402+&I,8503+&I,0,8303+&I,8403+&I,8402+&I,8503+&I,8703+&I
SLINES 8303+&I,8402+&I,8503+&I

SLINES 8503+&I,7803+&I

#SPLINE 7803+&I,7902+&I,0,7603+&I,7803+&I,7902+&I,7903+&I,8003+&I
#SPLINE 7902+&I,8003+&I,0,7603+&I,7803+&I,7902+&I,7903+&I,8003+&I
SLINES 7803+&I,7902+&I,8003+&I

SLINES 8003+&I,8203+&I,8303+&I:7902+&I,8102+&I,8402+&I

```
#SPLINE 8102+&I,8203+&I,0,8102+&I,8103+&I,8203+&I
SLINES 8102+&I,8203+&I
```

```
IJGRID 203+&I
#SPLINE 7702+&I,8603+&I,0,7702+&I,7703+&I,8603+&I
CIRCLE 8603+&I,103+&I,503+&I:103+&I,8203+&I,503+&I
#SPLINE 8102+&I,8203+&I,0,8102+&I,8103+&I,8203+&I
```

```
;10 NOP
```

```
*****
```

```
MSYS=11
RULE 6 5 7
RULE 11 9 11
RULE 16 13 15
RULE 21 17 19
RULE 26 21 23
IJSOLID 1703 1403 1 HSO 0 _NAME=MSH4
IJSOLID 1703 1302 1 HSO 0 _NAME=MSH4,TORS,WLD1
IJSOLID 1703 8603 1 HSO 0 _NAME=MSH4,,,PRES
KSSHELL 1602 1403 1 4M.025 4M0. 1 FSH 0 0 0 0. EDGE
IJSHELL 1503,8603 .025 .025 0.0 0.0 1 FSH 0 -1 0 0. EDGE
IJSHELL 1403,8603 .025 .025 0.0 0.0 1 FSH 0 -1 0 0. EDGE
MESH/IJGRID=3
```

```
MERGE
```

```
MSYS=11
RULE 6 105 107
RULE 11 109 111
RULE 16 113 115
RULE 21 117 119
RULE 26 121 123
IJSOLID 8003 8503 1 HSO 0 _NAME=MSH5
IJSOLID 7902 8503 1 HSO 0 _NAME=MSH5,TORS,WLD2
IJSOLID 8203 8503 1 HSO 0 _NAME=MSH5,,,PRES
IJSHELL 8203,8303 .025 .025 0.0 0.0 1 FSH 0 -1 0 0. EDGE
IJSHELL 8203,8003 .025 .025 0.0 0.0 1 FSH 0 -1 0 0. EDGE
KSSHELL 8303 7902 1 4M.025 4M0. 1 FSH 0 0 0 0. EDGE
MESH/IJGRID=103
```

```
MERGE
```

```
MSYS=11
RULE 6 205 207
RULE 11 209 211
RULE 16 213 215
RULE 21 217 219
RULE 26 221 223
IJSHELL 8603,8203 .050 .050 0.0 0.0 1 FSH 0 -1 0 0. _NAME=,,SHLL,PRES
MESH/IJGRID=203
```

```
MERGE
REMARK '
REMARK ' ROTATE AND MIRROR ALL PREVIOUS MESHES
ROTATE -90. 3 1 all
mirror 1 0 0 0 1 all
REMARK '
```

```

REMARK ' *****
REMARK ' * TORUS INTERSECTION MESHES *
REMARK ' * TOROID FROM 300 TO 360 DEGREES *
REMARK ' *****
REMARK '
DEFSYS 1 2 -91.08,-6.24,3.1137,-91.06722,-6.24,2.1137 >
          -91.08,-5.24,3.1137 # SYSTEM USED TO DEFINE CONE
DEFSYS 3 0 -91.08,-6.24,3.1137,-91.09278,-6.24,4.1137 >
          -91.08,-7.24,3.1137 # SYSTEM USED TO DEFINE CONE
DEFSYS 2 3 0.,0.,3.55,0.,-1.,3.55,1.,0.,3.55,4.38
DEFSYS 4 1 0.,0.,0.,0.,-1.,0.,1.,0.,0.
DEFSURFACE 1 1 3 88.5
DEFSURFACE 2 2 1 .92
REMARK '
REMARK ' MESH A - MESH COMING INTO INTERSECTION - MESH 7
REMARK ' *****
      MSYS 4
      IJPOINT 1 1 1 3.716223 0. 4.131503 4
      IJPOINT 2 1 4 3.716223 0. 4.131503 4
          3 1 5 .92 15. 90. 2 1,2
          4 1 8 .92 35 70. 2 1,2
          5 1 10 .92 53. 60. 2 1
          6 1 14 .92 53. -15. 2 1
          7 1 16 1.4 53. -70. 2 1
          8 1 18 1.2 42. -70. 2 1
          9 1 21 .91 15. -70. 2 1,2
          10 1 22 4.279954 0. 2.590498 4
          11 1 25 4.279954 0. 2.590498 4
      SLINE 2,3
      SINT 3,4,.5
          4,5
      PLINE 5,6,7
      SINT 7,8
          8,9,3.
      SLINE 9 10
      IJGRID 1
      LET &X1 = .5 * 3.716223 + .5 * 3.863789
      LET &Z1 = .5 * 4.131503 + .5 * 4.263800
      LET &X2 = .5 * 4.279954 + .5 * 4.488959
      LET &Z2 = .5 * 2.590498 + .5 * 2.593933
      IJPOINT 29 1 1 3.716223 30. 4.131503 4
          30 1 4 &X1 30. &Z1 4
          31 1 5 .92 31.5 120. 2 2
          32 1 9 .92 47. 60. 2 2
          33 1 14 .92 52. 0. 2 2
          34 1 21 .92 31.5 -80. 2 2
          35 1 22 &X2 30. &Z2 4
          36 1 25 4.279954 30. 2.590498 4
      SLINE 30,31
      SINT 31,32
          32,33
          33,34
      SLINE 34,35
      IJGRID 2
      IJPOINT 19 1 1 3.716223 60. 4.131503 4
          20 1 4 3.863789 60. 4.263800 4
          21 1 14 5.317389 60. 3.518000 4
          22 1 22 4.488959 60. 2.593933 4
          23 1 25 4.279954 60. 2.590498 4
          24 0 0 4.415000 60. 3.518000 4

```

CIRCLE 20,21,24
 CIRCLE 21,22,24
 KSHLL 20,22,1,6,4M.05,4M.0,1,FSH,0,0,0,0.,SEC1
 RULE 6 1 2
 MESH
 MERGE TYPE=FSH
 REMARK '
 REMARK ' MESH B - MESH AT SHELL ELEMENT/SOLID ELEMENT INTERFACE - MESH 8
 REMARK ' *****
 MSYS 4

IJPOINT	9	1	1	4.195000	0.0	2.662999	4
	10	3	1	4.195000	0.0	2.554202	4
IJPOINT	11	1	3	4.290326	0.	2.636950	4
	12	2	3	4.279954	0.	2.590498	4
	13	3	3	4.269582	0.	2.544046	4
	14	3	6	4.269582	0.	2.544046	4
	15	2	6	4.279954	0.	2.590498	4
	16	1	6	4.290326	0.	2.636950	4

 SLINES 11,9,10,13
 SLINES 11,12,13,14,15,16,11
 LET &X24 = .5 * 4.269582 + .5 * 4.486713
 LET &Z24 = .5 * 2.544046 + .5 * 2.569035
 LET &X25 = .5 * 4.279954 + .5 * 4.488959
 LET &Z25 = .5 * 2.590498 + .5 * 2.593933
 LET &X26 = .5 * 4.290326 + .5 * 4.491205
 LET &Z26 = .5 * 2.636950 + .5 * 2.618833
 IJGRID 1

IJPOINT	19	1	1	4.195000	30.0	2.662999	4
	20	3	1	4.195000	30.0	2.554202	4
IJPOINT	21	1	3	4.290326	30.	2.636950	4
	22	2	3	4.279954	30.	2.590498	4
	23	3	3	4.269582	30.	2.544046	4
	24	3	6	&X24	30.	&Z24 4	
	25	2	6	&X25	30.	&Z25 4	
	26	1	6	&X26	30.	&Z26 4	

 SLINES 21,19,20,23
 SLINES 21,22,23,24,25,26,21
 IJGRID 2

IJPOINT	29	1	1	4.195000	60.0	2.662999	4
	30	3	1	4.195000	60.0	2.554202	4
IJPOINT	31	1	3	4.290326	60.	2.636950	4
	32	2	3	4.279954	60.	2.590498	4
	33	3	3	4.269582	60.	2.544046	4
	34	3	6	4.486713	60.	2.569035	4
	35	2	6	4.488959	60.	2.593933	4
	36	1	6	4.491205	60.	2.618833	4

 SLINES 31,29,30,33
 SLINES 31,32,33,34,35,36,31
 IJSHELL 34 36 2M.025 2M0. 1 FSH 0 0 0 0. EDGE
 IJSOLID 29,34,1,HSO 0 MSHB
 IJSOLID 29,35,1,HSO 0 MSHB,PRES
 RULE 6 1 2
 MESH
 MERGE
 REMARK '
 REMARK ' MESH C - MESH AT SHELL ELEMENT/SOLID ELEMENT INTERFACE - MESH 9
 REMARK ' *****
 MSYS 4

IJPOINT	9	1	1	3.525998	0.0	3.867997	4
	10	3	1	3.563346	0.0	3.814658	4

IJPOINT	11	1	4	3.690646	0.	4.143754	4
	12	2	4	3.716223	0.	4.131503	4
	13	3	4	3.741757	0.	4.119106	4
	14	3	7	3.741757	0.	4.119106	4
	15	2	7	3.716223	0.	4.131503	4
	16	1	7	3.690646	0.	4.143754	4

SLINES 11,9,10,13

SLINES 11,12,13,14,15,16,11

LET &X24 = .5 * 3.741757 + .5 * 3.878649

LET &Z24 = .5 * 4.119106 + .5 * 4.243695

LET &X25 = .5 * 3.716223 + .5 * 3.863789

LET &Z25 = .5 * 4.131503 + .5 * 4.263800

LET &X26 = .5 * 3.690646 + .5 * 3.848908

LET &Z26 = .5 * 4.143754 + .5 * 4.283832

IJGRID 1

IJPOINT	19	1	1	3.525998	30.0	3.867997	4
	20	3	1	3.563346	30.0	3.814658	4
IJPOINT	21	1	4	3.690646	30.	4.143754	4
	22	2	4	3.716223	30.	4.131503	4
	23	3	4	3.741757	30.	4.119106	4
	24	3	7	&X24	30.	&Z24	4
	25	2	7	&X25	30.	&Z25	4
	26	1	7	&X26	30.	&Z26	4

SLINES 21,19,20,23

SLINES 21,22,23,24,25,26,21

IJGRID 2

IJPOINT	29	1	1	3.525998	60.0	3.867997	4
	30	3	1	3.563346	60.0	3.814658	4
IJPOINT	31	1	4	3.690646	60.	4.143754	4
	32	2	4	3.716223	60.	4.131503	4
	33	3	4	3.741757	60.	4.119106	4
	34	3	7	3.878649	60.	4.243695	4
	35	2	7	3.863789	60.	4.263800	4
	36	1	7	3.848908	60.	4.283832	4

SLINES 31,29,30,33

SLINES 31,32,33,34,35,36,31

RULE 6 1 2

IJSHELL 34 36 2M.025 2MO. 1 FSH 0 0 0 0. EDGE

IJSOLID 29,34,1,HSO 0 MSHC

IJSOLID 30,35,1,HSO 0 MSHC,PRES

MESH

MERGE

REMARK '

REMARK ' MESH D - MESH OF PART BEING INTERSECTED - MESH 10

REMARK ' *****

DEFSYS 10,1,8.59 -6.24 4.182926,8.59 -5.24 >

4.182926,8.59 -6.24 5.182926

MSYS 10

let &delz = -2.

IJPOINT	1	1	1	4.279954	0.	2.590498	4
	2	2	1	.91 15.	-70.	2 1,2	
	3	5	1	1.2 42.	-70.	2 1	
	4	7	1	1.4 53.	-70.	2 1	
	5	9	1	.92 53.	-15.	2 1	
	6	13	1	.92 53.	60.	2 1	
	7	15	1	.92 35 70.	2 1,2		
	8	18	1	.92 15.	90.	2 1,2	
	9	19	1	3.716223	0.	4.131503	4
	10	19	4	3.905653	0.0	4.787814	4
	11	19	14	8.649978	0.0	4.182927	4

```

12 14 14 2.512 179.99 &delz 10
13 14 8 2.512 60. &delz 10
14 6 8 2.512 -100. &delz 10
15 6 12 2.512 -179.99 &delz 10
16 1 12 8.649978 0.0 4.182925 4
17 1 4 4.704024 0.0 2.324177 4
18 0 0 6.240000 0.0 4.182926 4
19 0 0 0.0001 0.0 &delz 10

```

```

SLINE 1 2
SINT 2,3,.33333
SINT 3,4
PLINE 4,5,6
SINT 6,7
SINT 7,8,2.0
SLINE 8,9,10
CIRCLE 10,11,18
SLINE 11,12
CIRCLE 12,13,19
      13,14,19
      14,15,19
SLINE 15,16
CIRCLE 16,17,18
SLINE 17,1
KSSHELL 1 11 1 4M.05 4M0. 1 FSH
MESH 3
MERGE TYPE=FSH

```

```

REMARK '*****
REMARK 'MESH 11 - CYLINDRICAL SHELL
REMARK '*****

```

```

DEFSYS 11,1,8.59 -6.24 4.24,8.59 -5.24 >
4.24,8.59 -6.24 5.24
IJPOINT 1 1 1 2.512 179.99 &delz 10
      2 7 1 2.512 60. &delz 10
      3 15 1 2.512 -100. &delz 10
      4 19 1 2.512 -179.99 &delz 10
      9 0 0 0.000 0.0 &DELZ 10

```

```

IJPOINT 21 1 4 2.6 179.99 0.78 11
      22 7 4 2.6 60. 0.78 11
      23 15 4 2.6 -100. 0.78 11
      24 19 4 2.6 -179.99 0.78 11
      29 0 0 0.000 0.0 0.78 11

```

```

IJPOINT 31 1 5 2.6 179.999 1.36 11
      32 7 5 2.6 60. 1.36 11
      33 15 5 2.6 -100. 1.36 11
      34 19 5 2.6 -179.999 1.36 11
      39 0 0 0.0 0.0 1.36 11

```

```

CIRCLE 1,2,9 : 2,3,9 : 3,4,9
CIRCLE 21,22,29 : 22,23,29 : 23,24,29
CIRCLE 31,32,39 : 32,33,39 : 33,34,39

```

```

SLINES 1,21,31

```

```

SLINES 4,24,34

```

```

KSSHELL 1 34 1 4M.05 4M0. 1 FSH

```

```

MESH 2

```

```

MERGE TYPE=FSH

```

```

REMARK '*****
REMARK 'SPACE SHUTTLE MAIN ENGINE HIGH PRESSURE FUEL TURBO PUMP (HPFTP)
REMARK 'SUPPORT STRUCTURE MESH
REMARK '*****

```


DEFSYS 1 1 3MO.0, 1.0,0.0,0.0 0.0,1.0,0.0 #CYLINDRICAL COORD SYSTEM

REMARK ' *****
REMARK ' MESH 12 - CIRCULAR FLANGE
REMARK ' *****

IJPOINT 1 1 1 3.70 0.0 0.2
2 2 1 2.84 0.0 0.2
3 2 2 2.84 0.0 0.78
4 3 2 2.60 0.0 0.78
5 3 3 2.60 0.0 1.36
6 1 3 3.70 0.0 1.36

SLINES 1T6,1
IJSOLID 0 0 1 HSO
PRISM 19 0.,0.,0. 3 360.

KNAME 6 6 19 19 FLNG NOD9
KNAME 6 6 3 3 FLNG ND10
KNAME 6 6 5 5 FLNG ND11
KNAME 6 6 14 14 FLNG NOD5
KNAME 6 6 15 15 FLNG NOD6
KNAME 6 6 16 16 FLNG NOD7
KNAME 6 6 17 17 FLNG NOD8
MESH 0 1
ROTATE -10. 3
ROTATE 90. 2
TRANS -6.24 2
TRANS 8.59 1
TRANS 4.24 3
MERGE/PRI mesh=%ipp(9)
merge/pri type=Fsh

REMARK ' *****
REMARK ' MESH 13 - SUPPORT STRUCTURE BASE
REMARK ' *****

IJPOINT 1 1 1 10.86 0.0 -2.811
11 2 1 10.45 -2.54 -2.811
2 4 1 9.76 -6.65 -2.811
3 7 1 3.57 -10.15 -2.811
4 9 1 0.00 -10.15 -2.811
5 9 2 9.825 -90.0 -2.811 1
6 1 2 9.825 6.0 -2.811 1
100 0 0 0.0 0.0 -2.811

SLINES 1,2,3,4,5
CIRCLE 5,6,100
SLINE 6,1
SLINES

IJSOLID 0 0 1 HSO
PRISM 3 0.,0.,1.23
KNAME 11 11 3 3 BASE NOD1
KNAME 2 2 3 3 BASE NOD2
KNAME 3 3 3 3 BASE NOD3
KNAME 4 4 3 3 BASE NOD4
MESH
assign tol x=.002
merge mesh=3

SET SYNTAX ON

REMARK ' *****
REMARK ' MESH 14 - SHELL ELEMENTS BETWEEN MESH 12 AND 13
REMARK ' *****

#####

SUBROUTINE XYZ1 - Author K. V. Pool April, 1987
#

SUBROUTINE XYZ1 RETURNS THE X,Y AND Z COORDINATES
OF THE FIRST ELEMENT IN THE NODLIST &NLST IN
THE VARIABLES &XX,&YY, AND &ZZ. THESE X, Y AND Z COORDINATES CAN BE

THIS SUBROUTINE CAN BE USED TO CREATE NEW IJPOINTS THAT HAVE COORDINATES
IDENTICAL TO EXISTING NODAL POINTS SO THAT NEW MESHES CAN BE GENERATED
THAT ARE BASED ON PREVIOUS MESHES THAT HAVE SINCE BEEN ROTATED AND
AND/OR TRANSLATED TO NEW POSITIONS.
#

AS AN EXAMPLE OF THE USAGE SEE [KPOOL.SSME.HPFTP]HPFTP-SS.MSH
#

SUB XYZ1 &NLST,&XX,&YY,&ZZ,&IPRT
#

&IPRT = PRINT CONTROL
= 0 FOR NORMAL PRINT
= 1 FOR EXTENDED PRINT
#

REMARK '
REMARK ' *****
REMARK ' SUBROUTINE XYZ1 HAS BEEN CALLED
;10 FORMAT '(5X,' NODE LIST NUMBER =',I5)
WRITE 6 ;10 &NLST

GET THE NODE LIST FILE

LET &IFN=%IFL(NLST.NV,0,&NLST) # FIND DATABASE FILE NUMBER OF NODE LIST

CHECK FOR IMPROPER NODE LIST (IFN=0)
IF &IFN 1,;ERR1,1
LET &LN=%LFM(&IFN,1) # LOCK FILE IN BLANK COMMON AND
RETURN ADDRESS IN &LN

LET &NODE=%IBC1(&LN,1) # RETRIEVE NUMBER OF FIRST NODE IN LIST
LET &XX=%XN(&NODE,1)
LET &YY=%XN(&NODE,2)
LET &ZZ=%XN(&NODE,3)

REMARK ' *****
IF &IPRT 1,;SKIP,1
;200 FORMAT '(5X,' NODE NUMBER =',I6)
WRITE 6 ;200 &NODE
REMARK ' X-COORD Y-COORD Z-COORD
;201 FORMAT '(5X,3F9.3)
WRITE 6 ;201 &XX,&YY,&ZZ

REMARK ' *****
;SKIP NOP
RETURN
;ERR1 REMARK 'IMPROPER NODE LIST REFERENCED

```
;400 FORMAT '(5X,' NODE LIST =',I5)
WRITE 6 ;400 &NLST
RETURN
END
```

```
#
#####
NLIST 1 INSERT NAME=BASE,NOD1
NLIST 2 INSERT NAME=BASE,NOD2
NLIST 3 INSERT NAME=BASE,NOD3
NLIST 4 INSERT NAME=BASE,NOD4
NLIST 5 INSERT NAME=FLNG,NOD5
NLIST 6 INSERT NAME=FLNG,NOD6
NLIST 7 INSERT NAME=FLNG,NOD7
NLIST 8 INSERT NAME=FLNG,NOD8
NLIST 9 INSERT NAME=FLNG,NOD9
NLIST 10 INSERT NAME=FLNG,ND10
NLIST 11 INSERT NAME=FLNG,ND11
```

```
CALL XYZ1 1 &XX &YY &ZZ 1
IJPOINT 1 1 1 &XX,&YY,&ZZ
```

```
CALL XYZ1 2 &XX &YY &ZZ 1
IJPOINT 2 3 1 &XX,&YY,&ZZ
IJPOINT 102 4 1 &XX,&YY,&ZZ
```

```
CALL XYZ1 3 &XX &YY &ZZ 1
IJPOINT 3 7 1 &XX,&YY,&ZZ
```

```
CALL XYZ1 4 &XX &YY &ZZ 1
IJPOINT 4 9 1 &XX,&YY,&ZZ
```

```
CALL XYZ1 5 &XX &YY &ZZ 1
IJPOINT 5 9 4 &XX,&YY,&ZZ
```

```
CALL XYZ1 6 &XX &YY &ZZ 1
IJPOINT 6 8 4 &XX,&YY,&ZZ
```

```
CALL XYZ1 7 &XX &YY &ZZ 1
IJPOINT 7 7 4 &XX,&YY,&ZZ
```

```
CALL XYZ1 8 &XX &YY &ZZ 1
IJPOINT 8 6 4 &XX,&YY,&ZZ
IJPOINT 108 5 4 &XX,&YY,&ZZ
IJPOINT 208 4 4 &XX,&YY,&ZZ
```

```
CALL XYZ1 9 &XX &YY &ZZ 1
IJPOINT 9 3 4 &XX,&YY,&ZZ
```

```
CALL XYZ1 10 &XX &YY &ZZ 1
IJPOINT 10 2 4 &XX,&YY,&ZZ
```

```
CALL XYZ1 11 &XX &YY &ZZ 1
IJPOINT 11 1 4 &XX,&YY,&ZZ
```

```
SLINES 1,2,102,3,4,5,6,7,8,108,208,9,10,11,1
SLINES 102 208:3,7
```

```
KSSHLL 1 5 1 .5 .5 .5 .5 0.0 0.0 0.0 0.0 1 FSH 0 -1
MESH 2
```

```

mset 99,copy,type=HS0
mset 99,delete,mesh=1t6
MERGE mset=99

```

```

REMARK '
  NSET 11,COPY,NAME=OUTR,VANE
  NSET 11,INSERT,NAME=INSD,VANE
  MSET 11,COPY,NSET=11

```

```

REMARK '
REMARK ' 15 VANE MESHES - MESHES 15 THRU 29 (CLOCKWISE FROM 0 DEGREES)

```

```

REMARK ' *****
REMARK ' *****

```

```

DEFSYS 1 1 3M0.0, 1.0,0.0,0.0 0.0,1.0,0.0 #CYLINDRICAL COORD SYSTEM

```

```

IJPOINT 1 1 2 3.230719 12.0 3.461722 1
        2 3 2 2.726711 24.0 3.030447 1
        3 5 2 2.324505 36.0 2.503693 1
IJPOINT 4 1 8 3.888425 12.0 2.579901 1
        5 3 8 3.438335 24.0 2.194444 1
        6 5 8 3.171350 36.0 1.664181 1

```

```

#####

```

```

IJPOINT 7 1 1 3.184 12.0 3.529 1
        8 3 1 2.638 24.0 3.143 1
        9 5 1 2.277 36.0 2.532 1
IJPOINT 10 1 9 3.967 12.0 2.512 1
        11 3 9 3.575 24.0 2.108 1
        12 5 9 3.267 36.0 1.666 1
        13 1 3
        14 3 3
        15 5 3
        16 1 7
        17 3 7
        18 5 7

```

```

SLINE 7,8,9,3,6,12,11,10,4,1,7:8,2,5,11:1,2,3:4,5,6

```

```

KSSHELL 7 2 1 .052 .214 .590 .428 4M0. 1 FSH 0 0 0 0. VANE
KSSHELL 8 3 1 .214 .052 .428 .590 4M0. 1 FSH 0 0 0 0. VANE
KSSHELL 1 14 1 .428 .590 .214 .052 4M0. 1 FSH 0 0 0 0. VANE
KSSHELL 2 15 1 .590 .428 .052 .214 4M0. 1 FSH 0 0 0 0. VANE
KSSHELL 13 17 1 .052 .214 .214 .052 4M0. 1 FSH 0 0 0 0. VANE
KSSHELL 14 18 1 .214 .052 .052 .214 4M0. 1 FSH 0 0 0 0. VANE
KSSHELL 16 5 1 .052 .214 .590 .428 4M0. 1 FSH 0 0 0 0. VANE
KSSHELL 17 6 1 .214 .052 .428 .590 4M0. 1 FSH 0 0 0 0. VANE
KSSHELL 4 11 1 .428 .590 .214 .052 4M0. 1 FSH 0 0 0 0. VANE
KSSHELL 5 12 1 .590 .428 .052 .214 4M0. 1 FSH 0 0 0 0. VANE

```

```

MESH

```

```

ROTATE -90. 3

```

```

mirror 1

```

```

ASSIGN TOLX=.002

```

```

MERGE MSET=11

```

```

MSET 80,COPY,MESH=%IPP(9)

```

```

LET &ANG = 24.

```

```

DO ;END3 &I = 1 14

```

```

DITTO MSET=80

```

```

ROTATE &ANG 3

```

```

MERGE MSET=11

```

```

LET &ANG = &ANG + 24.

```

```

;END3 CONTINUE

```

```

ASSIGN TOLX=.001

```

```

MSET 22,COPY,NAME=VANE

```

```

MSET 33,COPY,NAME=EDGE

```

```

# ELTNAME QUAD,,,,,VOLUME,0.,10000.,89.,181.,-1000.,1000.,4
REMARK ' *****
REMARK ' SUPPRESSIONS
REMARK ' *****
DOFSUP 0 NAME=OUTR,BOLT
DOFLOOS
FINISH
STOP
$ BAND
START -1
REGPS
BAND
STOP
$SETUP
START -1
SETUP
STOP
$MATL
START -1
#
REMARK ' MATL #1 - TITANIUM 5A1 - 2.5Sn ELI - MESH 1,2,3,4
MATISO 1 .155E8 .35 3.E-6 0.
DENSITY 1 4.2E-4 #.162/386.088
#
#
MATL
STOP
$LOAD
START -1
SET SYNTAX ON
SET ECHO ON
LCLEAR 1
PSURF 1. 1 1 NAME=,,SHLL,PRES
PSURF 1. 1 1 MESH=7
PSURF 1. 1 1 MESH=10
PSURF -1. 1 -1 MESH=11
PSURF -1. 1 5 NAME=,,INNER,PRES
PSURF -1. 1 1 NAME=,,OUTR,PRES
PSURF -1. 1 1 NAME=MSHB,PRES
PSURF -1. 1 4 NAME=MSHC,PRES
PSURF -1. 1 1 NAME=MSH5,,,PRES
PSURF -1. 1 1 NAME=MSH4,,,PRES
LCLEAR 2

REMARK ' MESH 1 NEW LOADS

MSET 1 COPY MESH 1
NSET 1 COPY NAME P208,FAC1
MSET 1 MASK NSET 1
MSET 1 DELE ELEM 11T1403B48
MSET 1 DELE ELEM 12T1404B48
PSURF -208. 1 1 MSET 1

MSET 2 COPY MESH 1
NSET 2 COPY NAME P208,FAC2
MSET 2 MASK NSET 2
MSET 2 DELE ELEM 11T1403B48
MSET 2 DELE ELEM 12T1404B48
PSURF -208. 1 2 MSET 2

```

MSET 4 COPY MESH 1
NSET 4 COPY NAME P208,FAC4
MSET 4 MASK NSET 4
MSET 4 DELE ELEM 11T1403B48
MSET 4 DELE ELEM 12T1404B48
PSURF -208. 1 4 MSET 4

REMARK ' MESH 2 NEW LOADS

MSET 1 COPY MESH 2
NSET 1 COPY NAME P208,FAC1
MSET 1 MASK NSET 1
MSET 1 DELE ELEM 1464T3784B80
MSET 1 DELE ELEM 1476T3796B80
PSURF -208. 1 1 MSET 1

MSET 4 COPY MESH 2
NSET 4 COPY NAME P208,FAC4
MSET 4 MASK NSET 4
MSET 4 DELE ELEM 1464T3784B80
MSET 4 DELE ELEM 1476T3796B80
PSURF -208. 1 4 MSET 4

MSET 5 COPY MESH 2
NSET 5 COPY NAME P208,FAC5
MSET 5 MASK NSET 5
MSET 5 DELE ELEM 1464T3784B80
MSET 5 DELE ELEM 1476T3796B80
PSURF -208. 1 5 MSET 5

MSET 1 COPY MESH 2
NSET 1 COPY NAME P438,FAC1
MSET 1 MASK NSET 1
MSET 1 DELE ELEM 1490T3810B80
MSET 1 DELE ELEM 1504T3824B80
PSURF -1438. 1 1 MSET 1

MSET 5 COPY MESH 2
NSET 5 COPY NAME P438,FAC5
MSET 5 MASK NSET 5
MSET 5 DELE ELEM 1490T3810B80
MSET 5 DELE ELEM 1504T3824B80
PSURF -1438. 1 5 MSET 5

MSET 1 COPY ELEM 1507T3827B80
PSURF -1488. 1 1 MSET 1

#1488 PSI

MSET 1 COPY ELEM 1508T3828B80
PSURF -1546. 1 1 MSET 1

#1546 PSI

MSET 1 COPY ELEM 1509T3829B80
PSURF -1604. 1 1 MSET 1

#1604 PSI

MSET 1 COPY ELEM 1510T3830B80
PSURF -1662. 1 1 MSET 1

#1662 PSI

MSET 2 COPY ELEM 1502T3822B80
PSURF -1721. 1 2 MSET 2

#1721 PSI

MSET 2 COPY ELEM 1495T3815B80
PSURF -1777. 1 2 MSET 2

#1777 PSI

MSET 5 COPY MESH 2
NSET 5 COPY NAME P777,FAC5
MSET 5 MASK NSET 5
PSURF -1777. 1 5 MSET 5

REMARK ' MESH 3 NEW LOADS

MSET 5 COPY MESH 3
NSET 5 COPY NAME P777,FAC5
MSET 5 MASK NSET 5
MSET 5 DELE ELEM 3841T4914B37
PSURF -1777. 1 5 MSET 5

MSET 4 COPY MESH 3
NSET 4 COPY NAME P500,FAC4
MSET 4 MASK NSET 4
PSURF -500. 1 4 MSET 4

MSET 5 COPY MESH 3
NSET 5 COPY NAME P500,FAC5
MSET 5 MASK NSET 5
PSURF -500. 1 5 MSET 5

MSET 5 COPY MESH 3
NSET 5 COPY NAME P19K,FAC5
MSET 5 MASK NSET 5
MSET 5 DELE ELEM 3869T4942B37
MSET 5 DELE ELEM 3871T4944B37
PSURF -19069. 1 5 MSET 5

REMARK ' POINT LOADS

P 272.3 3 NAME INNR,BOLT

MSET 4 COPY MESH 3
NSET 4 COPY NAME P334,FAC4
MSET 4 MASK NSET 4
PSURF -3349. 1 4 MSET 4

#DIFFUSER PILOT LOAD 51,424 LBS/2PI*R*H +500 PSI

#R=6.247499 H=.46 IN. (SEE IJPOINT 57,58 ABOVE)

LOAD
STOP
\$ SOLVE
START -1
SET ECHO ON
LOADS 1 303.0
LOADS 2 1.0
ASSIGN IMPR=1
SAVE R
SAVE D
SAVE S
SAVE EF
FILE K [4]KE
FILE KG [4]KG
FILE KI [4]KI
SOLVE 0
TOC

```

STOP
$SCOPE
START 200000
META OPEN
DEVICE OPEN QMS
SET ECHO ON
TITLE
CATT NUMB SIZE .1
CATT TITL SIZE .3
CATT TEXT SIZE .25
TITLE1 'HPFTP - INLET HOUSING GLOBAL MODEL - VANES
GEOM HIDE
LABEL ON ELEM
PLOT MESH 15T29
STOP
$ UTILITY PROCESSOR
START -1
OPEN 8 'BCD1
BCDOUT/UNFORMAT=VAX 8 MATL.EV
BCDOUT/UNFORMAT=VAX      8 ELEM.EV
BCDOUT/UNFORMAT=VAX      8 INTO.EV
BCDOUT/UNFORMAT=VAX      8 X.NV
BCDOUT/UNFORMAT=VAX      8 NORM.NV
BCDOUT/UNFORMAT=VAX      8 ROT.NV
BCDOUT/UNFORMAT=VAX      8 SKEW.NV
BCDOUT/UNFORMAT=VAX      8 DOF.NV
BCDOUT/UNFORMAT=VAX      8 NAME.NV
BCDOUT/UNFORMAT=VAX      8 NAME.EV
BCDOUT/UNFORMAT=VAX      8 IR.NV
BCDOUT/UNFORMAT=VAX      8 IER.NV
BCDOUT/UNFORMAT=VAX      8 LCS.NV
BCDOUT/UNFORMAT=VAX      8 PCT.HED.MESH
BCDOUT/UNFORMAT=VAX      8 MESH.HED 0 ?
BCDOUT/UNFORMAT=VAX      8 CON.RM.DIR
BCDOUT/UNFORMAT=VAX      8 CON.CON 0 ?
BCDOUT/UNFORMAT=VAX      8 UL.SV 0 ?
BCDOUT/UNFORMAT=VAX      8 EDF.NV 0 0
BCDOUT/UNFORMAT=VAX      8 SDF.NV 0 0
BCDOUT/UNFORMAT=VAX      8 STLT.RM.DIR
BCDOUT/UNFORMAT=VAX      8 D.SV 0 1
BCDOUT/UNFORMAT=VAX      8 S.EIP 0 1
BCDOUT/UNFORMAT=VAX      8 EF.SEV 0 ?
BCDOUT/UNFORMAT=VAX      8 UT.NV 0 ?
BCDOUT/UNFORMAT=VAX      8 HEAD.COM 0 ?
BCDOUT/UNFORMAT=VAX      8 POLY.EV 0 ?
BCDOUT/UNFORMAT=VAX      8 POLY.RM 0 ?
BCDOUT/UNFORMAT=VAX      8 EDGE.RM 0 ?
BCDOUT/UNFORMAT=VAX      8 EDGE.EV 0 ?
BCDOUT/UNFORMAT=VAX      8 SYS.CRM
TOC
STOP
/EOF

```


Appendix B

FINAL HPFTP INLET HOUSING DETAILED VANE SUBMODEL
DIAL FINITE ELEMENT MODEL RUNSTREAM

```

JOB, JN=VANE2, T=300, MFL=1500000, US=670535.
ACCOUNT, AC=3, UPW=.
FETCH, DN=MESH, DF=TR, TEXT='DIAL$CRAY:MESH.CEX'.
FETCH, DN=BAND, DF=TR, TEXT='DIAL$CRAY:BAND.CEX'.
FETCH, DN=SETUP, DF=TR, TEXT='DIAL$CRAY:SETUP.CEX'.
FETCH, DN=UTILITY, DF=TR, TEXT='DIAL$CRAY:UTILITY.CEX'.
MESH.
BAND.
SETUP.
UTILITY.
DISPOSE, DN=FT08, DF=BB, TEXT='VANE2.U08'.
BAD.
EXIT.
DISPOSE, DF=TR, DN=FILO02, TEXT='VANE2.FL2'.
/EOF
$SD VANE
$AS VANE2.FL2 FILO02
$AS VANE2MESH.OUT FOR006
$RUN USER$DISK2: [DIAL.EXEL3D2]MESH
CLEAR 200000
MAX/MXP0=2000      10000 2500
ELTYPE 4,2,6
#-----
# DETAILED VANE MODEL WITH TORUS OF SSME HPFTP
#-----
#-- CONCAVE SURFACE TOROIDAL SYSTEM AND CONSTRAINT SURFACE 1 R=1.86 ----
DEFSYS 1 3 PT1=2MO. 4.903 PT2=10. 0. 4.903 PT3=0. 10. 4.903 R=2.055
DEFSUR 1 1 1 R=1.86
      58 1 1 1.954
      59 1 1 2.048
#-- CONCAVE SURFACE TOROIDAL SYSTEM AND CONSTRAINT SURFACE 2 R=3.037 ----
DEFSYS 2 3 PT1=2MO. .935 PT2=10. 0. .935 PT3=0. 10. .935 R=4.925
DEFSUR 2 2 1 R=3.037
      68 2 1 2.943
      69 2 1 2.849
#-- CONCAVE SURFACE TOROIDAL SYSTEM AND CONSTRAINT SURFACE 3 PHI=35 ----
DEFSYS 3 3 2MO. 1.3990682 10. 0. 1.3990682 0. 10. 1.3990682
DEFSUR 3 3 3 PHI=35.
#-- CONCAVE SURFACE TOROIDAL SYSTEM AND CONSTRAINT SURFACE 4 PHI=42.8012089
DEFSYS 4 3 2MO. .7196471 10. 0. .7196471 0. 10. .7196471
DEFSUR 4 4 3 PHI=42.8012089
#-- CONCAVE SURFACE TOROIDAL SYSTEM AND CONSTRAINT SURFACE 5 R=.5 ----
DEFSYS 5 3 2MO. 2.8958631 10. 0. 2.8958631 0. 10. 2.8958631 R=1.85
DEFSUR 5 5 1 R=.5
#-- CONCAVE SURFACE TOROIDAL SYSTEM AND CONSTRAINT SURFACE 6 R=3.147 ----
DEFSYS 6 3 PT1=2MO. .935 PT2=10. 0. .935 PT3=0. 10. .935 R=4.925
DEFSUR 6 6 1 R=3.147
#-----
#-- CONVEX SURFACE TOROIDAL SYSTEM AND CONSTRAINT SURFACE 7 R=1.3 ----
#DEFSYS 7 3 PT1=2MO. 1.394 PT2=10. 0. 1.394 PT3=0. 10. 1.394 R=4.421
DEFSYS 7 3 2MO. 1.3827953 10. 0. 1.3827953 0. 10. 1.3827953 R=4.421
DEFSUR 7 7 1 R=1.3
      78 7 1 1.372
      79 7 1 1.444
#-- CONVEX SURFACE TOROIDAL SYSTEM AND CONSTRAINT SURFACE 8 R=1.5805887 --
DEFSYS 8 3 PT1=2MO. 1.247 PT2=10. 0. 1.247 PT3=0. 10. 1.247 R=4.66
DEFSUR 8 8 1 R=1.5805887
      88 8 1 1.6525887
      89 8 1 1.7245887
#-- CONVEX SURFACE TOROIDAL SYSTEM AND CONSTRAINT SURFACE 9 PHI=45 ---

```

```

DEFSYS 9 3 PT1=2MO. -1.612 PT2=10. 0. -1.612 PT3=0. 10. -1.612
DEFSUR 9 9 3 PHI=45.
#-- CONVEX SURFACE TOROIDAL SYSTEM AND CONSTRAINT SURFACE 10 PHI=75. ---
DEFSYS 10 3 2MO. -10.8824664 10. 0. -10.8824664 0. 10. -10.8824664
DEFSUR 10 10 3 PHI=75.
#-- CONCAVE SURFACE TOROIDAL SYSTEM AND CONSTRAINT SURFACE 90 PHI=-35.1303336 -
DEFSYS 90 3 2MO. 8.8960272 10. 0. 8.8960272 0. 10. 8.8960272
DEFSUR 90 90 3 PHI=-54.9592082
#-- CONCAVE SURFACE CYLINDRICAL SYSTEM AND CONSTRAINT SURFACE 91 R=2.030 --
DEFSYS 91 1 3MO. 10. 0. 0. 0. 10. 0.
DEFSUR 91 91 1 R=2.030
#-- CONCAVE SURFACE CARTESIAN SYSTEM AND CONSTRAINT SURFACE 92 Z=1.97 -----
DEFSUR 92 0 3 Z=1.97
#-- CONVEX SURFACE CYLINDRICAL SYSTEM AND CONSTRAINT SURFACE 93 R=4.155 --
DEFSUR 93 91 1 R=4.155
#-- CONCAVE SURFACE CARTESIAN SYSTEM AND CONSTRAINT SURFACE 94 Z=1.34 -----
DEFSUR 94 0 3 Z=1.34
#-- CONVEX SURFACE CYLINDRICAL SYSTEM AND CONSTRAINT SURFACE 95 R=4.195 --
DEFSUR 95 91 1 R=4.195
#-- CONCAVE SURFACE CARTESIAN SYSTEM AND CONSTRAINT SURFACE 96 Z=2.543 -----
DEFSUR 96 0 3 Z=2.543
#-----
#-- VANE -----
#-- SECTION Z-Z CYLINDRICAL SYSTEM AND CONSTRAINT SURFACE 11 R=.026 ----
DEFSYS 11 1 3.3140034 .6308132 3.3181209 3.3140034 0. 3.3181209>
      4.0211101 .6308132 4.0252277
DEFSUR 21 11 1 r=.026
      31 11 1 r=.07
      41 11 1 r=.214
#-- SECTION Z-Z CYLINDRICAL SYSTEM AND CONSTRAINT SURFACE 12 R=2. ----
DEFSYS 12 1 1.9884341 1.249205 1.9925517 1.9884341 0. 1.9925517>
      2.6955409 1.249205 2.6996589
DEFSUR 22 12 1 r=2.
      32 12 1 r=2.044
      42 12 1 r=2.188
#-- SECTION Z-Z CYLINDRICAL SYSTEM AND CONSTRAINT SURFACE 13 R=3.471 -
DEFSYS 13 1 1.1739069 2.1640446 1.1780244 1.1739069 0. 1.1780244>
      1.8810136 2.1640446 1.8851312
DEFSUR 23 13 1 R=3.471
      33 13 1 r=3.515
      43 13 1 r=3.659
#-- SECTION Z-Z CYLINDRICAL SYSTEM AND CONSTRAINT SURFACE 14 R=.026 -
DEFSYS 14 1 2.4241186 -.7926370 2.4282361 2.4241186 -1.7926370 2.4282361>
      3.1312254 -.7926370 3.1353429
DEFSUR 24 14 1 R=.026
      34 14 1 r=.07
      44 14 1 r=.214
#-- SECTION Y-Y LOCAL PLANE SYSTEM AND CONSTRAINT SURFACE 15 ----
DEFSYS 15 0 2.9196439 0. 2.9237614 1.9196439 -1.5995893 1.9237614>
      3.9196439 0. 1.9237614
DEFSUR 15 15 3 z=0.
      25 15 3 z=-.026
      35 15 3 z=-.07
      45 15 3 z=-.214
      55 15 3 z=-.0525
      65 15 3 z=-.17
#-----
#-- SECTION Y-Y LOCAL PLANE SYSTEM AND CONSTRAINT SURFACE 16 R=.026 --
DEFSYS 16 1 3.7453632 .5086961 2.7340754 3.7453632 0. 2.7340754>
      4.4524700 .5086961 3.4411822

```

```

DEFSUR 26 16 1 _r=.026
      36 16 1 _r=.0525
      46 16 1 _r=.17
#-- SECTION Y-Y CYLINDRICAL SYSTEM AND CONSTRAINT SURFACE 12 R=2. ----
DEFSYS 17 1 2.4282407 1.1621884 1.4169529 2.4282407 0. 1.4169529>
      3.1353475 1.1621884 2.1240597
DEFSUR 27 17 1 _r=2.
      37 17 1 _r=2.0265
      47 17 1 _r=2.144
#-- SECTION Y-Y CYLINDRICAL SYSTEM AND CONSTRAINT SURFACE 13 R=3.275 -
DEFSYS 18 1 1.7390335 1.9841446 .7277457 1.7390335 0. .7277457>
      2.4461402 1.9841446 1.4348524
DEFSUR 28 18 1 _R=3.275
      38 18 1 _r=3.3015
      48 18 1 _r=3.419
#-- SECTION Y-Y CYLINDRICAL SYSTEM AND CONSTRAINT SURFACE 14 R=.026 -
DEFSYS 19 1 2.9318213 -.7926370 1.9205335 2.9318213 -1.7926370 1.9205335>
      3.6389280 -.7926370 2.6276403
DEFSUR 29 19 1 _R=.026
      39 19 1 _r=.0525
      49 19 1 _r=.17

#-----
#-----
#----- MESH 1 - VANE -----
#----- STATION 1 - BOUNDARY AT CONCAVE SURFACE SIDE ---
IJPOIN 101 1 1 _R=.214 _THETA=138.5197667 _Z=.320 11 3 15 41
ASSIGN TOLX=0.005
IJPOIN 102 3 1 .214 -140. .320 11 3 4 41
ASSIGN TOLX=0.001
IJPOIN 103 5 1 .214 -131.4802333 .320 11 4 41 45
IJPOIN 104 13 1 _x=-.2 _y=-.320 _z=-.214 15 4 45
ASSIGN TOLX=0.005
IJPOIN 122 19 1 _x=.3958574 -.320 -.214 15 4 5 45
IJPOIN 123 23 1 _x=.7665687 -.320 -.214 15 5 6 45
ASSIGN TOLX=0.001
IJPOIN 105 25 1 _r=.214 -131.4802333 .320 14 6 44 45
      106 29 1 .214 -41.4802333 .320 14 6 15 44
      107 29 3 _x=1.058 -.320 0. 15 5 15
ASSIGN TOLX=0.005
IJPOIN 108 29 5 .214 -41.4802333 .320 14 6 15 44
IJPOIN 109 27 5 .214 -5.5 .320 14 5 6 44
IJPOIN 110 25 5 .214 30.8790069 .320 14 5 43 44
ASSIGN TOLX=0.001
IJPOIN 124 23 5 3.659 34.0043818 .320 13 4 5 43
IJPOIN 125 17 5 3.659 43. .320 13 4 43
ASSIGN TOLX=0.001
IJPOIN 111 13 5 3.659 51.5437539 .320 13 4 42 43
      112 11 5 2.188 54.9443595 .320 12 3 4 42
IJPOIN 113 5 5 2.188 69.3596831 .320 12 3 42
IJPOIN 114 3 5 2.188 71.7436894 .320 12 3 41 42
IJPOIN 115 1 5 .214 138.5197667 .320 11 3 15 41
      116 1 3 _x=-.842 -.320 0. 15 3 15
      117 3 3 _x=-.842 -.320 0. 15 3 15
      118 5 3 _x=-.842 -.320 0. 15 3 15
      119 13 3 _x=-.2 -.320 0. 15 4 15
      120 25 3 _x=1.058 -.320 0. 15 5 15
      121 27 3 _x=1.058 -.320 0. 15 5 15
#----- STATION 2 - INTERSECTION OF THE VANE AND CONCAVE SURFACE ---
ASSIGN TOLX=0.005
IJPOIN 201 1 1 _R=.214 _THETA=138.5197667 _Z=.175 11 1 15 41

```

```

IJPOIN 202 3 1 .214 -150.3004833 .175 11 1 2 41
ASSIGN TOLX=0.001
IJPOIN 203 5 1 .214 -131.4802333 .175 11 2 41 45
      204 13 1 _x=-.2 _y=-.175 _z=-.214 15 2 45
IJPOIN 222 19 1 _x=.3958574 -.175 -.214 15 2 45
IJPOIN 223 23 1 _x=.7665687 -.175 -.214 15 2 45
      205 25 1 _r=.214 -131.4802333 .175 14 2 44 45
      206 29 1 .214 -41.4802333 .175 14 2 44
      207 29 3 _x=1.058 -.175 0. 15 2 15
      208 29 5 .214 -41.4802333 .175 14 2 44
      209 27 5 .214 -5.5 .175 14 2 44
      210 25 5 .214 30.8790069 .175 14 2 43 44
      224 23 5 3.659 35. .175 13 2 43
      225 17 5 3.659 45. .175 13 2 43
ASSIGN TOLX=0.005
IJPOIN 211 13 5 3.659 51.5437539 .175 13 2 42 43
      212 11 5 2.188 53.9324362 .175 12 1 2 42
ASSIGN TOLX=0.001
IJPOIN 213 5 5 2.188 69.3596831 .175 12 1 42
IJPOIN 214 3 5 2.188 71.7436894 .175 12 1 41 42
IJPOIN 215 1 5 .214 138.5197667 .175 11 1 15 41
      216 1 3 _x=-.842 -.175 0. 15 1 15
      217 3 3 _x=-.842 -.175 0. 15 1 15
      218 5 3 _x=-.842 -.175 0. 15 1 15
      219 13 3 _x=-.2 -.175 0. 15 2 15
      220 25 3 _x=1.058 -.175 0. 15 2 15
      221 27 3 _x=1.058 -.175 0. 15 2 15
#----- STATION 3 - FILLET OF THE VANE AND CONCAVE SURFACE ---
IJPOIN 301 1 1 R=.120 _THETA=138.5197667 _Z=.090 11 58 15 31
ASSIGN TOLX=0.005
IJPOIN 302 3 1 .120 -150.3004833 .090 11 58 31
IJPOIN 303 5 1 .120 -131.4802333 .090 11 58 68 35
ASSIGN TOLX=0.001
IJPOIN 304 13 1 _x=-.2 _y=-.090 _z=-.120 15 68 35
      305 25 1 _r=.120 -131.4802333 .090 14 68 34 35
      306 29 1 .120 -41.4802333 .090 14 68 34
      307 29 3 _x=1.058 -.090 0. 15 68 15
      308 29 5 .120 -41.4802333 .090 14 68 34
      309 27 5 .120 -5.5 .090 14 68 34
      310 25 5 .120 30.8790069 .090 14 68 33 34
ASSIGN TOLX=0.001
IJPOIN 311 13 5 3.515 51.5437539 .090 13 68 32 33
      312 11 5 2.044 59. .090 12 58 68 32
ASSIGN TOLX=0.001
IJPOIN 313 5 5 2.094 70.9043343 .090 12 58 32
IJPOIN 314 3 5 2.094 71.7436894 .090 12 58 31 32
IJPOIN 315 1 5 .120 138.5197667 .090 11 58 15 31
      316 1 3 _x=-.842 -.090 0. 15 58 15
      317 3 3 _x=-.842 -.090 0. 15 58 15
      318 5 3 _x=-.842 -.090 0. 15 58 15
      319 13 3 _x=-.2 -.090 0. 15 68 15
      320 25 3 _x=1.058 -.090 0. 15 68 15
      321 27 3 _x=1.058 -.090 0. 15 68 15
#----- STATION 4 - THE VANE SECTION NEAR CONCAVE SURFACE ---
IJPOIN 401 1 1 R=.026 _THETA=138.5197667 _Z=.009 11 59 15 21
ASSIGN TOLX=0.007
IJPOIN 402 3 1 .026 -150. .009 11 59 21
IJPOIN 403 5 1 .026 -131.4802333 .009 11 59 69 25
ASSIGN TOLX=0.001
IJPOIN 404 13 1 _x=-.2 _y=-.009 _z=-.026 15 69 25

```

405	25	1	r=.026	-131.4802333	.009	14	69	24	25
406	29	1	.026	-41.4802333	.009	14	69	24	
407	29	3	x=1.058	-.009	0.	15	69	15	
408	29	5	.026	-41.4802333	.009	14	69	24	
409	27	5	.026	-5.5	.009	14	69	24	
410	25	5	.026	30.8790069	.009	14	69	23	24
ASSIGN TOLX=0.001									
IJPOIN	411	13	5	3.471	51.5437539	.009	13	69	22 23
	412	11	5	2.000	60.	.009	12	59	69 22
ASSIGN TOLX=0.001									
IJPOIN	413	5	5	2.000	71.4244601	.009	12	59	22
IJPOIN	414	3	5	2.000	71.7436894	.009	12	59	21 22
IJPOIN	415	1	5	.026	138.5197667	.009	11	59	15 21
	416	1	3	x=-.842	-.009	0.	15	59	15
	417	3	3	x=-.842	-.009	0.	15	59	15
	418	5	3	x=-.842	-.009	0.	15	59	15
	419	13	3	x=-.2	-.009	0.	15	69	15
	420	25	3	x=1.058	-.009	0.	15	69	15
	421	27	3	x=1.058	-.009	0.	15	69	15
#----- STATION 5 - THE VANE SECTION NEAR CONVEX SURFACE ----									
ASSIGN TOLX=0.001									
IJPOIN	501	1	1	R=.026	THETA=138.5197667	Z=-.030	16	79	15 26
IJPOIN	502	3	1	.026	-150.	-.030	16	79	26
IJPOIN	503	5	1	.026	-131.4802333	-.030	16	79	26 25
IJPOIN	504	13	1	x=0.	y=.748	z=-.026	15	79	25
ASSIGN TOLX=0.0058									
IJPOIN	522	19	1	x=.6	.748	-.026	15	79	89 25
ASSIGN TOLX=0.001									
IJPOIN	505	25	1	r=.026	-131.4802333	-.030	19	89	29 25
	506	29	1	.026	-41.4802333	-.030	19	89	29
	507	29	3	x=1.058	.748	0.	15	89	15
	508	29	5	.026	-41.4802333	-.030	19	89	29
IJPOIN	509	27	5	.026	-5.5	-.030	19	89	29
IJPOIN	510	25	5	.026	30.8790069	-.030	19	89	28 29
ASSIGN TOLX=0.0058									
IJPOIN	511	19	5	3.275	36.	-.030	18	79	89 28
ASSIGN TOLX=0.001									
IJPOIN	512	13	5	2.000	49.8589617	-.030	17	79	27 28
IJPOIN	513	5	5	2.000	70.3646510	-.030	17	79	27
IJPOIN	514	3	5	2.000	70.6675	-.030	17	79	26 27
IJPOIN	515	1	5	.026	138.5197667	-.030	16	79	15 26
	516	1	3	x=-.679	.748	0.	15	79	15
	517	3	3	x=-.679	.748	0.	15	79	15
	518	5	3	x=-.679	.748	0.	15	79	15
	519	13	3	x=0.	.748	0.	15	79	15
	520	25	3	x=1.058	.748	0.	15	89	15
	521	27	3	x=1.058	.748	0.	15	89	15
#----- STATION 6 - FILLET OF THE VANE SECTION AT CONVEX SURFACE ----									
IJPOIN	601	1	1	R=.0525	THETA=138.5197667	Z=-.030	16	78	15 36
IJPOIN	602	3	1	.0525	-160.	-.030	16	78	36
IJPOIN	603	5	1	.0525	-131.4802333	-.030	16	78	36 55
IJPOIN	604	13	1	x=0.	y=.748	z=-.0525	15	78	55
ASSIGN TOLX=0.0058									
IJPOIN	622	19	1	x=.52	.748	-.0525	15	78	88 55
ASSIGN TOLX=0.001									
IJPOIN	605	25	1	r=.0525	-131.4802333	-.030	19	88	39 55
	606	29	1	.0525	-41.4802333	-.030	19	88	15 39
	607	29	3	x=1.058	.748	0.	15	88	15
	608	29	5	.0525	-41.4802333	-.030	19	88	15 39
IJPOIN	609	27	5	.0525	-5.5	-.030	19	88	39

IJPOIN	610	25	5	.0525	30.8790069	-.030	19	88	38	39
ASSIGN TOLX=0.0058										
IJPOIN	611	21	5	3.3015	36.	-.030	18	78	88	38
ASSIGN TOLX=0.001										
IJPOIN	612	13	5	2.0525	49.8589617	-.030	17	78	37	38
IJPOIN	613	5	5	2.0525	69.3372175	-.030	17	78		37
IJPOIN	614	3	5	2.0525	70.6675	-.030	17	78	36	37
IJPOIN	615	1	5	.0525	138.5197667	-.030	16	78	15	36
	616	1	3	_x=-.679	.748	0.	15	78	15	
	617	3	3	_x=-.679	.748	0.	15	78	15	
	618	5	3	_x=-.679	.748	0.	15	78	15	
	619	13	3	_x=0.	.748	0.	15	78	15	
	620	25	3	_x=1.058	.748	0.	15	88	15	
	621	27	3	_x=1.058	.748	0.	15	88	15	
#----- STATION 7 - FILLET OF THE VANE SECTION AT CONVEX SURFACE ----										
ASSIGN TOLX=0.001										
IJPOIN	701	1	1	_R=.170	_THETA=138.5197667	_Z=-.150	16	7	15	46
IJPOIN	702	3	1	.170	-160.	-.150	16	7		46
IJPOIN	703	5	1	.170	-131.4802333	-.150	16	7	46	65
IJPOIN	722	7	1	_x=-.51	_y=.868	_z=-.150	15	7		65
ASSIGN TOLX=0.001										
IJPOIN	704	13	1	_x=0.	_y=.868	_z=-.150	15	7		65
ASSIGN TOLX=0.005705										
IJPOIN	723	17	1	_x=.381	.868	-.150	15	7	8	65
IJPOIN	724	19	1	_x=.5	.868	-.150	15	8		65
IJPOIN	705	25	1	_r=.170	-131.4802333	-.150	19	8	49	65
ASSIGN TOLX=0.001										
IJPOIN	706	29	1	.170	-41.4802333	-.150	19	8	15	49
	707	29	3	_x=1.058	.868	0.	15	8	15	
	708	29	5	.170	-41.4802333	-.150	19	8	15	49
ASSIGN TOLX=0.001										
IJPOIN	709	27	5	.170	-5.5	-.150	19	8		49
IJPOIN	710	25	5	.170	30.8790069	-.150	19	8	48	49
IJPOIN	725	23	5	3.419	34.	-.150	18	8		48
ASSIGN TOLX=0.0058										
IJPOIN	711	21	5	3.419	35.25	-.150	18	7	8	48
ASSIGN TOLX=0.001										
IJPOIN	726	19	5	3.419	40.	-.150	18	7		48
IJPOIN	712	13	5	2.144	49.8589617	-.150	17	7	47	48
IJPOIN	727	11	5	2.144	54.5	-.150	17	7		47
IJPOIN	728	9	5	2.144	59.	-.150	17	7		47
ASSIGN TOLX=0.005										
IJPOIN	713	5	5	2.144	68.8300281	-.150	17	7		47
IJPOIN	714	3	5	2.144	70.6675	-.150	17	7	46	47
ASSIGN TOLX=0.001										
IJPOIN	715	1	5	.170	138.5197667	-.150	16	7	15	46
	716	1	3	_x=-.679	.868	0.	15	7	15	
	717	3	3	_x=-.679	.868	0.	15	7	15	
	718	5	3	_x=-.679	.868	0.	15	7	15	
	719	13	3	_x=0.	.868	0.	15	7	15	
	720	25	3	_x=1.058	.868	0.	15	8	15	
	721	27	3	_x=1.058	.868	0.	15	8	15	
#----- STATION 8 - BOUNDARY AT CONVEX SURFACE SIDE ----										
ASSIGN TOLX=0.001										
IJPOIN	801	1	1	_R=.170	_THETA=138.5197667	_Z=-.425	16	9	15	46
IJPOIN	802	3	1	.170	-160.	-.425	16	9		46
IJPOIN	803	5	1	.170	-131.4802333	-.425	16	9		46
	822	7	1	_x=-.6353931	1.143	-.170	15	9		65
IJPOIN	804	13	1	_x=0.	_y=1.143	_z=-.170	15	9		65
ASSIGN TOLX=.005										

```

IJPOIN 823 19 1 _x=.5218596 1.143 -.170 15 9 10 65
IJPOIN 805 25 1 _r=.170 -131.4802333 -.425 19 10 49 65
ASSIGN TOLX=0.001
IJPOIN 806 29 1 .170 -41.4802333 -.425 19 10 15 49
      807 29 3 _x=1.058 1.143 0. 15 10 15
      808 29 5 .170 -41.4802333 -.425 19 10 15 49
ASSIGN TOLX=.001
IJPOIN 809 27 5 .170 -5.5 -.425 19 10 49
IJPOIN 810 25 5 .170 30.8790069 -.425 19 10 48 49
ASSIGN TOLX=0.001
IJPOIN 811 23 5 3.419 33.5646343 -.425 18 10 9 48
      824 19 5 3.419 41. -.425 18 9 48
IJPOIN 812 13 5 2.144 49.8589617 -.425 17 9 47 48
      825 11 5 2.144 52.7420319 -.425 17 9 47
      826 9 5 2.144 58. -.425 17 9 47
IJPOIN 813 5 5 2.144 68.8300281 -.425 17 9 47
IJPOIN 814 3 5 2.144 70.6675 -.425 17 9 46 47
IJPOIN 815 1 5 .170 138.5197667 -.425 16 9 15 46
      816 1 3 _x=-.679 1.143 0. 15 9 15
      817 3 3 _x=-.679 1.143 0. 15 9 15
      818 5 3 _x=-.679 1.143 0. 15 9 15
      819 13 3 _x=0. 1.143 0. 15 9 15
      820 25 3 _x=1.058 1.143 0. 15 10 15
      821 27 3 _x=1.058 1.143 0. 15 10 15

```

```

#-----
SINTER 101 102 : 102 103 : 103 104 : 104 122 : 122 123 : 123 105 : 105 106
      106 107 : 107 108 : 108 109 : 109 110 : 110 124 : 124 125 : 125 111
      111 112

```

```

      112 113 : 113 114 : 114 115 : 115 116 : 116 101 : 118 119 : 119 120
SLINES 117 117 : 121 121

```

```

#-----
IJGRID 1

```

```

SINTER 201 202 : 202 203 : 203 204 : 204 222 : 222 223 : 223 205
      205 206 : 206 207 : 207 208 : 208 209
      209 210 : 210 224 : 224 225 : 225 211 : 211 212 : 212 213
      213 214 : 214 215 : 215 216 : 216 201 : 218 219 : 219 220

```

```

SLINES 217 217 : 221 221

```

```

#-----
IJGRID 2

```

```

SINTER 301 302 : 302 303 : 303 304 : 304 305 : 305 306 : 306 307
      307 308 : 308 309 : 309 310 : 310 311 : 311 312 : 312 313
      313 314 : 314 315 : 315 316 : 316 301 : 318 319 : 319 320

```

```

SLINES 317 317 : 321 321

```

```

#-----
IJGRID 3

```

```

SINTER 401 402 : 402 403 : 403 404 : 404 405 : 405 406 : 406 407
      407 408 : 408 409 : 409 410 : 410 411 : 411 412 : 412 413
      413 414 : 414 415 : 415 416 : 416 401 : 418 419 : 419 420

```

```

SLINES 417 417 : 421 421

```

```

#-----
IJGRID 4

```

```

SINTER 501 502 : 502 503 : 503 504 : 504 522 : 522 505 : 505 506 : 506 507
      507 508 : 508 509 : 509 510 : 510 511 : 511 512 : 512 513
      513 514 : 514 515 : 515 516 : 516 501 : 518 519 : 519 520

```

```

SLINES 517 517 : 521 521

```

```

#-----
IJGRID 5

```

```

SINTER 601 602 : 602 603 : 603 604 : 604 622 : 622 605 : 605 606 : 606 607
      607 608 : 608 609 : 609 610 : 610 611 : 611 612 : 612 613
      613 614 : 614 615 : 615 616 : 616 601 : 618 619 : 619 620

```


SLINES 617 617 : 621 621

#-----
IJGRID 6
SINTER 701 702 : 702 703 : 703 722 : 722 704 : 704 723
723 724 : 724 705 : 705 706 : 706 707
707 708 : 708 709 : 709 710 : 710 725 : 725 711 : 711 726
726 712 : 712 727 : 727 728 : 728 713
713 714 : 714 715 : 715 716 : 716 701 : 718 719 : 719 720

SLINES 717 717 : 721 721

#-----
IJGRID 7
SINTER 801 802 : 802 803 : 803 822 : 822 804 : 804 823 : 823 805
805 806 : 806 807 : 807 808 : 808 809 : 809 810 : 810 811
811 824 : 824 812 : 812 825 : 825 826 : 826 813
813 814 : 814 815 : 815 816 : 816 801 : 818 819 : 819 820

SLINES 817 817 : 821 821

IJSOL 0 0 1 50

RULE 5 1
13 2 3
23 4
31 5 6
35 7

#-----
#KNAME 119 102 1 1 FACE IN CENT C
119 112 1 1 FACE IN CENT C
119 122 1 1 FACE IN CENT C
119 124 1 1 FACE IN CENT C
#KNAME 819 822 35 35 FACE OUT CENT C
819 825 35 35 FACE OUT CENT C
819 823 35 35 FACE OUT CENT C
819 811 35 35 FACE OUT CENT C
#-----

MESH

MERGE

NSET=1 COPY RANGE=3 19 1
NSET=1 INSE RANGE=32 40 1
NSET=1 INSE RANGE=47 62 1
NSET=1 INSE RANGE=69 76 1
NSET=1 INSE RANGE=88 100 1
NODNAM FACE IN CENT C 0 NSET=1
NSET=2 COPY RANGE=2455 2467 1
NSET=2 INSE RANGE=2481 2487 1
NSET=2 INSE RANGE=2495 2510 1
NSET=2 INSE RANGE=2517 2523 1
NSET=2 INSE RANGE=2536 2548 1
NODNAM FACE OUT CENT C 0 NSET=2

#----- MESH 2 - CONCAVE BOTTOM LEFT -----

#----- STATION 1 -----

IJPOIN	131	1	1	2.030	24.	1.97	91	91	92
	132	23	1	2.030	-30.	1.97	91	91	92
	133	23	3	3.147	-30.	156.9149353	6	6	91
	134	23	5	3.147	-30.	150.	6	6	
	106	19	5	.214	-41.4802333	.320	14	6	15 44
IJPOIN	105	15	5	r=.214	-131.4802333	.320	14	6	44 45

ASSIGN TOLX=0.005

IJPOIN	123	15	7	x=.7665687	-.320	-.214	15	5	6 45
	135	13	7	x=.7665687	-.320	-.214	15	5	6 45
IJPOIN	122	13	11	x=.3958574	-.320	-.214	15	4	5 45
	136	11	11	x=.3958574	-.320	-.214	15	4	5 45

ASSIGN TOLX=0.001

IJPOIN 104 11 17 _x=-.2 _y=-.320 _z=-.214 15 4 45
 137 9 17 _x=-.2 _y=-.320 _z=-.214 15 4 45
 IJPOIN 103 9 25 .214 -131.4802333 .320 11 4 41 45
 138 7 25 .214 -131.4802333 .320 11 4 41 45

ASSIGN TOLX=0.005

IJPOIN 102 7 27 .214 -140. .320 11 3 4 41
 IJPOIN 101 7 29 _R=.214 _THETA=138.5197667 _Z=.320 11 3 15 41

ASSIGN TOLX=0.001

IJPOIN 139 7 33 _R=4.3044512 _THATER=12.75 _PHI=35. 3 3 90

ASSIGN TOLX=0.001

IJPOIN 140 1 33 _R=4.3044512 _THATER=24. _PHI=35. 3 3 90
 141 1 29 3.950 24. 35. 3 3
 142 1 27 3.6725711 24. 35. 3 3 4
 IJPOIN 143 1 11 3.2028762 24. 42.8012089 4 4 5
 144 1 7 .5 24. -32.5248043 5 5 6
 145 1 5 3.147 24. 150. 6 6
 146 1 3 3.147 24. 156.9149353 6 6 91

#----- STATION 2 -----
 IJPOIN 231 1 1 3.037 24. 160.0745708 2 2 92
 232 23 1 3.037 -30. 160.0745708 2 2 92
 233 23 3 3.037 -30. 156. 2 2
 234 23 5 3.037 -30. 150. 2 2
 206 19 5 .214 -41.4802333 .175 14 2 44
 205 15 5 _r=.214 -131.4802333 .175 14 2 44 45
 IJPOIN 223 15 7 _x=.7665687 -.175 -.214 15 2 45
 IJPOIN 235 13 7 _x=.7665687 -.175 -.214 15 2 45
 IJPOIN 222 13 11 _x=.3958574 -.175 -.214 15 2 45
 IJPOIN 236 11 11 _x=.3958574 -.175 -.214 15 2 45
 204 11 17 _x=-.2 _y=-.175 _z=-.214 15 2 45
 237 9 17 _x=-.2 _y=-.175 _z=-.214 15 2 45
 IJPOIN 203 9 25 .214 -131.4802333 .175 11 2 41 45
 IJPOIN 238 7 25 .214 -131.4802333 .175 11 2 41 45
 ASSIGN TOLX=0.005
 IJPOIN 202 7 27 .214 -150.3004833 .175 11 1 2 41
 IJPOIN 201 7 29 _R=.214 _THETA=138.5197667 _Z=.175 11 1 15 41
 ASSIGN TOLX=0.001
 IJPOIN 239 7 33 _R=1.86 12.75 _PHI=-35.8105867 1 1 90
 IJPOIN 240 1 33 _R=1.86 24. _PHI=-35.8105867 1 1 90
 241 1 29 1.86 24. -48. 1 1
 242 1 27 1.86 24. -54.1233 1 1 2
 IJPOIN 243 1 11 3.037 24. 143. 2 2
 244 1 7 3.037 24. 146. 2 2
 245 1 5 3.037 24. 150. 2 2
 246 1 3 3.037 24. 156. 2 2

#-----
 SINTER 131 132 : 132 133 : 133 134 : 134 106 : 106 105 : 105 123 : 135 122
 136 104 : 137 103 : 138 102 : 101 102 : 101 139 : 139 140
 140 141 : 141 142 : 142 143 : 143 144 : 144 145 : 145 146
 146 131

SLINES 123 135 : 122 136 : 104 137 : 103 138

#-----
 IJGRID 1
 SINTER 231 232 : 232 233 : 233 234 : 234 206 : 206 205 : 205 223 : 235 222
 236 204 : 237 203 : 238 202 : 201 202 : 201 239 : 239 240
 240 241 : 241 242 : 242 243 : 243 244 : 244 245 : 245 246
 246 231

SLINES 223 235 : 222 236 : 204 237 : 203 238

IJSOL 0 0 1 S0

RULE 5 1

KNAME 122 142 1 1 FACE IN CENT A

131 140 1 5 FACE IN LEFT A

132 134 1 5 FACE IN RIGHT A

#----- 139 140 1 5 FACE IN TOP A (VANE2.PRF)

MESH

MERGE

ASSIGN TOLX=0.005

MERGE

ASSIGN TOLX=0.001

#----- MESH 3 - CONCAVE BOTTOM RIGHT -----

#----- STATION 1 -----

IJPOIN	139	1	29	R=4.3044512	THATER=12.75	PHI=35.	3	3	90
IJPOIN	101	1	25	R=.214	THETA=138.5197667	Z=.320	11	3	15 41
IJPOIN	114	3	25	2.188	71.7436894	.320	12	3	41 42
IJPOIN	113	5	25	2.188	69.3596831	.320	12	3	42
	150	5	19	2.188	54.9443595	.320	12	3	4 42
	112	7	19	2.188	54.9443595	.320	12	3	4 42
IJPOIN	151	7	17	3.659	51.5437539	.320	13	4	42 43
IJPOIN	149	9	17	3.659	51.5437539	.320	13	4	42 43
IJPOIN	111	11	17	3.659	51.5437539	.320	13	4	42 43
IJPOIN	152	11	13	3.659	43.	.320	13	4	43
IJPOIN	153	13	13	3.659	43.	.320	13	4	43
IJPOIN	154	13	7	3.659	34.0043818	.320	13	4	5 43
IJPOIN	124	15	7	3.659	34.0043818	.320	13	4	5 43
ASSIGN TOLX=0.005									
IJPOIN	155	15	5	.214	30.8790069	.320	14	5	43 44
IJPOIN	110	17	5	.214	30.8790069	.320	14	5	43 44
IJPOIN	109	17	3	.214	-5.5	.320	14	5	6 44
IJPOIN	106	17	1	.214	-41.4802333	.320	14	6	15 44
ASSIGN TOLX=0.001									
IJPOIN	134	21	1	3.147	-30.	150.	6	6	
IJPOIN	156	21	3	.5	-30.	-32.5248043	5	5	6
IJPOIN	157	21	7	3.2028762	-30.	42.8012089	4	4	5
	158	21	19	3.6725711	-30.	35.	3	3	4
IJPOIN	159	21	29	R=4.3044512	THATER=-30.	PHI=35.	3	3	90
	160	7	29	4.3044512	5.	35.	3	3	90
	161	5	29	4.3044512	7.	35.	3	3	90
	162	3	29	4.3044512	9.	35.	3	3	90

#----- STATION 2 -----

IJPOIN	239	1	29	R=1.86	12.75	PHI=-35.1303336	1	1	90
IJPOIN	201	1	25	R=.214	THETA=138.5197667	Z=.175	11	1	15 41
IJPOIN	214	3	25	2.188	71.7436894	.175	12	1	41 42
IJPOIN	213	5	25	2.188	69.3596831	.175	12	1	42
ASSIGN TOLX=0.005									
IJPOIN	250	5	19	2.188	53.9324362	.175	12	1	2 42
	212	7	19	2.188	53.9324362	.175	12	1	2 42
IJPOIN	251	7	17	3.659	51.5437539	.175	13	2	42 43
IJPOIN	249	9	17	3.659	51.5437539	.175	13	2	42 43
IJPOIN	211	11	17	3.659	51.5437539	.175	13	2	42 43
IJPOIN	252	11	13	3.659	45.	.175	13	2	43
IJPOIN	253	13	13	3.659	45.	.175	13	2	43
	254	13	7	3.659	35.	.175	13	2	43
	224	15	7	3.659	35.	.175	13	2	43
IJPOIN	255	15	5	.214	30.8790069	.175	14	2	43 44
	210	17	5	.214	30.8790069	.175	14	2	43 44
	209	17	3	.214	-5.5	.175	14	2	44
	206	17	1	.214	-41.4802333	.175	14	2	44
	234	21	1	3.037	-30.	150.	2	2	
IJPOIN	256	21	3	3.037	-30.	145.	2	2	
IJPOIN	257	21	7	3.037	-30.	140.	2	2	
	258	21	19	1.86	-30.	-54.1223	1	1	2

```

IJPOIN 259 21 29 R=1.86 -30. -35.8105867 1 1 90
        260 7 29 R=1.86 5. -35.8105867 1 1 90
        261 5 29 R=1.86 7. -35.8105867 1 1 90
        262 3 29 R=1.86 9. -35.8105867 1 1 90

```

```

#-----
SINTER 139 101 : 101 114 : 114 113 : 113 150 : 112 151 : 111 152
        153 154 : 124 155
        110 109 : 109 106 : 106 134 : 134 156 : 156 157
        157 158 : 158 159 : 159 160 : 160 161 : 161 162 : 162 139
SLINES 150 112 : 151 149 : 149 111 : 152 153 : 154 124 : 155 110

```

```

#-----
IJGRID 1
SINTER 239 201 : 201 214 : 214 213 : 213 250 : 212 251 : 211 252
        253 254 : 224 255
        210 209 : 209 206 : 206 234 : 234 256 : 256 257
        257 258 : 258 259 : 259 260 : 260 261 : 261 262 : 262 239
SLINES 250 212 : 251 249 : 249 211 : 252 253 : 254 224 : 255 210
IJSOL 0 0 1 S0
RULE 5 1
KNAME 150 157 1 1 FACE IN CENT B
        134 159 1 5 FACE IN RIGH B

```

```

#----- 139 159 1 5 FACE IN TOP B (VANE2.PRF)

```

```

MESH
MERGE
ASSIGN TOLX=0.005
MERGE
ASSIGN TOLX=0.001

```

```

#----- MESH 4 - CONVEX BOTTOM LEFT -----

```

```

#----- STATION 7 -----
IJPOIN 731 1 1 3.121 24. Z=1.34 91 8 94
        732 23 1 3.121 -30. 1.34 91 8 94
        733 23 3 1.5805887 -30. 172. 8 8
IJPOIN 706 19 3 .170 -41.4802333 -.150 19 8 15 49
ASSIGN TOLX=.005705
IJPOIN 705 15 3 r=.170 -131.4802333 -.150 19 8 49 65
IJPOIN 734 15 9 x=.5 .868 -.150 15 8 65
IJPOIN 724 13 9 x=.5 .868 -.150 15 8 65
IJPOIN 723 13 11 x=.381 .868 -.150 15 7 8 65
ASSIGN TOLX=0.001
IJPOIN 735 13 15 x=0. y=.868 z=-.150 15 7 65
IJPOIN 704 11 15 x=0. y=.868 z=-.150 15 7 65
IJPOIN 736 11 21 x=-.51 y=.868 z=-.150 15 7 65
IJPOIN 722 9 21 x=-.51 y=.868 z=-.150 15 7 65
IJPOIN 703 9 23 .170 -131.4802333 -.150 16 7 46 65
IJPOIN 702 9 25 .170 -160. -.150 16 7 46
IJPOIN 701 9 27 R=.170 THETA=138.5197667 Z=-.150 16 7 15 46
        737 9 29 4.155 9. 2.66 91 7 93
IJPOIN 738 1 29 4.155 24. 2.66 91 7 93
ASSIGN TOLX=.006
IJPOIN 739 1 11 1.3 24. 150.3955773 7 7 8
ASSIGN TOLX=.001
IJPOIN 760 9 31 4.195 9. 2.663 91 7 95
        761 1 31 4.195 24. 2.663 91 7 95

```

```

#----- STATION 8 -----
IJPOIN 831 1 1 12.6536283 24. 75. 10 10 94
        832 23 1 12.6536283 -30. 75. 10 10 94
        833 23 3 12.75 -30. 75. 10 10
IJPOIN 806 19 3 .170 -41.4802333 -.425 19 10 15 49
ASSIGN TOLX=.005
IJPOIN 805 15 3 r=.170 -131.4802333 -.425 19 10 49 65

```

```

IJPOIN 834 15 9 _x=.5218596 1.143      -.170      15 9 10 65
IJPOIN 823 13 9 _x=.5218596 1.143      -.170      15 9 10 65
ASSIGN TOLX=0.001
IJPOIN 835 13 15 _x=0. _y=1.143      _z=-.170      15 9 65
IJPOIN 804 11 15 _x=0. _y=1.143      _z=-.170      15 9 65
      836 11 21 _x=-.6353931 1.143      -.170      15 9 65
      822 9 21 _x=-.6353931 1.143      -.170      15 9 65
IJPOIN 803 9 23      .170      -131.4802333      -.425      16 9 46
IJPOIN 802 9 25      .170      -160.      -.425      16 9 46
IJPOIN 801 9 27 _R=.170 _THETA=138.5197667 _Z=-.425      16 9 15 46
      838 9 29 4.155      9.      2.543      91 9 93 96
IJPOIN 839 1 29 4.155      24.      2.543      91 9 93 96
IJPOIN 840 1 21 _R=5.5652664      24.      45.      9 9
      841 1 9 13.1076135      24.      75.      10 9 10
      860 9 31 4.195      9.      2.543      91 95 96
      861 1 31 4.195      24.      2.543      91 95 96

```

```

#-----
SINTER 731 732 : 732 733 : 733 706 : 706 705 : 705 734 : 724 723
      723 735 : 704 736
      722 703 : 703 702 : 702 701 : 701 737 : 737 738 : 738 739
      739 731 : 737 760 : 760 761 : 761 738
SLINES 734 724 : 735 704 : 736 722

```

```

#-----
IJGRID 1
SINTER 831 832 : 832 833 : 833 806 : 806 805 : 805 834 : 823 835
      804 836
      822 803 : 803 802 : 802 801 : 801 838 : 838 839 : 839 840
      840 841 : 841 831 : 838 860 : 860 861 : 861 839
SLINES 834 823 : 835 804 : 836 822
IJSOL 0 0 1 S0
RULE 5 1
KNAME 834 840 5 5 FACE OUT CENT A
      831 861 1 5 FACE OUT LEFT A
      832 833 1 5 FACE OUT RIGH A

```

```

#----- 838 839 1 5 FACE OUT TOP A (VANE.PRF)

```

```

MESH
MERGE
ASSIGN TOLX=0.005
MERGE
ASSIGN TOLX=0.001

```

```

#----- MESH 5 - CONVEX BOTTOM RIGHT -----

```

```

#----- STATION 7 -----

```

```

IJPOIN 737 1 27 4.155      9.      2.663      91 7 93
IJPOIN 701 1 25 _R=.170 _THETA=138.5197667 _Z=-.150      16 7 15 46
ASSIGN TOLX=0.005
IJPOIN 714 3 25 2.144      70.6675      -.150      17 7 46 47
IJPOIN 713 5 25 2.144      68.8300281      -.150      17 7 47
ASSIGN TOLX=0.001
IJPOIN 750 5 21 2.144      59.      -.150      17 7 47
IJPOIN 728 7 21 2.144      59.      -.150      17 7 47
IJPOIN 751 7 19 2.144      54.5      -.150      17 7 47
IJPOIN 727 9 19 2.144      54.5      -.150      17 7 47
IJPOIN 752 9 17 2.144      49.8589617      -.150      17 7 47 48
IJPOIN 712 11 17 2.144      49.8589617      -.150      17 7 47 48
IJPOIN 753 11 11 3.419      40.      -.150      18 7 48
IJPOIN 726 13 11 3.419      40.      -.150      18 7 48
ASSIGN TOLX=0.0058
IJPOIN 711 13 9 3.419      35.25      -.150      18 7 8 48
ASSIGN TOLX=0.001
IJPOIN 754 13 7 3.419      34.      -.150      18 8 48

```

IJPOIN	725	15	7	3.419	34.	-.150	18	8	48
IJPOIN	710	15	5	.170	30.8790069	-.150	19	8	48 49
IJPOIN	709	15	3	.170	-5.5	-.150	19	8	49
IJPOIN	706	15	1	.170	-41.4802333	-.150	19	8	15 49
	733	19	1	1.5805887	-30.	172.	8	8	
ASSIGN TOLX=0.006									
IJPOIN	755	19	9	1.3	-30.	150.3955773	7	7	8
ASSIGN TOLX=0.001									
IJPOIN	756	19	27	4.155	-30.	2.66	91	7	93
IJPOIN	757	5	27	4.155	5.	2.66	91	7	93
IJPOIN	758	3	27	4.155	7.	2.66	91	7	93
	762	19	29	4.195	-30.	2.663	91	7	95
	763	5	29	4.195	5.	2.663	91	7	95
	764	3	29	4.195	7.	2.663	91	7	95
	760	1	29	4.195	9.	2.663	91	7	95
#----- STATION 8 -----									
IJPOIN	838	1	27	4.155	9.	2.543	91	9	93 96
IJPOIN	801	1	25	.170	138.5197667	-.425	16	9	15 46
IJPOIN	814	3	25	.11	90.	-.425	16	9	
IJPOIN	813	5	25	2.144	68.8300281	-.425	17	9	47
	850	5	21	2.144	58.	-.425	17	9	47
	826	7	21	2.144	58.	-.425	17	9	47
	851	7	19	2.144	52.7420319	-.425	17	9	47
	825	9	19	2.144	52.7420319	-.425	17	9	47
IJPOIN	852	9	17	2.144	49.8589617	-.425	17	9	47 48
IJPOIN	812	11	17	2.144	49.8589617	-.425	17	9	47 48
	853	11	11	3.419	41.	-.425	18	9	48
	824	13	11	3.419	41.	-.425	18	9	48
IJPOIN	854	13	7	3.419	33.5646343	-.425	18	10	9 48
IJPOIN	811	15	7	3.419	33.5646343	-.425	18	10	9 48
IJPOIN	810	15	5	.170	30.8790069	-.425	19	10	48 49
IJPOIN	809	15	3	.170	-5.5	-.425	19	10	49
IJPOIN	806	15	1	.170	-41.4802333	-.425	19	10	15 49
	833	19	1	12.75	-30.	75.	10	10	
	855	19	7	13.1076135	-30.	75.	10	9	10
IJPOIN	856	19	19	R=5.5652664	-30.	45.	9	9	
IJPOIN	857	19	27	4.155	-30.	2.543	91	9	93 96
IJPOIN	858	5	27	4.155	5.	2.543	91	9	93 96
IJPOIN	859	3	27	4.155	7.	2.543	91	9	93 96
	860	1	29	4.195	9.	2.543	91	95	96
	862	19	29	4.195	-30.	2.543	91	95	96
	863	5	29	4.195	5.	2.543	91	95	96
	864	3	29	4.195	7.	2.543	91	95	96
#-----									
SINTER	737	701	:	701	714	:	714	713	:
	712	753	:	726	711	:	711	754	:
	706	733	:	733	755	:	755	756	:
	756	762	:	762	763	:	763	764	:
SLINES	750	728	:	751	727	:	752	712	:
			:	753	726	:	754	725	:
#-----									
IJGRID	1								
SINTER	838	801	:	801	814	:	814	813	:
	812	853	:	824	854	:	811	810	:
	833	855	:	855	856	:	856	857	:
	857	862	:	862	863	:	863	864	:
SLINES	850	826	:	851	825	:	852	812	:
			:	853	824	:	854	811	:
IJSOL	0 0 1 S0								
RULE	5 1								
KNAME	851 855 5 5 FACE OUT CENT B								
	833 862 1 5 FACE OUT RIGH B								

```

#----- 838 857 1 5 FACE OUT TOP B (VANE.PRF)
MESH
MERGE
ASSIGN TOLX=0.005
MERGE
ASSIGN TOLX=0.001
#----- MESH 6 TORUS INNER RING -----
#----- TORUS STATION 3 AT 0 DEGREE -----
#FIXED POINTS (EXCEPT FOR THETA)
IJPOINT 101 1 5 3.525998 0.0 3.867997 91 3 90
102 7 5 3.690646 0.0 4.143754 91
107 1 1 3.563346 0.0 3.814658 91 1 90
106 7 1 3.741757 0.0 4.119106 91
108 7 3 3.716223 0.0 4.131503 91
116 55 3 4.279954 0.0 2.590498 91
110 55 1 4.290326 0.0 2.636950 91
109 59 1 4.195000 0.0 2.662999 91 7 95
114 55 5 4.269582 0.0 2.544046 91
115 59 5 4.195000 0.0 2.554202 91 95 96
#VARYING POINTS
IJPOIN 103 13 5 3.881081 0.0 4.792418 91
104 13 3 3.905653 0.0 4.787814 91
105 13 1 3.930226 0.0 4.783211 91
111 49 1 4.717591 0.0 2.345176 91
112 49 3 4.704024 0.0 2.324177 91
113 49 5 4.690458 0.0 2.303178 91
117 33 3 8.649978 0.0 4.182926 91
118 0 0 6.240000 0.0 4.182997 91
#----- TORUS STATION 3.1 AT 7.5 DEGREE -----
#FIXED POINTS (EXCEPT FOR THETA)
IJPOINT 201 1 5 3.525998 -7.5 3.867997 91 3 90
202 7 5 3.690646 -7.5 4.143754 91
207 1 1 3.563346 -7.5 3.814658 91 1 90
206 7 1 3.741757 -7.5 4.119106 91
208 7 3 3.716223 -7.5 4.131503 91
216 55 3 4.279954 -7.5 2.590498 91
210 55 1 4.290326 -7.5 2.636950 91
209 59 1 4.195000 -7.5 2.662999 91 7 95
214 55 5 4.269582 -7.5 2.544046 91
215 59 5 4.195000 -7.5 2.554202 91 95 96
#VARYING POINTS
IJPOIN 203 13 5 3.8806591 -7.5 4.7860231 91
204 13 3 3.9052143 -7.5 4.7813334 91
205 13 1 3.9297707 -7.5 4.7766447 91
211 49 1 4.7158003 -7.5 2.3468049 91
212 49 3 4.7022295 -7.5 2.3258080 91
213 49 5 4.6886601 -7.5 2.3048112 91
217 33 3 8.5976315 -7.5 4.1729436 91
218 0 0 6.2124996 -7.5 4.1729970 91
#----- TORUS STATION 3.2 AT 15 DEGREE -----
#FIXED POINTS (EXCEPT FOR THETA)
IJPOINT 301 1 5 3.525998 -15.0 3.867997 91 3 90
302 7 5 3.690646 -15.0 4.143754 91
307 1 1 3.563346 -15.0 3.814658 91 1 90
306 7 1 3.741757 -15.0 4.119106 91
308 7 3 3.716223 -15.0 4.131503 91
316 55 3 4.279954 -15.0 2.590498 91
310 55 1 4.290326 -15.0 2.636950 91
309 59 1 4.195000 -15.0 2.662999 91 7 95
314 55 5 4.269582 -15.0 2.544046 91

```

	315	59	5	4.195000	-15.0	2.554202	91 95 96
#VARYING POINTS							
IJPOINT	303	13	5	3.8802371	-15.0	4.7796288	91
	304	13	3	3.9047756	-15.0	4.7748528	91
	305	13	1	3.9293151	-15.0	4.7700782	91
	311	49	1	4.7140098	-15.0	2.3484335	91
	312	49	3	4.7004356	-15.0	2.3274391	91
	313	49	5	4.6868625	-15.0	2.3064446	91
	317	33	3	8.5452862	-15.0	4.1629610	91
	318	0	0	6.1849990	-15.0	4.1629968	91
#-----	TORUS STATION 3.3 AT 17 DEGREE						
#FIXED POINTS (EXCEPT FOR THETA)							
IJPOINT	401	1	5	3.525998	-17.0	3.867997	91 3 90
	402	7	5	3.690646	-17.0	4.143754	91
	407	1	1	3.563346	-17.0	3.814658	91 1 90
	406	7	1	3.741757	-17.0	4.119106	91
	408	7	3	3.716223	-17.0	4.131503	91
	416	55	3	4.279954	-17.0	2.590498	91
	410	55	1	4.290326	-17.0	2.636950	91
	409	59	1	4.195000	-17.0	2.662999	91 7 95
	414	55	5	4.269582	-17.0	2.544046	91
	415	59	5	4.195000	-17.0	2.554202	91 95 96
#VARYING POINTS							
IJPOINT	403	13	5	3.8801246	-17.0	4.7779231	91
	404	13	3	3.9046586	-17.0	4.7731242	91
	405	13	1	3.9291937	-17.0	4.7683272	91
	411	49	1	4.7135320	-17.0	2.3488679	91
	412	49	3	4.6999569	-17.0	2.3278739	91
	413	49	5	4.6863832	-17.0	2.3068800	91
	417	33	3	8.5313272	-17.0	4.1602988	91
	418	0	0	6.1776657	-17.0	4.1603298	91
#-----	TORUS STATION 3.4 AT 19 DEGREE						
#FIXED POINTS (EXCEPT FOR THETA)							
IJPOINT	501	1	5	3.525998	-19.0	3.867997	91 3 90
	502	7	5	3.690646	-19.0	4.143754	91
	507	1	1	3.563346	-19.0	3.814658	91 1 90
	506	7	1	3.741757	-19.0	4.119106	91
	508	7	3	3.716223	-19.0	4.131503	91
	516	55	3	4.279954	-19.0	2.590498	91
	510	55	1	4.290326	-19.0	2.636950	91
	509	59	1	4.195000	-19.0	2.662999	91 7 95
	514	55	5	4.269582	-19.0	2.544046	91
	515	59	5	4.195000	-19.0	2.554202	91 95 96
#VARYING POINTS							
IJPOINT	503	13	5	3.8800120	-19.0	4.7762179	91
	504	13	3	3.9045415	-19.0	4.7713962	91
	505	13	1	3.9290721	-19.0	4.7665758	91
	511	49	1	4.7130547	-19.0	2.3493021	91
	512	49	3	4.6994786	-19.0	2.3283091	91
	513	49	5	4.6859035	-19.0	2.3073156	91
	517	33	3	8.5173683	-19.0	4.1576371	91
	518	0	0	6.1703320	-19.0	4.1576629	91
#-----	TORUS STATION 3.5 AT 24 DEGREE						
#FIXED POINTS (EXCEPT FOR THETA)							
IJPOINT	601	1	5	3.525998	-24.0	3.867997	91 3 90
	602	7	5	3.690646	-24.0	4.143754	91
	607	1	1	3.563346	-24.0	3.814658	91 1 90
	606	7	1	3.741757	-24.0	4.119106	91
	608	7	3	3.716223	-24.0	4.131503	91
	616	55	3	4.279954	-24.0	2.590498	91

	610	55	1	4.290326	-24.0	2.636950	91	
	609	59	1	4.195000	-24.0	2.662999	91	7 95
	614	55	5	4.269582	-24.0	2.544046	91	
	615	59	5	4.195000	-24.0	2.554202	91	95 96
#VARYING POINTS								
IJPOINT	603	13	5	3.8797307	-24.0	4.7719550	91	
	604	13	3	3.9042490	-24.0	4.7670755	91	
	605	13	1	3.9287684	-24.0	4.7621984	91	
	611	49	1	4.7118607	-24.0	2.3503881	91	
	612	49	3	4.6982822	-24.0	2.3293962	91	
	613	49	5	4.6847053	-24.0	2.3084044	91	
	617	33	3	8.4824705	-24.0	4.1509819	91	
	618	0	0	6.1519985	-24.0	4.1509962	91	
#----- TORUS STATION 3.6 AT 29 DEGREE -----								
#FIXED POINTS (EXCEPT FOR THETA)								
IJPOINT	701	1	5	3.525998	-29.0	3.867997	91	3 90
	702	7	5	3.690646	-29.0	4.143754	91	
	707	1	1	3.563346	-29.0	3.814658	91	1 90
	706	7	1	3.741757	-29.0	4.119106	91	
	708	7	3	3.716223	-29.0	4.131503	91	
	716	55	3	4.279954	-29.0	2.590498	91	
	710	55	1	4.290326	-29.0	2.636950	91	
	709	59	1	4.195000	-29.0	2.662999	91	7 95
	714	55	5	4.269582	-29.0	2.544046	91	
	715	59	5	4.195000	-29.0	2.554202	91	95 96
#VARYING POINTS								
IJPOINT	703	13	5	3.8794494	-29.0	4.7676916	91	
	704	13	3	3.9039564	-29.0	4.7627549	91	
	705	13	1	3.9284649	-29.0	4.7578206	91	
	711	49	1	4.7106671	-29.0	2.3514738	91	
	712	49	3	4.6970863	-29.0	2.3304837	91	
	713	49	5	4.6835070	-29.0	2.3094933	91	
	717	33	3	8.4475737	-29.0	4.1443267	91	
	718	0	0	6.1336651	-29.0	4.1443291	91	
#----- TORUS STATION 5.1 AT 34 DEGREE -----								
#FIXED POINTS (EXCEPT FOR THETA)								
IJPOINT	801	1	5	3.525998	-34.0	3.867997	91	3 90
	802	7	5	3.690646	-34.0	4.143754	91	
	807	1	1	3.563346	-34.0	3.814658	91	1 90
	806	7	1	3.741757	-34.0	4.119106	91	
	808	7	3	3.716223	-34.0	4.131503	91	
	816	55	3	4.279954	-34.0	2.590498	91	
	810	55	1	4.290326	-34.0	2.636950	91	
	809	59	1	4.195000	-34.0	2.662999	91	7 95
	814	55	5	4.269582	-34.0	2.544046	91	
	815	59	5	4.195000	-34.0	2.554202	91	95 96
#VARYING POINTS								
IJPOINT	803	13	5	3.8791013	-34.0	4.7621150	91	
	804	13	3	3.9035928	-34.0	4.7571039	91	
	805	13	1	3.9280858	-34.0	4.7520952	91	
	811	49	1	4.7087231	-34.0	2.3520501	91	
	812	49	3	4.6950526	-34.0	2.3311200	91	
	813	49	5	4.6813831	-34.0	2.3101897	91	
	817	33	3	8.4076223	-34.0	4.1356626	91	
	818	0	0	6.1126652	-34.0	4.1356626	91	
#----- TORUS STATION 5.2 AT 39 DEGREE -----								
#FIXED POINTS (EXCEPT FOR THETA)								
IJPOINT	901	1	5	3.525998	-39.0	3.867997	91	3 90
	902	7	5	3.690646	-39.0	4.143754	91	
	907	1	1	3.563346	-39.0	3.814658	91	1 90

906	7	1	3.741757	-39.0	4.119106	91	
908	7	3	3.716223	-39.0	4.131503	91	
916	55	3	4.279954	-39.0	2.590498	91	
910	55	1	4.290326	-39.0	2.636950	91	
909	59	1	4.195000	-39.0	2.662999	91	7 95
914	55	5	4.269582	-39.0	2.544046	91	
915	59	5	4.195000	-39.0	2.554202	91	95 96
#VARYING POINTS							
IJPOIN	903	13	5	3.8787367	-39.0	4.7562099	91
	904	13	3	3.9032116	-39.0	4.7511201	91
	905	13	1	3.9276876	-39.0	4.7460327	91
	911	49	1	4.7065916	-39.0	2.3524990	91
	912	49	3	4.6928096	-39.0	2.3316436	91
	913	49	5	4.6790285	-39.0	2.3107884	91
	917	33	3	8.3664074	-39.0	4.1264963	91
	918	0	0	6.0909986	-39.0	4.1264963	91
#----- TORUS STATION 5.3 AT 44 DEGREE -----							
#FIXED POINTS (EXCEPT FOR THETA)							
IJPOINT	1001	1	5	3.525998	-44.0	3.867997	91 3 90
	1002	7	5	3.690646	-44.0	4.143754	91
	1007	1	1	3.563346	-44.0	3.814658	91 1 90
	1006	7	1	3.741757	-44.0	4.119106	91
	1008	7	3	3.716223	-44.0	4.131503	91
	1016	55	3	4.279954	-44.0	2.590498	91
	1010	55	1	4.290326	-44.0	2.636950	91
	1009	59	1	4.195000	-44.0	2.662999	91 7 95
	1014	55	5	4.269582	-44.0	2.544046	91
	1015	59	5	4.195000	-44.0	2.554202	91 95 96
#VARYING POINTS							
IJPOIN	1003	13	5	3.8783720	-44.0	4.7503052	91
	1004	13	3	3.9028301	-44.0	4.7451367	91
	1005	13	1	3.9272897	-44.0	4.7399702	91
	1011	49	1	4.7044601	-44.0	2.3529477	91
	1012	49	3	4.6905665	-44.0	2.3321674	91
	1013	49	5	4.6766739	-44.0	2.3113868	91
	1017	33	3	8.3251934	-44.0	4.1173301	91
	1018	0	0	6.0693326	-44.0	4.1173301	91
#----- TORUS STATION 5.4 AT 49 DEGREE -----							
#FIXED POINTS (EXCEPT FOR THETA)							
IJPOINT	1101	1	5	3.525998	-49.0	3.867997	91 3 90
	1102	7	5	3.690646	-49.0	4.143754	91
	1107	1	1	3.563346	-49.0	3.814658	91 1 90
	1106	7	1	3.741757	-49.0	4.119106	91
	1108	7	3	3.716223	-49.0	4.131503	91
	1116	55	3	4.279954	-49.0	2.590498	91
	1110	55	1	4.290326	-49.0	2.636950	91
	1109	59	1	4.195000	-49.0	2.662999	91 7 95
	1114	55	5	4.269582	-49.0	2.544046	91
	1115	59	5	4.195000	-49.0	2.554202	91 95 96
#VARYING POINTS							
IJPOIN	1103	13	5	3.8780072	-49.0	4.7444000	91
	1104	13	3	3.9024489	-49.0	4.7391529	91
	1105	13	1	3.9268918	-49.0	4.7339077	91
	1111	49	1	4.7023282	-49.0	2.3533967	91
	1112	49	3	4.6883235	-49.0	2.3326910	91
	1113	49	5	4.6743193	-49.0	2.3119853	91
	1117	33	3	8.2839785	-49.0	4.1081638	91
	1118	0	0	6.0476661	-49.0	4.1081638	91
#----- TORUS STATION 5.5 AT 54 DEGREE -----							
#FIXED POINTS (EXCEPT FOR THETA)							

IJPOINT	1201	1	5	3.525998	-54.0	3.867997	91	3	90
	1202	7	5	3.690646	-54.0	4.143754	91		
	1207	1	1	3.563346	-54.0	3.814658	91	1	90
	1206	7	1	3.741757	-54.0	4.119106	91		
	1208	7	3	3.716223	-54.0	4.131503	91		
	1216	55	3	4.279954	-54.0	2.590498	91		
	1210	55	1	4.290326	-54.0	2.636950	91		
	1209	59	1	4.195000	-54.0	2.662999	91	7	95
	1214	55	5	4.269582	-54.0	2.544046	91		
	1215	59	5	4.195000	-54.0	2.554202	91	95	96

#VARYING POINTS

	1203	13	5	3.8776426	-54.0	4.7384949	91		
	1204	13	3	3.9020674	-54.0	4.7331691	91		
	1205	13	1	3.9264936	-54.0	4.7278452	91		
	1211	49	1	4.7001967	-54.0	2.3538454	91		
	1212	49	3	4.6860809	-54.0	2.3332145	91		
	1213	49	5	4.6719646	-54.0	2.3125839	91		
	1217	33	3	8.2427645	-54.0	4.0989976	91		
	1218	0	0	6.0259995	-54.0	4.0989976	91		

#-----
 SLINES 101 102 103 104 105 106 107 : 108 104
 SINTER 107 101
 #-----

IJGRID 1
 SLINES 201 202 203 204 205 206 207 : 208 204
 SINTER 207 201
 #-----

IJGRID 2
 SLINES 301 302 303 304 305 306 307 : 308 304
 SINTER 307 301
 #-----

IJGRID 3
 SLINES 401 402 403 404 405 406 407 : 408 404
 SINTER 407 401
 #-----

IJGRID 4
 SLINES 501 502 503 504 505 506 507 : 508 504
 SINTER 507 501
 #-----

IJGRID 5
 SLINES 601 602 603 604 605 606 607 : 608 604
 SINTER 607 601
 #-----

IJGRID 6
 SLINES 701 702 703 704 705 706 707 : 708 704
 SINTER 707 701
 #-----

IJGRID 7
 SLINES 801 802 803 804 805 806 807 : 808 804
 SINTER 807 801
 #-----

IJGRID 8
 SLINES 901 902 903 904 905 906 907 : 908 904
 SINTER 907 901
 #-----

IJGRID 9
 SLINES 1001 1002 1003 1004 1005 1006 1007 : 1008 1004
 SINTER 1007 1001
 #-----

IJGRID 10

SLINES 1101 1102 1103 1104 1105 1106 1107 : 1108 1104
SINTER 1107 1101

#-----
IJGRID 11

SLINES 1201 1202 1203 1204 1205 1206 1207 : 1208 1204
SINTER 1207 1201

#-----
IJSOL 107 103 1 S0 0 TORU IN SOL

RULE 9 1 2
13 3 4
17 5 6
21 7 8
25 9 10
27 11

KNAME 107 103 1 1 FACE TORU IN LARG
KNAME 1207 1203 27 27 FACE TORU IN SMAL

IJNAME 107 101 FACE AAAA

MESH 0 1

ROTATE 24. 3

MERGE

ASSIGN TOLX=0.005

MERGE

ASSIGN TOLX=0.001

#----- MESH 7 TORUS OUTER RING -----

SLINES 109 110 111 112 113 114 115 109 : 112 116

#-----
IJGRID 1

SLINES 209 210 211 212 213 214 215 209 : 212 216

#-----
IJGRID 2

SLINES 309 310 311 312 313 314 315 309 : 312 316

#-----
IJGRID 3

SLINES 409 410 411 412 413 414 415 409 : 412 416

#-----
IJGRID 4

SLINES 509 510 511 512 513 514 515 509 : 512 516

#-----
IJGRID 5

SLINES 609 610 611 612 613 614 615 609 : 612 616

#-----
IJGRID 6

SLINES 709 710 711 712 713 714 715 709 : 712 716

#-----
IJGRID 7

SLINES 809 810 811 812 813 814 815 809 : 812 816

#-----
IJGRID 8

SLINES 909 910 911 912 913 914 915 909 : 912 916

#-----
IJGRID 9

SLINES 1009 1010 1011 1012 1013 1014 1015 1009 : 1012 1016

#-----
IJGRID 10

SLINES 1109 1110 1111 1112 1113 1114 1115 1109 : 1112 1116

#-----
IJGRID 11

SLINES 1209 1210 1211 1212 1213 1214 1215 1209 : 1212 1216

#-----
IJSOL 111 115 1 S0 0 TORU OUT SOL

```

RULE 9 1 2
      13 3 4
      17 5 6
      21 7 8
      25 9 10
      27 11
KNAME 111 115 1 1 FACE TORU OUT LARG
KNAME 1211 1215 27 27 FACE TORU OUT SMAL
IJNAME 1209 1215 FACE BBBB
MESH 0 1
ROTATE 24. 3
MERGE
ASSIGN TOLX=0.005
MERGE
ASSIGN TOLX=0.001
#----- MESH 8 TORUS SHELL -----
SLINES 103 104 105 : 111 112 113
CIRCLE 104 117 118 : 117 112 118
#-----
IJGRID 1
SLINES 203 204 205 : 211 212 213
CIRCLE 204 217 218 : 217 212 218
#-----
IJGRID 2
SLINES 303 304 305 : 311 312 313
CIRCLE 304 317 318 : 317 312 318
#-----
IJGRID 3
SLINES 403 404 405 : 411 412 413
CIRCLE 404 417 418 : 417 412 418
#-----
IJGRID 4
SLINES 503 504 505 : 511 512 513
CIRCLE 504 517 518 : 517 512 518
#-----
IJGRID 5
SLINES 603 604 605 : 611 612 613
CIRCLE 604 617 618 : 617 612 618
#-----
IJGRID 6
SLINES 703 704 705 : 711 712 713
CIRCLE 704 717 718 : 717 712 718
#-----
IJGRID 7
SLINES 803 804 805 : 811 812 813
CIRCLE 804 817 818 : 817 812 818
#-----
IJGRID 8
SLINES 903 904 905 : 911 912 913
CIRCLE 904 917 918 : 917 912 918
#-----
IJGRID 9
SLINES 1003 1004 1005 : 1011 1012 1013
CIRCLE 1004 1017 1018 : 1017 1012 1018
#-----
IJGRID 10
SLINES 1103 1104 1105 : 1111 1112 1113
CIRCLE 1104 1117 1118 : 1117 1112 1118
#-----
IJGRID 11

```

SLINES 1203 1204 1205 : 1211 1212 1213
CIRCLE 1204 1217 1218 : 1217 1212 1218

#-----
IJSHE 103 105 2M.05 2MO.0 1 SH 0 -1 0 0 TORU IN SHEL
IJSHE 111 113 2M.05 2MO.0 1 SH 0 -1 0 0 TORU OUT SHEL
IJSHE 104 112 2M.05 2MO.0 1 SH 0 -1 0 0 TORU TORO SHEL

RULE 9 1 2
13 3 4
17 5 6
21 7 8
25 9 10
27 11

KNAME 104 112 1 1 FACE TORU SHEL LARG
KNAME 1204 1212 27 27 FACE TORU SHEL SMAL

MESH 0 0 1

ROTATE 24. 3

MERGE

SHLNOR

DOFLOO

FINISH

STOP

\$DF6

\$RUN DIAL\$DIR:BAND

START -1

REGPS

NPRINT

BAND

STOP

\$RUN DIAL\$DIR:SETUP

START

SETUP

STOP

\$RUN DIAL\$DIR:UTILITY

START

BCDOUT/UNFO=VAX	8 MATL.EV
BCDOUT/UNFO=VAX	8 ELEM.EV
BCDOUT/UNFO=VAX	8 INTO.EV
BCDOUT/UNFO=VAX	8 X.NV
BCDOUT/UNFO=VAX	8 NORM.NV
BCDOUT/UNFO=VAX	8 SKEW.NV
BCDOUT/UNFO=VAX	8 ROT.NV
BCDOUT/UNFO=VAX	8 DOF.NV
BCDOUT/UNFO=VAX	8 SDF.NV
BCDOUT/UNFO=VAX	8 RDF.NV
BCDOUT/UNFO=VAX	8 IR.NV
BCDOUT/UNFO=VAX	8 IER.EV
BCDOUT/UNFO=VAX	8 LCS.NV
BCDOUT/UNFO=VAX	8 ILL.NV
BCDOUT/UNFO=VAX	8 NAME.NV
BCDOUT/UNFO=VAX	8 NAME.EV
BCDOUT/UNFO=VAX	8 NXC.RM.DIR
BCDOUT/UNFO=VAX	8 SYS.CRM
BCDOUT/UNFO=VAX	8 PCT.HED.MESH
BCDOUT/UNFO=VAX	8 MESH.HED 0 ?
BCDOUT/UNFO=VAX	8 PCT.HED.SETU
BCDOUT/UNFO=VAX	8 CON.RM.DIR
BCDOUT/UNFO=VAX	8 CON.CON 0 ?
BCDOUT/UNFO=VAX	8 HEAD.COM
BCDOUT/UNFO=VAX	8 IER.NV

STOP

JOB, JN=VANE42, T=1000, CL=DEFERRD, MFL=1500000, US=670535.

ACCOUNT, AC=3, UPW=.

FETCH, DN=FILO01, DF=TR, TEXT='DIAL\$CRAY:FILO01.'

FETCH, DN=FILO02, DF=TR, TEXT='HYBRID6.DB'.

FETCH, DN=SCOPE, DF=TR, TEXT='DIAL\$CRAY:SCOPE.CEX'.

FETCH, DN=DOMAIN, DF=TR, TEXT='DIAL\$CRAY:DOMAIN.CEX'.

FETCH, DN=MESH, DF=TR, TEXT='DIAL\$CRAY:MESH.CEX'.

FETCH, DN=BAND, DF=TR, TEXT='DIAL\$CRAY:BAND.CEX'.

FETCH, DN=SETUP, DF=TR, TEXT='DIAL\$CRAY:SETUP.CEX'.

FETCH, DN=MATL, DF=TR, TEXT='DIAL\$CRAY:MATL.CEX'.

FETCH, DN=LOAD, DF=TR, TEXT='DIAL\$CRAY:LOAD.CEX'.

FETCH, DN=SOLVE, DF=TR, TEXT='DIAL\$CRAY:SOLVE.CEX'.

FETCH, DN=UTILITY, DF=TR, TEXT='DIAL\$CRAY:UTILITY.CEX'.

SCOPE.

DOMAIN.

RELEASE, DN=FILO02.

FETCH, DN=FILO10, DF=TR, TEXT='VANE2.FL2'.

MESH.

BAND.

SETUP.

MATL.

DOMAIN.

LOAD.

SOLVE.

UTILITY.

DISPOSE, DN=FT08, DF=BB, TEXT='VANE42.U08'.

BAD.

EXIT.

SAVE, DN=FILO02, PDN=VANE42, ID=SZETO, NA.

DISPOSE, DF=TR, DN=FILO02, TEXT='VANE42.FL2'.

/EOF

\$RUN DIAL\$DIR:SCOPE

START -1

#-----
APPLIED DISPLACEMENT CONDITIONS FROM NEW GLOBAL MODEL AND NEW LOADING
CONDITION - HYBRID6.DB
#-----

DSET D 0 1

STOP

\$RUN DIAL\$DIR:DOMAIN

START

#-----
DOMAIN VOLUME FROM MAIN MODEL
#-----

FILE SUB [4]SUB

#----- INNER RING ELEMENTS AT LARGER TORUS SIDE -----

MSET=1 COPY RANGE=1 48 1

MSET=1 INSE RANGE=4951 4962 1

#----- INNER RING ELEMENTS AT SMALLER TORUS SIDE -----

MSET=2 COPY RANGE=193 240 1

MSET=2 INSE RANGE=4999 5010 1

#----- OUTER RING ELEMENTS AT LARGER TORUS SIDE -----

MSET=3 COPY RANGE=1441 1472 1

MSET=3 INSE RANGE 5307 5316 1

#----- OUTER RING ELEMENTS AT SMALLER TORUS SIDE -----

MSET=4 COPY RANGE=1761 1792 1

MSET=4 INSE RANGE=5347 5356 1

#----- LARGER TORUS SHELL SIDE -----

MSET=5 COPY RANGE=5613 5630 1

#----- SMALLER TORUS SHELL SIDE -----

```

MSET=6 COPY RANGE=5685 5702 1
#----- INNER RING CENTER PORTION -----
MSET=7 COPY RANGE=49 192 1
#----- OUTER RING CENTER PORTION -----
MSET=8 COPY RANGE=1521 1552 1
MSET=8 INSE RANGE=1601 1632 1
MSET=8 INSE RANGE=1681 1712 1
#-----
#----- TEST AREA 1 -----
MSET=9 COPY RANGE=4999 5010 1
MSET=9 INSE ELEM=228 229 231 232 235 236 239 240
#----- TEST AREA 2 -----
MSET=10 COPY ELEM=1761T1766 1780T1784 5347T5356
#----- TEST AREA 3 -----
MSET=11 COPY ELEM=1451T1454 1465T1468
SUBMOD 1 0 MSET=9
SUBSCA 1 1 [4] SUB.RV.DIS1,0,1
        1 2 [4] SUB.RV.DIS1,0,2
        1 3 [4] SUB.RV.DIS1,0,3
        1 4 [4] SUB.RV.DIS1,0,4
        1 5 [4] SUB.RV.DIS1,0,5
        1 6 [4] SUB.RV.DIS1,0,6
SUBMOD 2 0 MSET=10
SUBSCA 2 1 [4] SUB.RV.DIS2,0,1
        2 2 [4] SUB.RV.DIS2,0,2
        2 3 [4] SUB.RV.DIS2,0,3
        2 4 [4] SUB.RV.DIS2,0,4
        2 5 [4] SUB.RV.DIS2,0,5
        2 6 [4] SUB.RV.DIS2,0,6
SUBMOD 3 0 MSET=11
SUBSCA 3 1 [4] SUB.RV.DIS3,0,1
        3 2 [4] SUB.RV.DIS3,0,2
        3 3 [4] SUB.RV.DIS3,0,3
        3 4 [4] SUB.RV.DIS3,0,4
        3 5 [4] SUB.RV.DIS3,0,5
        3 6 [4] SUB.RV.DIS3,0,6
SUBMOD 4 0 MSET=1 2 3 4 5 6 7 8
SUBSCA 4 1 [4] SUB.RV.DIS4,0,1
        4 2 [4] SUB.RV.DIS4,0,2
        4 3 [4] SUB.RV.DIS4,0,3
        4 4 [4] SUB.RV.DIS4,0,4
        4 5 [4] SUB.RV.DIS4,0,5
        4 6 [4] SUB.RV.DIS4,0,6

STOP
$RUN DIAL$DIR:MESH
CLEAR 200000
MAX/MXP0=999      10000 2500
ELTYPE  4 2 6
ASSIGN  IPAL=0
#----- MESH 1 COPY FROM VANE.PRF MODEL ALL MESHES -----
MODEL [10]
ROTATE -114. 3
SHLNOR
DOFLOO
DOFNOR 2
FINISH
STOP
$RUN DIAL$DIR:BAND
START -1
REGPS

```



```

BAND
STOP
$RUN DIAL$DIR:SETUP
START
SETUP
STOP
$RUN DIAL$DIR:MATL
START
#----- MATERIAL Ti-5Al-2.5Sn (ELI) -----
MATISO 1 .155E+08 .35 .3E-06 0.
MATL
STOP
$RUN DIAL$DIR:DOMAIN
START
FILE SUB [4]SUB
ASSIGN TOLV=2.0
MSET=1 COPY ELEM=714 724 794 804 1253T1264
NSET=1 COPY MSET=1
NSET=1 MASK NAME=FACE
DOMAIN/CLO 1 1 NSET=1
ASSIGN TOLV=.001
INTER/CLEA 1 [4]SUB.RV.DIS1,0,1 11
           1 [4]SUB.RV.DIS1,0,2 12
           1 [4]SUB.RV.DIS1,0,3 13
           1 [4]SUB.RV.DIS1,0,4 14
           1 [4]SUB.RV.DIS1,0,5 15
           1 [4]SUB.RV.DIS1,0,6 16
ASSIGN TOLV=3.0
MSET=2 COPY ELEM=1023 1032 1041 1090 1099 1108 1385T1394
NSET=2 COPY MSET=2
NSET=2 MASK NAME=FACE
DOMAIN/CLO 2 2 NSET=2
ASSIGN TOLV=.001
INTER/CLEA 2 [4]SUB.RV.DIS2,0,1 21
           2 [4]SUB.RV.DIS2,0,2 22
           2 [4]SUB.RV.DIS2,0,3 23
           2 [4]SUB.RV.DIS2,0,4 24
           2 [4]SUB.RV.DIS2,0,5 25
           2 [4]SUB.RV.DIS2,0,6 26
ASSIGN TOLV=2.0
MSET=3 COPY ELEM=805 816 823 830 837 890 901 908 915 922
NSET=3 COPY MSET=3
NSET=3 MASK NAME=FACE
DOMAIN/CLO 3 3 NSET=3
ASSIGN TOLV=.001
INTER/CLEA 3 [4]SUB.RV.DIS3,0,1 31
           3 [4]SUB.RV.DIS3,0,2 32
           3 [4]SUB.RV.DIS3,0,3 33
           3 [4]SUB.RV.DIS3,0,4 34
           3 [4]SUB.RV.DIS3,0,5 35
           3 [4]SUB.RV.DIS3,0,6 36
ASSIGN TOLV=.5
NSET=4 COPY NAME=FACE
NSET=4 DELE NSET=1 2 3
DOMAIN/CLO 4 4 NSET=4
ASSIGN TOLV=.001
INTER/CLEA 4 [4]SUB.RV.DIS4,0,1 41
           4 [4]SUB.RV.DIS4,0,2 42
           4 [4]SUB.RV.DIS4,0,3 43
           4 [4]SUB.RV.DIS4,0,4 44

```

4 [4]SUB.RV.DIS4,0,5 45

4 [4]SUB.RV.DIS4,0,6 46

STOP

\$RUN DIAL\$DIR:LOAD

START -1

LCASE 1 # APPLIED DISPLACEMENTS ON THE BOUNDARY

#----- TEST AREA 1 -----

U/NQU=11 0 1 NSET=1

U/NQU=12 0 2 NSET=1

U/NQU=13 0 3 NSET=1

U/NQU=14 0 4 NSET=1

U/NQU=15 0 5 NSET=1

U/NQU=16 0 6 NSET=1

#----- TEST AREA 2 -----

U/NQU=21 0 1 NSET=2

U/NQU=22 0 2 NSET=2

U/NQU=23 0 3 NSET=2

U/NQU=24 0 4 NSET=2

U/NQU=25 0 5 NSET=2

U/NQU=26 0 6 NSET=2

#----- TEST AREA 3 -----

U/NQU=31 0 1 NSET=3

U/NQU=32 0 2 NSET=3

U/NQU=33 0 3 NSET=3

U/NQU=34 0 4 NSET=3

U/NQU=35 0 5 NSET=3

U/NQU=36 0 6 NSET=3

#----- ALL EXCEPT THE ABOVE 3 AREAS -----

U/NQU=41 0 1 NSET=4

U/NQU=42 0 2 NSET=4

U/NQU=43 0 3 NSET=4

U/NQU=44 0 4 NSET=4

U/NQU=45 0 5 NSET=4

U/NQU=46 0 6 NSET=4

LCASE 2 # UNIT PRESSURE ON SURFACES

PSURF -303. 1 6 RANGE=561 644 1 # INNER RING PRESSURE SURFACE LEFT

-303. 1 6 RANGE=725 804 1 # INNER RING PRESSURE SURFACE RIGHT

-303. 1 3 RANGE=805 889 1 # OUTER RING PRESSURE SURFACE LEFT

-303. 1 3 RANGE=975 1041 1 # OUTER RING PRESSURE SURFACE RIGHT

-303. 1 2 RANGE= 57 70 1 # INNER RING PRESSURE SURFACE FILLET SIDE 1

-303. 1 5 RANGE= 71 84 1 # INNER RING PRESSURE SURFACE FILLET SIDE 2

-303. 1 2 RANGE= 85 98 1 # INNER RING PRESSURE SURFACE FILLET SIDE 1

-303. 1 5 RANGE= 99 112 1 # INNER RING PRESSURE SURFACE FILLET SIDE 2

-303. 1 2 RANGE=113 126 1 # INNER RING PRESSURE SURFACE FILLET SIDE 1

-303. 1 5 RANGE=127 140 1 # INNER RING PRESSURE SURFACE FILLET SIDE 2

-303. 1 2 RANGE=141 154 1 # INNER RING PRESSURE SURFACE FILLET SIDE 1

-303. 1 5 RANGE=155 168 1 # INNER RING PRESSURE SURFACE FILLET SIDE 2

-303. 1 2 RANGE=309 322 1 # OUTER RING PRESSURE SURFACE FILLET SIDE 1

-303. 1 5 RANGE=323 336 1 # OUTER RING PRESSURE SURFACE FILLET SIDE 2

-303. 1 2 RANGE=337 350 1 # OUTER RING PRESSURE SURFACE FILLET SIDE 1

-303. 1 5 RANGE=351 364 1 # OUTER RING PRESSURE SURFACE FILLET SIDE 2

-303. 1 2 RANGE=365 378 1 # OUTER RING PRESSURE SURFACE FILLET SIDE 1

-303. 1 5 RANGE=379 392 1 # OUTER RING PRESSURE SURFACE FILLET SIDE 2

-303. 1 2 RANGE=393 406 1 # OUTER RING PRESSURE SURFACE FILLET SIDE 1

-303. 1 5 RANGE=407 420 1 # OUTER RING PRESSURE SURFACE FILLET SIDE 2

-303. 1 1 RANGE=1109 1259 12 # INNER RING PRESSURE SURFACE TORUS SOLID

-303. 1 1 RANGE=1110 1260 12 # INNER RING PRESSURE SURFACE TORUS SOLID

-303. 1 1 RANGE=1111 1261 12 # INNER RING PRESSURE SURFACE TORUS SOLID

-303. 1 1 RANGE=1112 1262 12 # INNER RING PRESSURE SURFACE TORUS SOLID

-303. 1 1 RANGE=1113 1263 12 # INNER RING PRESSURE SURFACE TORUS SOLID

```

-303. 1 1 RANGE=1114 1264 12 # INNER RING PRESSURE SURFACE TORUS SOLID
-303. 1 1 RANGE=1265 1385 10 # OUTER RING PRESSURE SURFACE TORUS SOLID
-303. 1 1 RANGE=1266 1386 10 # OUTER RING PRESSURE SURFACE TORUS SOLID
-303. 1 1 RANGE=1267 1387 10 # OUTER RING PRESSURE SURFACE TORUS SOLID
-303. 1 1 RANGE=1268 1388 10 # OUTER RING PRESSURE SURFACE TORUS SOLID
-303. 1 1 RANGE=1269 1389 10 # OUTER RING PRESSURE SURFACE TORUS SOLID
303. 1 -1 RANGE=1447 1680 1 # TORUS SHELL INSIDE PRESSURE
-208. 1 3 ELEM=11T14 26T28 # INNER RING NONPRESSURE SURFACE VANE
-208. 1 3 RANGE=477 517 1 # INNER RING NONPRESSURE SURFACE LEFT
-208. 1 3 RANGE=645 651 1 # INNER RING NONPRESSURE SURFACE RIGHT
-208. 1 6 ELEM=459T462 474T476 # OUTER RING NONPRESSURE SURFACE VANE
-208. 1 6 RANGE=890 921 1 # OUTER RING NONPRESSURE SURFACE LEFT
-208. 1 6 RANGE=1042 1047 1 # OUTER RING NONPRESSURE SURFACE RIGHT

```

LOAD

STOP

\$RUN DIAL\$DIR:SOLVE

START -1

REMARK 'UNIT LOAD CASE 1 - APPLIED DISPLACEMENTS

LOADS 1,1.0

ASSIGN RK=0.

SAVE D

SAVE S

SAVE EF

FILE K [3]KE

FILE KI [3]KI

SOLVE

REMARK 'UNIT LOAD CASE 2 - UNIT PRESSURE

LOADS 2,1.0

MATRIX

ASSIGN RK=0.

SAVE D

SAVE S

SAVE EF

FILE K [3]KE

FILE KI [3]KI

SOLVE

STOP

\$UTILITY3

START -1

```

BCDOUT/UNFO=VAX      8 MATL.EV
BCDOUT/UNFO=VAX      8 ELEM.EV
BCDOUT/UNFO=VAX      8 INTO.EV
BCDOUT/UNFO=VAX      8 X.NV
BCDOUT/UNFO=VAX      8 NORM.NV
BCDOUT/UNFO=VAX      8 SKEW.NV
BCDOUT/UNFO=VAX      8 ROT.NV
BCDOUT/UNFO=VAX      8 DOF.NV
BCDOUT/UNFO=VAX      8 SDF.NV
BCDOUT/UNFO=VAX      8 RDF.NV
BCDOUT/UNFO=VAX      8 IR.NV
BCDOUT/UNFO=VAX      8 IER.EV
BCDOUT/UNFO=VAX      8 LCS.NV
BCDOUT/UNFO=VAX      8 ILL.NV
BCDOUT/UNFO=VAX      8 NAME.NV
BCDOUT/UNFO=VAX      8 NAME.EV
BCDOUT/UNFO=VAX      8 NXC.RM.DIR
BCDOUT/UNFO=VAX      8 SYS.CRM
BCDOUT/UNFO=VAX      8 PCT.HED.MESH
BCDOUT/UNFO=VAX      8 MESH.HED 0 ?
BCDOUT/UNFO=VAX      8 PCT.HED.SETU

```

BCDOUT/UNFO=VAX	8 CON.RM.DIR
BCDOUT/UNFO=VAX	8 CON.CON O ?
BCDOUT/UNFO=VAX	8 HEAD.COM
BCDOUT/UNFO=VAX	8 IER.NV
BCDOUT/UNFO=VAX	8 D.SV,?,?
BCDOUT/UNFO=VAX	8 S.EIP,?,?
BCDOUT/UNFO=VAX	8 R.SRV,?,?
BCDOUT/UNFO=VAX	8 EF.SEV,?,?
BCDOUT/UNFO=VAX	8 UL.SV,?,?
BCDOUT/UNFO=VAX	8 UL.NV,?,?
BCDOUT/UNFO=VAX	8 UAD.SV,?,?
BCDOUT/UNFO=VAX	8 UAD.NV,?,?
BCDOUT/UNFO=VAX	8 UT.NV,?,?
BCDOUT/UNFO=VAX	8 UT.NV.ENVI,?,?
BCDOUT/UNFO=VAX	8 STLT.RM.DIR
STOP	
\$DEASSIGN FOR006	
/EOF	